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COMPRESSOR STAGES 5. DATA AND PERFORMANCE
OF J.P. Nikkanen, et al (Pratt and Whitney Unclas Aircraft) Mar. 1972 261 p CSCL 21E G3/28 24820



SINGLE-STAGE EVALUATION OF HIGHLY-LOADED HIGH-MACH-NUMBER COMPRESSOR STAGES V. DATA AND PERFORMANCE OF BASELINE, CORNER-BLOW, WALL-SUCTION, AND COMBINED CORNER-BLOW WALL-SUCTION STATOR

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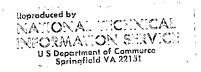
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L. Reid, Program Manager
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16. Abstract					
A single-stage compressor with a rotor tip speed of 1600 ft/sec and a 0.5 hub tip ratio was used to investigate the effects of several stator endwall treatment methods on stage range and performance. These endwall treatment methods consisted of stator corner-blow, annular wall suction upstream of stator leading edge, and combined corner-blow and annular wall suction. The overall stage performance with corner blow was essentially the same as the baseline performance. The performance for the annular wall suction and the combined corner-blow and wall suction showed a reduction in peak efficiency of 2.5 percentage points compared to the baseline data.					
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FOREWORD

The work described herein was done under NASA Contract NAS3-10482 by the Pratt & Whitney Aircraft Division of United Aircraft Corporation, East Hartford, Connecticut. The Project Manager was Mr. L. Reid, NASA-Lewis Research Center, Fluid System Components Division. The work was performed during the period 11 June 1971 through 28 October 1971.

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SINGLE-STAGE EVALUATION OF HIGHLY LOADED, HIGH-MACH-NUMBER COMPRESSOR STAGES V. DATA AND PERFORMANCE OF BASELINE, CORNER-BLOW, WALL SUCTION, AND COMBINED CORNER-BLOW AND WALL SUCTION STATOR

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SUMMARY

A compressor stage with a rotor tip speed of 1600 ft/sec was tested to evaluate the effectiveness of several stator endwall treatment methods. Blowing was applied in the corners formed by the stator suction surface and the lD wall and stator suction surface and OD wall. Annulus suction was applied at both lD and OD walls ahead of the stator leading edge plane. A combination of blowing and annulus wall suction was also applied at both lD and OD.

Comparison of data taken with and without blowing showed no significant changes in stage performance. With suction and combined suction and blowing, the corrected peak efficiency dropped 2.5 percent relative to the baseline. Blowing and combined suction and blowing gave reduced stator endwall losses, but these reductions were too small and too local to affect the overall stage performance. The weight flows at surge were practically the same for each of the stator endwall treatment methods and resulted in a surge line identical to that for the baseline data.

INTRODUCTION

Recent results from research compressors have shown that compressor rotors can be designed to operate with a high aerodynamic blade loading and/or a high inlet relative Mach number and still achieve good efficiency (85 to 94 percent) with acceptable stall-margin (12 to 15 percent). However, there is a severe penalty on stage efficiency due to high stator-losses. The major portion of the high loss region occurs in the vicinity of the stator endwalls. Therefore, gains in stage performance are limited by the level of losses in the stator endwall regions. In addition to high stator-losses, in many cases the stall-free range of the compressor stage is limited by stator stall.

As part of Contract NAS3-10482, a stator endwall treatment test program was initiated to investigate the effectiveness of various types of endwall treatments on reducing stator losses and increasing the stator stall-free range of operation. The single-stage compressor used in this investigation was the same compressor used in the work presented in reference 1 with stator corner-blow and wall-suction added. To evaluate the effect of endwall treatment on stator range, the stator vanes were restaggered four degrees open (increased incidence) with respect to the design stagger. This compressor had a design rotor tip-speed of 1600 ft/sec and demonstrated a rotor pressure ratio of 2.0, a rotor efficiency of 89 percent, a stage pressure ratio of 1.946, and a stage efficiency of 84.5 percent.

Small amounts of blowing air have been used in the past to energize boundary layers. The corner-blow technique is an adaptation of this concept to stator endwalls. Since stator endwall loss is a function of inlet condition, a reduction in inlet boundary layer should reduce the loss; the wall-suction concept is an effort to do this.

This report presents the results of applying stator corner-blow, wall suction, and combined corner-blow and wall suction to a highly-loaded, high-Mach-number single-stage compressor.

TEST APPARATUS

TEST COMPRESSOR

The compressor used in this program, Figure 1, was a highly-loaded, high-Mach-number, single-stage compressor with no inlet guide vanes, 30 MCA rotor blades, and 44 MCA stator vanes. It was the same compressor as used in the work presented in reference 1 except for the addition of corner-blow nozzles and wall suction slits and restaggered stator blades. The stator blades were restagged four degrees to increase incidence so that the effects of endwall boundary layer control treatments on stator flow range could be evaluated. The rotor was the same one used in the work presented in reference 2. A summary of rotor and stator design parameters is provided in the table below. Complete design details are given in reference 3.

MCA ROTOR AND STATOR DESIGN PARAMETERS

ROTOR – STATIONS 8 AND 9	RO	TOR –	STAT	IONS	8 ANI	D 9
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% Span	Dia — 1	Dia — 2	β* 1	β* 2	eta^* 1ss	eta^* sh	Solidity
5 (hub)	17.47	19.77	48.97	1.87	55.40	45.74	2.276
10	18.47	20.41	49.59	9.63	56.02	46.76	2.173
15	19.47	21.05	50.44	16.51	56.59	47.76	2.080
30	22.31	22.96	53.77	29.73	57.87	50.53	1.855
50	25.79	25.52	56.40	42.30	59.30	54.68	1.638
70	28.95	28.08	59.08	50.53	61.07	59.17	1.476
85	31.29	29.99	61.63	54.11	62.96	63.01	1.379
90	31.88	30.63	62.53	55.10	63.65	64.18	1.355
95 (tip)	32.50	31.27	63.21	55.84	64.14	64.96	1.332
STATOR	STATIO	NS 10 AND 1	1				·
5 (hub)	20.41	21.49	39.23	-16.41	42.15	34.47	2.010
10	21.01	21.96	38.27	-15.44	41.21	32.62	1.959
15	21.59	22.43	37.42	-14.89	40.36	30.94	1.911
30	23.31	23.90	35.44	-15.22	38.44	27.18	1.781
50	25.60	25.89	33.60	-16.04	36.72	24.01	1.632
70	27.82	27.90	32.45	-17.48	35.68	22.38	1.508
85	29.41	29.38	32.12	-19.91	35.44	22.82	1.430
90	29.91	29.86	32.15	-21.40	35.48	23.36	1.407
95 (tip)	30.38	30.29	32.33	-23.69	35.69	24.40	1.387

NOTE: Symbol definitions appear in Appendix D.

AERODYNAMIC DESIGN

Corner-Blow Stator

Significant improvements in stator performance can be obtained by reducing endwall losses. Studies have shown that separation in the corner between the stator suction surface and endwalls is a major source of loss. A stator endwall boundary layer control system was designed which uses blowing to energize this corner flow. The methods used to determine the separation points of the corner boundary layer and to calculate blowing flow rates required to prevent separation are outlined below.

The shape parameter introduced by K. Gersten [ref. 4] for a three-dimensional corner boundary layer

$$\Gamma_3 = \frac{\sqrt{-\overline{\theta}_3}}{V_{fs}} \frac{dV_{fs}}{dx} \left(\frac{V_{fs}\sqrt{-\overline{\theta}_3}}{\nu}\right)^{\frac{1}{4}}$$
 (1)

was used as the criterion for corner separation. Gersten found that turbulent corner separation occurs for Γ_3 = -0.007. A chordwise distribution of Γ_3 was calculated from airfoil static pressure distribution data obtained from the MCA stator tests conducted under NASA Contract NAS3-7614 in which stator geometry and aerodynamic conditions were very similar to those of the subject investigation. The distribution of the local values of pressure coefficient used is shown in Figure 2. Two probable points of corner boundary layer separation are indicated on the chordwise distribution of Γ_3 shown in Figure 3. They occur at approximately 22 and 52 percent of the stator chord length where Γ_3 is about -0.007. Even when the boundary layer at 22 percent chord was assumed to be completed energized, calculations showed that separation may still occur at approximately 65 percent chord. Nozzles were located in both the hub and tip stator case at 18 and 48 percent chord to blow high-energy air into the corner boundary layer just upstream of each potential separation point. Blowing simultaneously through both sets of nozzles should prevent separation at both chordwise locations. Requirements for operating with one-half optimum blowing flow were met by using nozzles at only one chordwise location, giving reduced flow while maintaining high velocity in the blowing flow.

The blowing rate required to prevent separation at each separation point is given by the expression

$$W_{\text{blow}} = \rho_{\text{fs}} V_{\text{fs}} \left(K \sqrt{-1.1\overline{\theta}_3} \delta_{x2}^* \right)$$
 (2)

where K is a shape factor for corner boundary layers obtained empirically from P&WA cascade experiments.

Figure 4 presents a sketch of the corner boundary layer showing the extent of the interference region, t, where the stator gapwise velocity profiles are affected by the corner.

Chordwise distributions of the velocity and interference momentum loss area used in the solution of equation (2) were calculated from the pressure coefficients, C_p , obtained from the stator tests conducted under NASA Contract NAS3-7614. The distribution of δ_{x2}^* was found from a correlation of cascade data [ref. 5]. A correlation of endwall boundary layer growth [ref. 5] was used to predict displacement thicknesses on hub and tip walls at the rotor exit and stator exit. Rotor inlet boundary layer measurements obtained in tests of a similar single-stage compressor in the same test stand were assumed to be the same for the subject stage. Calculated growths through the rotor and stator gave displacement thicknesses at the stator exit which were in good agreement with displacement thicknesses calculated from wake rake measurements during tests of this compressor.

Blowing flow rates at the probable points of boundary separation were established by intergrating chordwise distributions of the local values of flow given by equation (2). This procedure provided a flow rate at one point equivalent to what would be supplied by a continuous slit at the corner between the stator suction surface and the endwalls. It gave a surplus flow to insure that the boundary layer was energized. The total design flow at 18 and 48 percent chord was 0.158 lb/sec at the hub for 44 vanes calculated with this procedure and 0.096 lb/sec at the tip. The nozzles were designed to operate choked, with blowing flow rate controlled by the stator hub and tip supply pressures.

Wall-Suction-Stator

A wall-suction boundary layer control scheme was designed to improve stator performance by reducing the stator inlet displacement thickness. This was accomplished by removing wall boundary layer air through annular slits upstream of the stator leading edge, Figure 5. Enough flow was extracted to reduce $\delta_{x\,2}^*$, the boundary layer thickness at the stator inlet, below the value at which separation was predicted to occur. This value of $\delta_{x\,2}^*$ was calculated using the expression

$$\frac{2 \, \delta_{x2}^*}{c} = \left(\frac{K_2}{\Delta P/q} \right) - K_1 \tag{3}$$

where
$$K_2 = \left(\frac{\delta_{x2}^*}{c} + \frac{\delta_{x1}^*}{c}\right) - \frac{\Delta P}{q}$$

and
$$K_1 = \left(\frac{\delta_{x2}^*}{c} - \frac{\delta_{x1}^*}{c}\right)$$

 ${\rm K_1}$ and ${\rm K_2}$ have been correlated with cascade data [ref. 5].

The amount of suction flow required to obtain the desired δ_{x2}^* was obtained from

$$W_{SUCTION} = 2\pi r \rho_{fs} V_{m} \left(\theta_{a,2} - \theta_{a,1}\right)$$
 (4)

where $\theta_{a,2}$ is the momentum thickness downstream of the suction slit

$$\theta_{a,2} = \frac{1}{H_a} \left(\frac{\delta_{x2}^*}{\delta_{x2}^* / \delta_{a,2}^*} \right) \tag{5}$$

and $\theta_{a,1}$ is the momentum thickness upstream of the suction slit

$$\theta_{a,1} = \frac{\delta_{a,1}^*}{H_{a,1}} \tag{6}$$

where

$$H_a = \frac{2}{n} + 1$$
 and $\frac{\delta_a^*}{\delta} = \frac{1}{n+1}$

The displacement thickness, δ_a^* , and the boundary layer thickness, δ , were calculated from data taken during the MCA and tandem rotor tests.

The hub and tip suction slit flow rates calculated using equation (4) were 2.02 and 2.66 lb/sec, respectively. The tip slit was designed to operate choked, but choked operation of the hub slit was not possible because of piping limitations.

MECHANICAL DESIGN

Baseline Stator

The baseline stator configuration was the same as that tested with stator hub slit suction [ref. 2] except that there were no suction slits in the corner between the vane suction surface and the hub endwall. As shown in Figure 1, tubes were located in the hub and tip endwalls which were used as blowing nozzles during the corner-blow-stator test. Blowing flow was not supplied to these tubes during baseline stator tests.

Corner-Blow-Stator

Blowing nozzles were located at 18 and 48 percent of the chord length in corners followed by the vane suction surfaces and endwalls at both the stator hub and tip (Figure 5). These nozzles directed blowing flow tangent to vane suction surface and at an angle of between 10 and 15 degrees to the endwalls. Four common manifolds supplied pressurized air to sets of blowing nozzles at the same location on all the vanes. The flow rate into each of the four common manifolds and the total pressure and total temperature in each manifold were measured. These measurements were used to calculate the pressure of air entering the compressor using a calibration of Pt-nozzle-exit/Pt-manifold versus blowing flow rate corrected to the manifold temperature and pressure. Each set of forty-four blowing tubes at a given vane location could be operated and controlled independent of the other sets.

A sample vane and blowing-nozzle-assembly was calibrated to determine the choke flow rate and pressure loss for each of the four nozzle configurations. The assembly was connected to a variable high-pressure air supply to simulate the manifold that supplies the nozzles in the test stage. Flow rates were measured for nozzle exit pressures from 1.4 to 2.2 times atmosheric pressure, and the choke flow rate was determined for each nozzle. Based on the results of this calibration, a blowing nozzle tube inner diameter of 0.096 inch was selected. With this tube size, the ID and OD nozzles were capable of supplying 260 and 240 percent of their respective design flow rates.

Wall-Suction-Stator

Wall boundary layer air was extracted through annular slits in the flowpath casing, shown in Figure 6, and collected in separate hub and tip plenums which were evacuated by external exhausters. The hub slit annulus was 0.170 inch wide and made an angle of 38 degrees with the flowpath. The tip slit annulus was 0.140 inch wide and made on air angle of 25 degrees with the flowpath. Flow rate, total pressure, and total temperature were measured for each plenum.

Four hollow struts ahead of the rear bearing supports removed the boundary layer air extracted through the hub slit (Figure 1). Flowpath exit area requirements limited the number and size of the struts used to remove the suction flow. Additional blockage from more than four struts would have caused the compressor discharge flow to choke near the hub at the wide open throttle data point. With only four struts and a requirement to pass a flow of 2.02 lb/sec, it was necessary to design the suction system for low pressure-loss. Slit manifold pressure was below the lowest gapwise static pressure previously measured at the stator inlet; therefore, recirculation should not have occurred in the slots during slot suction testing.

During the corner blow stator test, the annular wall-suction slits were sealed to prevent recirculation in the slits due to the static pressure variation across the gap between adjacent stator vanes. Access for removing the sealer material from the hub and tip slits was obtained by removing the rotor and front shaft assembly at the test stand.

Combined Corner-Blow Wall-Suction Stator

Simultaneous or independent operation of the corner-blow nozzles and the annular wall-suction slits was possible with this stator. For tests with combined corner-blowing and wall suction, both treatments were operated simultaneously.

FACILITIES

To satisfy the blowing and suction flow requirements for the boundary layer control treatments, connecting piping was designed to provide access to the test facility suction and high pressure air supply systems (Figure 7). The design provided remotely and independently controllable flow rates for each of the four sets of blow nozzles and each of the two annular wall-suction slits. Other facility hardware was the same as described in reference 1.

INSTRUMENTATION AND CALIBRATION

Static pressure in the four blowing-nozzle manifolds and in the hub annular wall-suction slit plenum was measured by means of four static pressure taps, and the total temperature was measured with two bare-wire thermocouples. Eight static pressure taps and four bare-wire thermocouples were used to measure the static pressure and total temperature in the tip wall-suction slit plenum. There were two static pressure taps and one thermocouple in each of four 90-degree segments of the tip plenum. Blowing and suction flow rates for each manifold or plenum were measured by means of sharp edge orifices. Other instrumentation was as described in reference 1. Typical instrumentation is shown in Figure 8, and axial and circumferential locations of instrumentation are shown in Figures 9 and 10, respectively.

TEST PROCEDURE

Uniform inlet-flow was used for all tests. Vibratory stresses were measured with strain gages located at selected blades and vanes and were monitored and/or recorded by on-stand equipment. The test program was divided into two phases. During the first phase, which included baseline and corner-blow stator tests, the annular wall-suction slit upstream of the stator was sealed to prevent the baseline stator performance from being affected by recirculation in these slits. The second phase of the test program was conducted after this sealer material was removed. This was accomplished at the test stand by separating the rotor front-shaft assembly from the rear shaft to provide access to the suction slits.

PHASE I — BASELINE AND CORNER-BLOW STATOR TESTS

Corner-Blow Flow Optimization Tests

To determine the optimum corner-blow flow to be used for subsequent testing, overall and blade element performance data were taken at five points at design speed near peak efficiency. At each of these five data points, a different combination of the four sets of blowing nozzles were operated at choke flow. Choke flow through the forty-four hub nozzles at 18 and 48 percent chord-lengths was 0.22 lb/sec and 0.19 lb/sec, respectively. Choke flow through the tip nozzles at 18 and 48 percent chord-lengths was 0.21 lb/sec for each set of nozzles. The following nozzle combinations were tested:

- 1. all four nozzles operative
- 2. only the two hub nozzles operative
- 3. only the two tip nozzles operative
- 4. only the hub and tip nozzles at 18 percent of the vane chord-length operative
- 5. only the hub and tip nozzles at 48 percent of the vane chord-length operative.

Data were taken at another point without blowing flow to provide a baseline for comparing the effects of the different nozzle combinations. The compressor discharge throttle setting was identical for all six data points and only the number of operative nozzles was varied. Because of the small changes in performance seen with blowing, combination 1 (all four nozzles operative) was selected as the optimum combination for further testing.

Rotating-Stall Surveys

Rotating stall surveys were conducted at 50, 70, 90, and 100 percent of design speed. The surveys were conducted both without blowing flow and with optimum blowing flow. These surveys consisted of determining the point of initiation of rotating stall and the radial extent of the stall zones. As the discharge throttle was closed from wide open into stall, velocity fluctuations at the rotor inlet were measured and recorded simultaneously with the measurements from strain gages, a speed signal, and the measurements from a stator leading edge

static pressure probe. The strain gages were located on selected stators and rotors, and the velocity fluctuations were measured by means of three-sensor hot-film probes at 25, 50, and 80 percent span from the hub.

Overall and Blade Element Performance Tests

Twenty overall and blade element performance data points were taken without blowing flow and 20 with blowing flow. The points were taken over a range between wide-open throttle and stall at 50, 70, 90, and 100 percent of design speed. Stall flow was also measured for each of these percent speeds. Sixteen performance data points were taken with choked blowing flow through different combinations of nozzles. Five data points were taken at both 70 and 100 percent of design speed with the optimum flow rate; all four blowing nozzles were operative. At design speed, five points were also taken with one-half the optimum flow rate—choked blowing flow through two of the four nozzles (the hub and tip nozzles at only 48 percent of the vane chord-length). One additional near-stall point was taken with the hub and tip nozzles at only 18 percent of the vane chord-length operative. The data points taken without blowing flow were at identical compressor throttle settings. This was accomplished by first setting a particular operating condition without blowing, taking overall and blade-element performance data, and then successively repeating the data point after introducing blowing flow through the different nozzle combinations to be tested.

Boundary Layer Surveys

Boundary layer surveys were conducted at the stator inlet and exit for six data points at design speed. At three discharge throttle settings, data were taken first without blowing flow and then with choked blowing flow through all four nozzles. A boundary layer survey was also conducted at a near-surge point at 90 percent of design speed without blowing flow. These surveys consisted of radial and tangential traverses of total pressure, total temperature, static pressure, and airflow angle at 15 radial locations. Tangential traverse data were used to make contour plots of these parameters at the stator exit.

PHASE II — WALL-SUCTION AND COMBINED CORNER-BLOW WALL-SUCTION STATOR TESTS

Wall-Suction/Flow Optimization Tests

At the design speed and peak efficiency throttle setting, five data points were taken with different amounts of suction flow through the hub and tip annular slits to determine the optimum suction flow rate for further testing. Data points for the following conditions were obtained:

- 1. maximum suction flow through both the hub and tip slits
- 2. maximum suction flow through the hub slit only
- 3. maximum suction flow through the tip slit only

- 4. 75 percent of the maximum hub and 84 percent of the maximum tip suction flow rate
- 5. 65 percent of the maximum hub and 76 percent of the maximum tip suction flow rate

The maximum hub suction flow rate achieved was 1.71 lb/sec as compared to a design flow rate of 2.02 lb/sec. Design hub suction flow rate was not achieved because of high losses in the piping system used to remove the hub suction flow. The maximum tip suction flow rate achieved was 2.67 lb/sec as compared to a design flow rate of 2.66 lb/sec. Maximum flow through the hub and tip annular slits was selected as the optimum flow rate for further testing.

Rotating Stall Surveys

Rotating stall surveys were conducted at 50, 70, 90, and 100 percent of design speed with the optimum wall-suction and with combined optimum corner-blowing and optimum wall-suction flow. These surveys were conducted in the same manner as for the baseline and corner-blowing stator tests.

Overall and Blade-Element Performance Tests

Eight overall and blade-element performance data points were taken at 70 and 100 percent of design speed with both optimum wall-suction flow and combined optimum wall-suction and corner-blowing (a total of sixteen data points). For each boundary layer treatment, five of the data points were taken at 70 percent of design speed, but only three data points were taken at design speed because the program was abbreviated due to test facility difficulties. As in the baseline and corner-blow stator tests, speed and throttle settings were made with suction only and then data points were taken with and without blowing flow.

Boundary Layer Survey

Boundary layer surveys were conducted at three throttle-settings at design speed with wall-suction and then with combined wall-suction and corner-blowing (a total of six data points). The surveys were conducted at approximately the same operating conditions as the boundary layer surveys with the baseline and corner-blow stators so that the stator exit contours could be compared for all four stators.

CALCULATION PROCEDURES

Raw data measurements from all probes were converted to engineering units, aerodynamically corrected, and mass averaged in the same manner as discussed in reference 1 for uniform inlet flow. Blade element and overall performance parameters were calculated similar to reference 1 but with corrections made to account for flow added or extracted between the rotor inlet and stator exit. The corrections made are explained below.

The flow-field analysis computer program of reference 1 was used with modified input procedures to simulate the physical processes of blowing and wall suction. Each data point with

blowing and without blowing (baseline) was taken at the same throttle setting. Each data point with blowing and wall-suction combined and wall-suction alone was also taken at the same throttle setting. The input to the flow-field program for blowing included measured distributions of rotor total pressure ratio and temperature ratio from the baseline point and with radial distributions of stator exit pressure, air angle, and wake blockage factors from blowing point measurements. For the combined blowing and suction points, the flow-field program input used radial distributions of rotor total pressure ratio and total temperature ratio from the suction-alone point with stator exit pressure, air angle, and wake blockages as measured with combined blowing and suction.

All points with suction had stator leading and trailing edge blockage factors reduced so that the streamline calculation used the correct effective flow area to obtain velocity distributions at these locations.

The computer program used to calculate overall system efficiency and pressure ratio was separate from the computer program used to calculate stator recovery. System efficiency was defined as ideal-work/actual-work in the conventional manner but accounted for blowing and suction flows. Ideal work is the net isentropic work required to bring all constituent flows reaching the stator exit to the mass-averaged stator exit pressure. This ideal work accounts for high-pressure blowing from an outside source. The actual-work calculation included rotor work done on the flow that reaches the stator exit and rotor work on the suction flow extracted at the stator inlet. It did not include the work done by the facility exhausters or blowers. System performance was calculated for each configuration tested using equations derived in Appendix B. Calculations for the corner blow and combined blowingsuction configuration included overall pressure ratio and stator recovery corrections due to the mixing of high-pressure blowing air with mainstream air. The wall-suction overall rotor and stage pressure ratios and stator recovery are the radially mass-averaged values calculated by the flow-field program as was done for baseline performance. A detailed description of the overall performance calculation for each configuration is provided in Appendix B. Adjusted efficiency, pressure ratio, and stator recovery are tabulated for each data point in Appendix C.

For the boundary layer survey points, overall performance and blade element calculations were made using the wake rake data, and contour plots of P, p, β , and T were generated from combination-probe measurements. Velocities were calculated from measurements of total and static pressure, total temperature, and air angle as described in reference 2.

RESULTS AND DISCUSSION

The results of the baseline, corner-blow, annular slit suction, and combined corner-blow and annular slit suction stator tests are discussed under the headings "Shakedown Test" and "Performance Test". The shakedown results include some brief observations of vibratory stress levels and rotating stall phenomena which occurred during the surge cycle. Also included are the results of the flow optimization test for the corner-blow stator.

Overall performance for rotor and stage is presented for the baseline (no endwall treatment), corner-blow, annular slit suction, and combined corner-blow and annular slit suction stator

tests. Rotor blade elements plots are presented for the baseline stator test only. Stator blade elements plots are presented for the baseline, corner-blow, annular slit suction, and combined corner-blow and annular slit suction stator tests. Gapwise distributions of stator exit total pressures are presented for the baseline, corner-blow, annular slit suction, and combined corner-blow and annular slit suction stator test for the near-surge and near-choke conditions at 70 and 100 percent design speed. Contour plots of stator exit traverse data are presented for three weight flows at 70 and 100 percent design speed for the baseline, corner-blow, annular slit suction, and combined corner-blow and slit suction.

SHAKEDOWN TEST

Levels of vibratory stresses on the blades and vanes were recorded during accelerations and decelerations between 50 and 105 percent of design speed with wide-open throttle and near-stall throttle settings. All observed blade and vane vibratory stress levels were within acceptable limits.

At all speeds, minimum flow was determined by compressor surge for both the baseline and for all boundary layer control combinations. This was determined from continuous recordings of signals from a three-sensor, hot-film probe at the rotor inlet, from strain gages, and from static pressure probes located along the flow-path walls. At high speeds these measurements showed large fluctuations in velocity simultaneous with high vibratory stresses in rotor and stator blades and static pressure variations. Periodic fluctuations in velocity indicated that rotating stall occurred at the beginning of the surge cycle.

Optimization tests were conducted at 100 percent design speed to determine the most favorable locations and rates of blowing and suction. Figure 11 presents stator wake rake data at a part-throttle flow for the near-wall locations of 5 and 90 percent of span from the hub. Vane wakes at these span locations indicated that most of the benefit of blowing was being achieved with the 48 percent chord nozzles and that the tip was being benefitted more than the hub. However, due to the small magnitude of the changes observed and the small amount of flow required to choke each nozzle, it was decided that the test program would be conducted with all blowing nozzles and suction slits active.

PERFORMANCE TEST

Overall Performance

Overall baseline rotor and stage performance is presented in Figures 12 and 13. Stage performance with and without selected rates of suction and/or blowing is presented in Figure 14. The stall line in each case was established by extrapolating the characteristic speed-lines to measured stall airflows, shown as slashed symbols on the figures. Peak baseline rotor efficiency was 86.7 percent at design speed and 87.0 percent at 70 percent speed.

Stage performance for baseline and maximum blowing revealed no changes in the pressure ratio, airflow characteristic at 70 and 100 percent design speed. Local changes in stator performance near endwalls were too small to affect overall performance. The same observation could be made for the configuration with suction and combined suction and blowing. Both uncorrected and corrected efficiencies are presented in Figure 14. For blowing, the efficiency

correction, which accounts for the addition of high energy air behind the rotor, reduced the peak stage efficiency by a 0.5 percentage point at design speed and by 1.3 percentage points at 70 percent design speed. With suction, the efficiency correction, reflecting the rotor work done on the bleed flow, reduced peak stage efficiency by 2.5 percentage points at design speed and by 3.5 percentage points at 70 percent design speed. The efficiency corrections with combined blowing and suction were consistent with corrections for blowing alone and suction alone. In general, differences in pressure ratios between the baseline stator and the stator with blowing or suction were small.

Blade Element Performance

Figure 15 presents blade element total pressure loss coefficient, diffusion factor, and deviation versus incident angle for the baseline rotor. Figures 16 through 19 present stator blade element data with and without blowing, with suction, and with combined blowing and suction.

Some caution should be observed in interpreting the blade element loss and loading data since the calculation procedure satisfied continuity accounting for mass addition or removal between axial stations, but losses were calculated based on the differences between peak total pressure and mass flow averaged total pressure from stator exit rake wake measurements. With a jet of high-pressure blowing air at one gapwise location, the peak pressure may not represent a true average, stable-inlet pressure. Also, the effects on streamline of adding or subtracting flow at particular locations were not accounted for. A tabulation of the data is given in Appendix C.

Stator Wake Rake Total Pressure Profiles

Gapwise distributions of stator-exit total pressure are presented in Figures 20 through 27 at 70 and 100 percent design speed for the near-surge and wide-open throttle positions. Figures 20 to 23 show a comparison of stator wake profiles with and without blowing. Similarly, Figures 24 to 27 show a comparison of suction with combined suction and blowing. The largest change in wake profile due to blowing was found to occur at 70 percent design speed for the wide-open throttle point. This was also true for the effect of stator hub-slit suction discussed in reference 2, which achieved significant improvements in stator hub wake profiles. A plot of the integrated difference in stator wake total pressure with and without blowing is presented in Figure 28. The improvement at each span location at 70 percent design speed and wide open throttle is shown. Also shown on the graph is the product of the total nozzle area and the difference between the nozzle total pressure and stator baseline exit average total pressure. The resulting parameter reflects the effect of mixing with the free-stream air and, in a sense, is proportional to the minimum total pressure change to be expected at stator exit due to blowing. Figure 28 indicates that jet mixing had affected a region out to 5 percent span from the hub and from 85 to 95 percent span at the tip. Reductions in stator loss were approximately equal to the pressure rise obtained by simple mixing of the nozzle and free-stream flow. However, the greater part of the reduction of stator loss was achieved using only the 48 percent chord corner nozzle, as shown during the optimization tests.

A comparison of baseline stator wakes with those having suction (Figure 20 versus 24 and Figure 22 versus 26) reveals only small differences at both 70 and 100 percent design for the near-surge flow. As these points were not run back-to-back, some differences in wake peak

pressure ratio are evident. However, the peak-to-valley wake pressure difference at hub and tip was slightly smaller for the case with suction as compared to baseline indicating improved exit total pressures near the walls. Examination of the wide open flow (Figure 21 versus 25 and Figure 23 versus 27) for both speeds indicates that the situation had been altered, and the difference in stator wake peak-to-valley pressure was now greater at the 5 and 95 percent span locations for the case having suction compared to baseline, indicating an increase in wake depth with suction.

Contour Plots of Stator Exit Traverse Data

Circumferential traverses were made at the stator exit for part-throttle, maximum efficiency, and near-stall points at 100 and 70 percent design speed, for the baseline, blowing, suction, and combined suction and blowing configurations. Measurements of total and static pressure, total temperature, and absolute air-angle were obtained at 3.8, 4.9, 5.9, 8.4, 11.0, 15.4, 31.0, 51.2, 72.7, 87.8, 92.8, 94.1, 95.3, 96.6, and 97.4 percent passage height from the hub. Tangential spacing gave 15 readings across a stator gap at 90 percent span and 11 readings at 4.3 percent span. These measurements were used to calculate velocity vectors and to construct contour plots showing patterns of P/P_{INLET} , T/T_{INLET} , airflow angle, and $Vm\sqrt{\theta_T}$ at the stator exit instrumentation plane. These contours are shown in Figures 29 through 48.

Comparison of stator exit plane total pressure plots shown on Figures 29 (for design speed) and 44 (for 90 percent design speed) reveals no significant differences between the baseline stator and the stator with blowing, suction, or combined blowing and suction. These results are more easily seen on the stator wake profiles discussed previously.

Rapid Response Hot-Film Data

Some indication of post-surge behavior of this stage may be gained by examining the traces of hot-film probes positioned approximately 2.2 inches upstream of the rotor at 25, 50, and 85 percent span. Traces from these probes are shown on Figure 49 for the 100 percent design speed. For the baseline, the surge pulse reaches the measurement plane uniformly at root, mean, and tip. Pulse duration was not constant over the span but indicates that the hub recovered first and was followed by the mean and tip sections. Overall pulse duration was 0.014 second.

The traces obtained during surge with blowing indicate no significant change in the surge pulse. However, a significant change in the surge pulse can be seen for the test with suction. As before, the pulse reaches the measurement plane uniformly at root, mean, and tip. The magnitude of the perturbation, however, was dramatically reduced at the hub. The length of the surge pulse was approximately 0.013 second.

For combined blowing and suction, there was no significant change in post-surge behavior compared to suction only. Evidently annular suction had changed the characteristic of the stage in the deep-stall mode, resulting in a reduction in pulse severity and radial extent.

It should be noted that the hub suction slot was much closer to the rotor trailing edge than was the tip suction slot. This would make the hub slot more effective in changing rotor char-

acteristics than the tip slot. As indicated in reference 2, the high speed surge is believed to be controlled by the rotor. The presence of an essentially choked suction slot near the rotor hub can be expected to significantly change the aerodynamic flow path of the rotor at the very low flows encountered during a surge pulse.

SUMMARY REMARKS

The use of stator corner-blow and annular slit suction ahead of the stator leading edge and combined corner-blowing and annular slit suction, did not produce any significant changes in the unstall or presurge performance of the stage. All of these endwall treatments showed some improvement in stator recovery in the regions of 5 percent span and 85 to 95 percent span from the hub. These local improvements in stator recovery were not enough to produce significant improvements in overall stator recovery.

The subject endwall treatments showed no improvements in stator range. Examination of stator performance at the near-surge point for the baseline (no blowing or suction) indicates that this stator was performing reasonably well without endwall treatment in spite of the fact that the stator had been restaggered four degrees open (4 degree increase in incidence angle).

Hot-film data indicated a reduction in the severity of the surge pulse for the stage when suction was applied behind the stalling rotor.

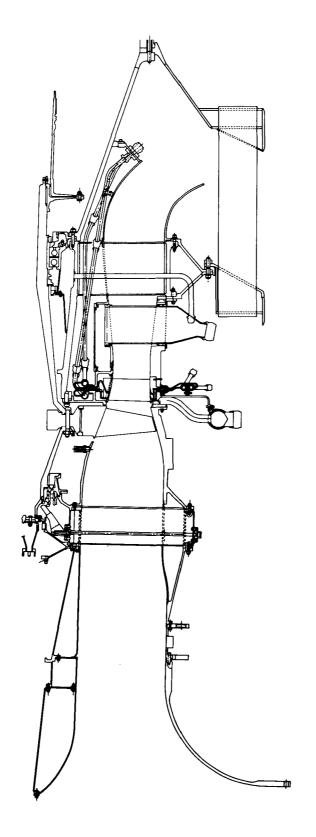


Figure 1 Cross Section of Test Compressor

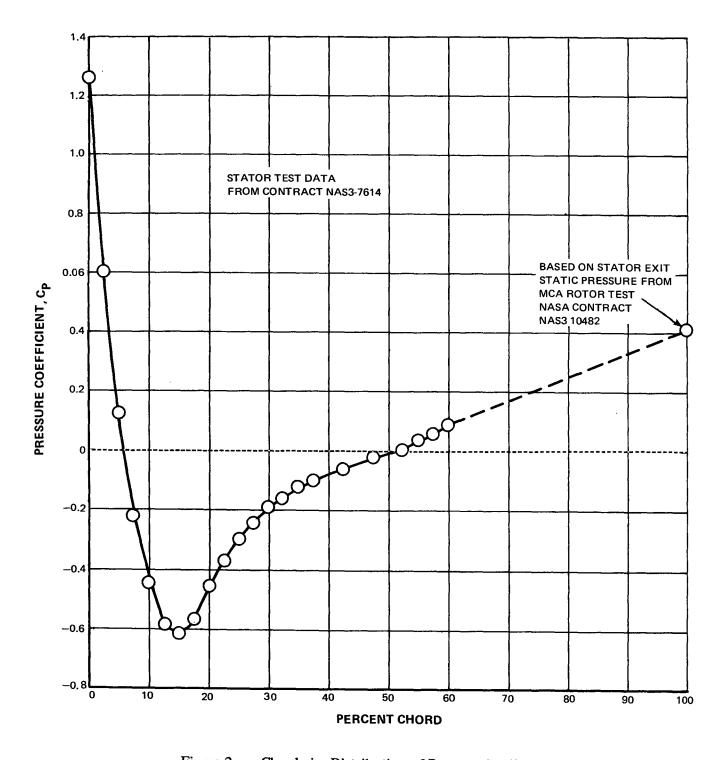


Figure 2 Chordwise Distribution of Pressure Coefficient

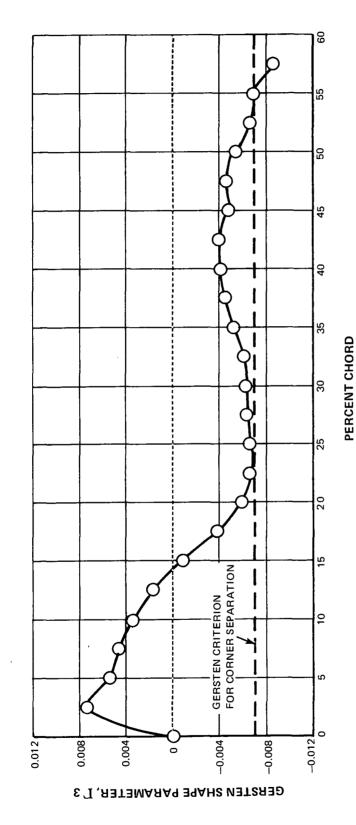


Figure 3 Chordwise Distribution of Gersten Shape Parameter

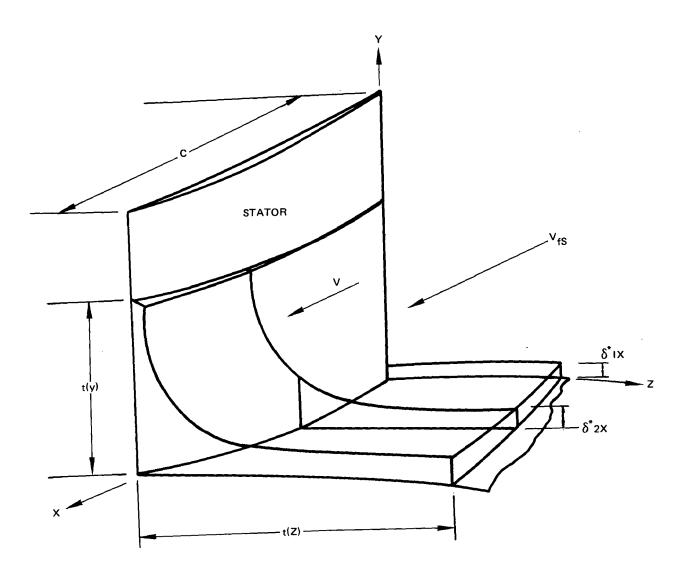


Figure 4 Three Dimensional Corner Boundary Layer

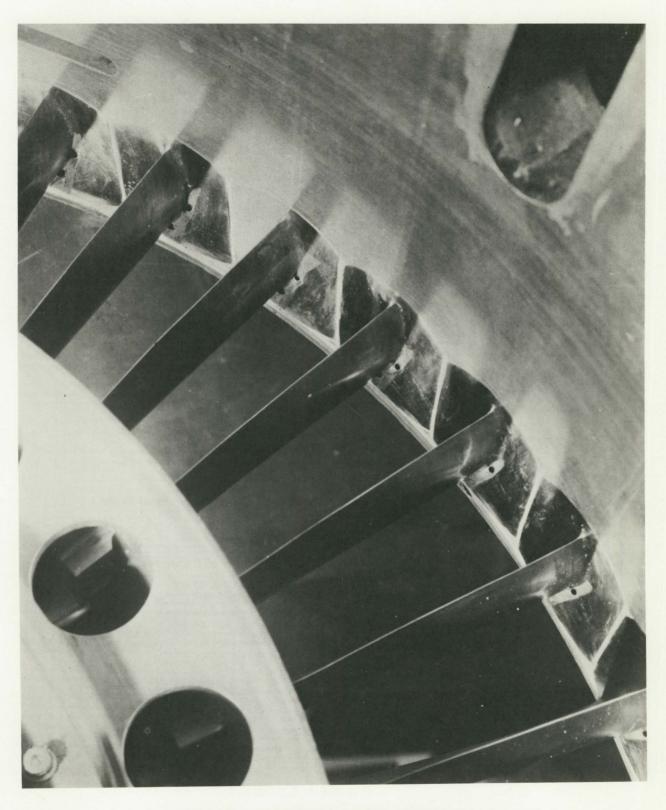


Figure 5 Stator Blow Configuration

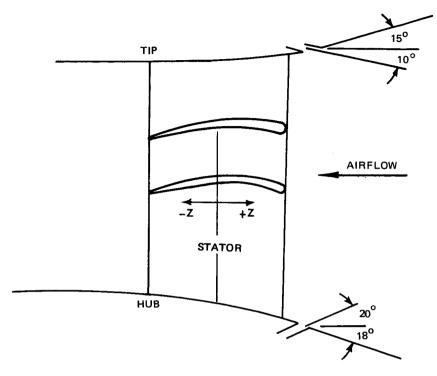


Figure 6 Wall-Suction-Slit Configuration

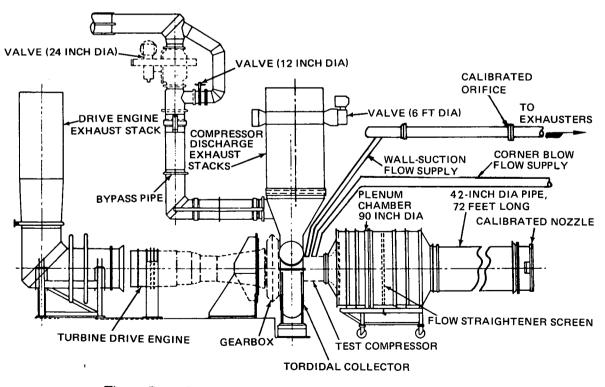


Figure 7 Schematic of Compressor Test Facility

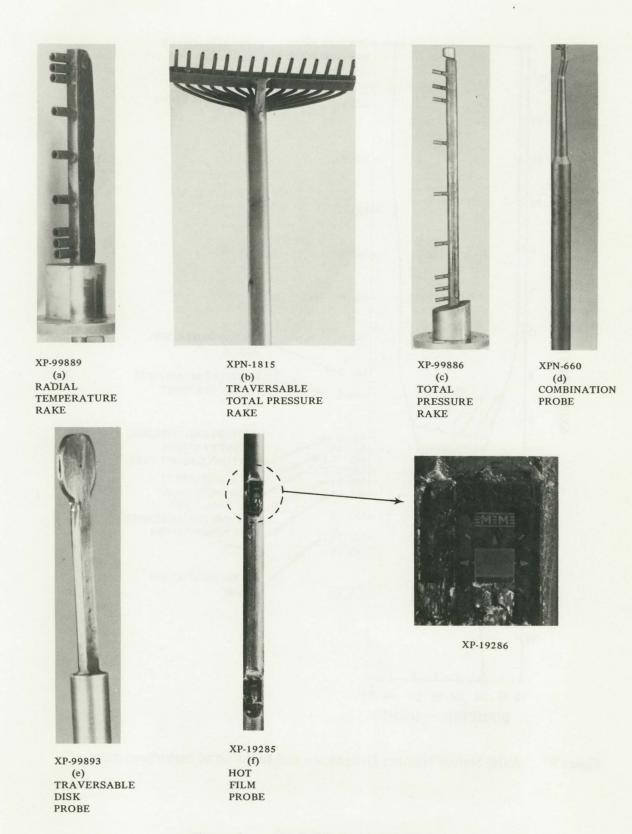


Figure 8 Typical Instrumentation

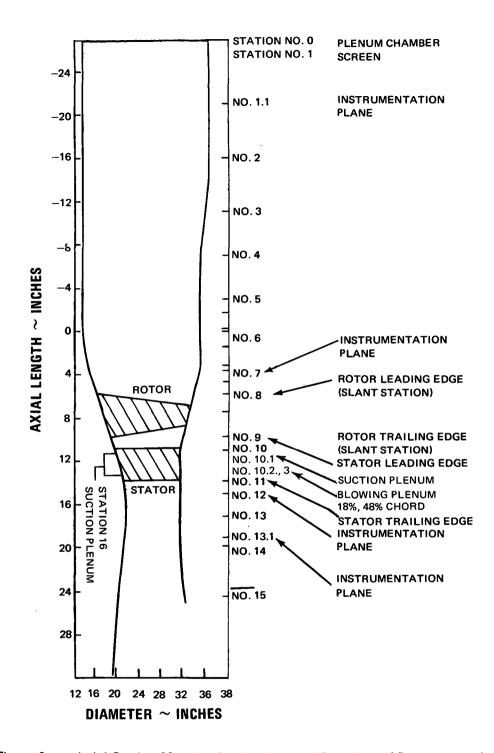


Figure 9 Axial Station Number Designation and Location of Instrumentation

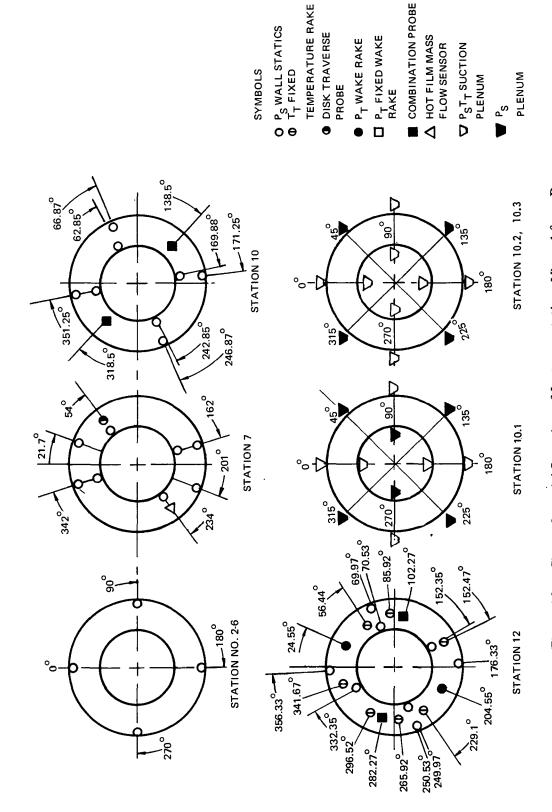


Figure 10 Circumferential Location of Instrumentation, Viewed from Rear

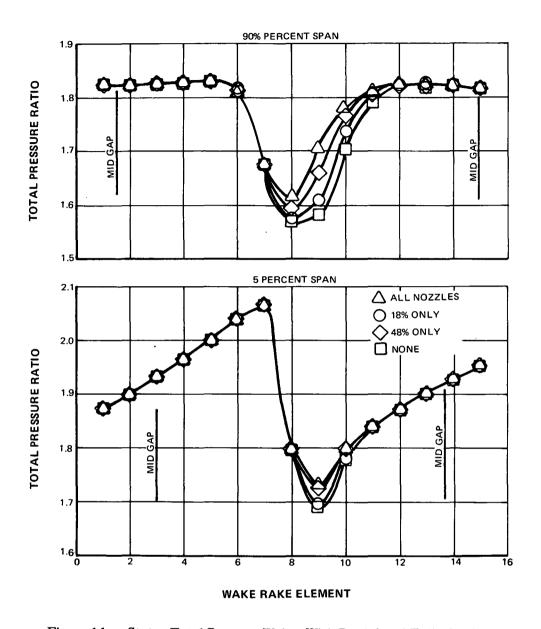


Figure 11 Stator Total Pressure Wakes With Partial and Full Blowing

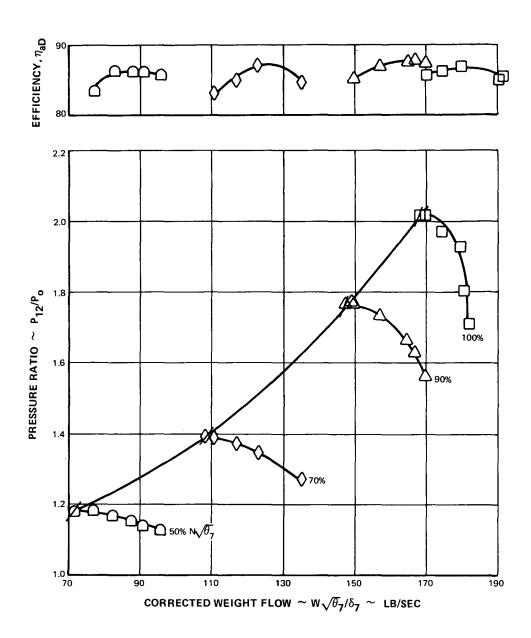


Figure 12 Rotor Overall Performance

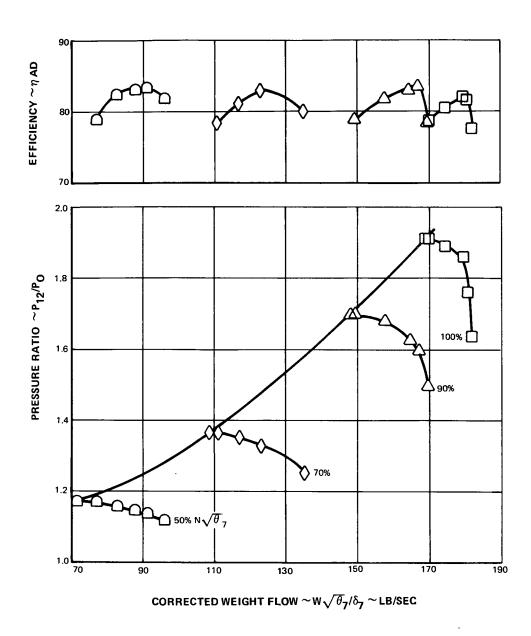


Figure 13 Stage Overall Performance - Baseline

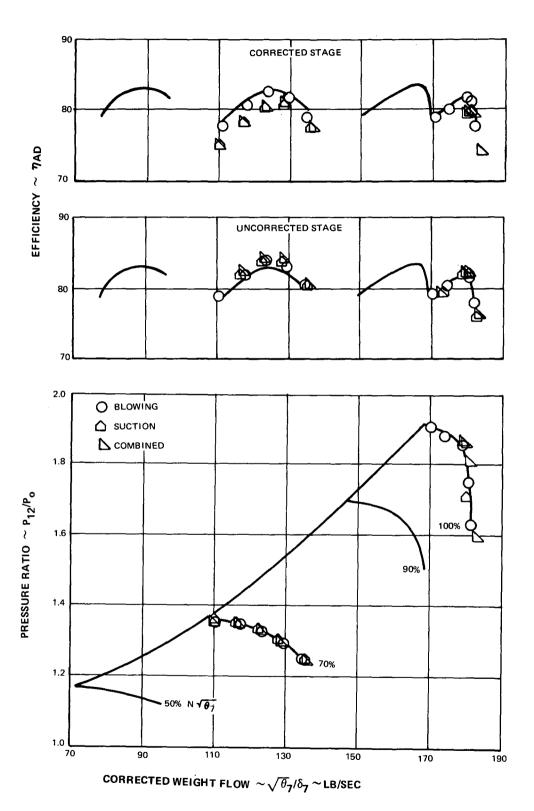
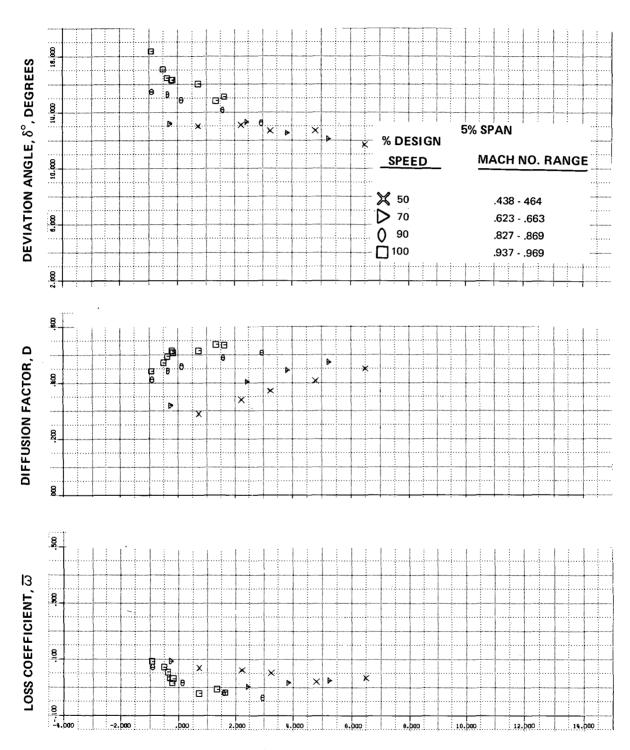


Figure 14 Stage Overall Performance - Blowing, Suction, Combined Blowing and Suction



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INCIDENCE ANGLE, SUCTION SURFACE, $\mathbf{I}_{\mathbf{S}}$, DEGREES

Figure 15a Blade Element Data - Rotor

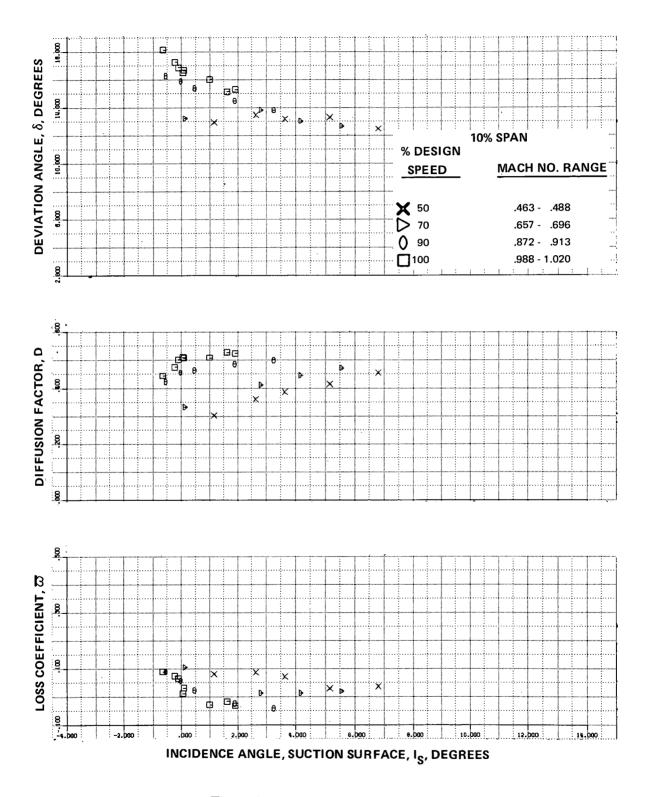


Figure 15b Blade Element Data - Rotor

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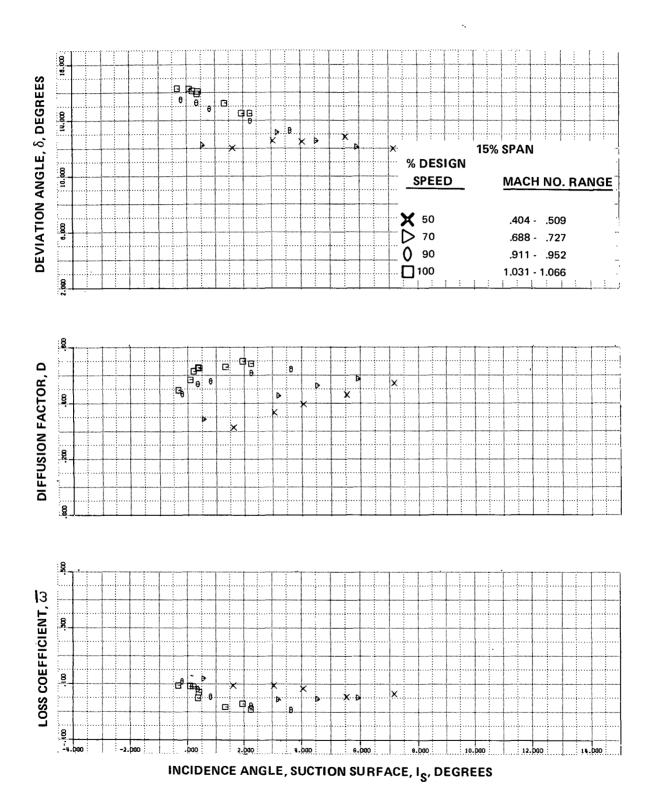


Figure 15c Blade Element Data - Rotor

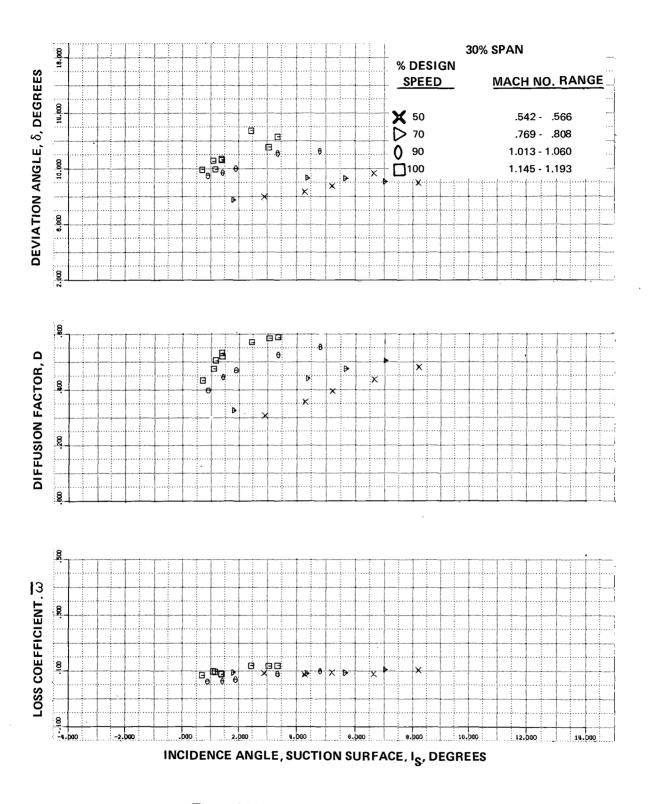


Figure 15d Blade Element Data - Rotor

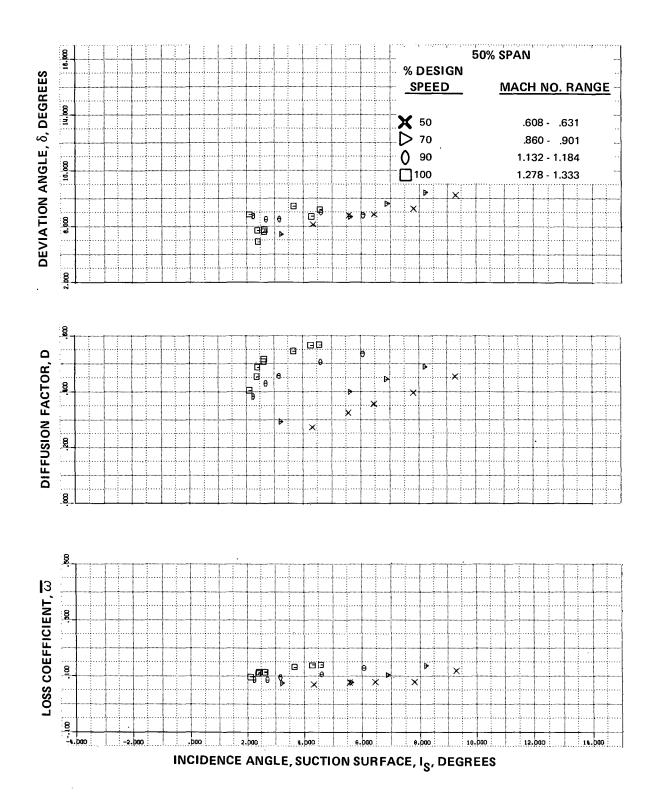


Figure 15e Blade Element Data - Rotor

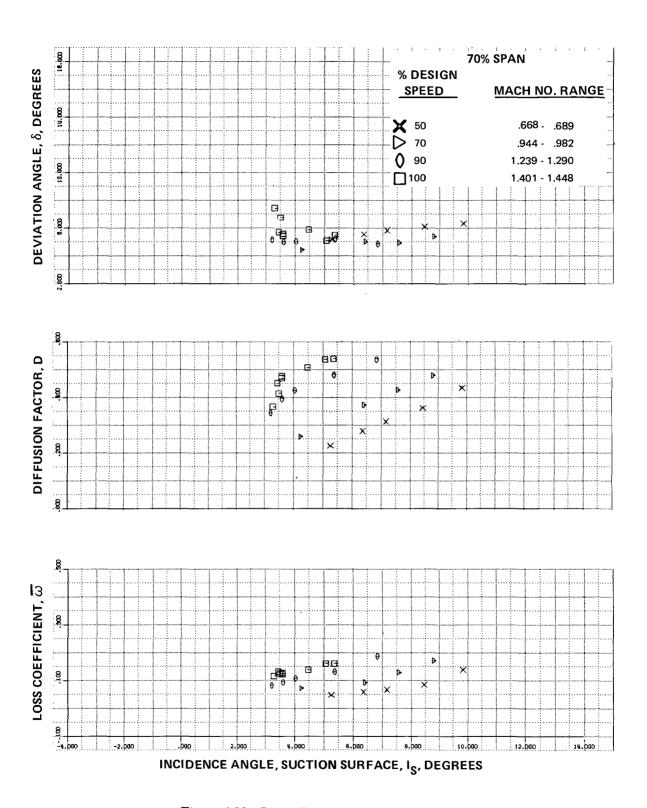


Figure 15f Blade Element Data - Rotor

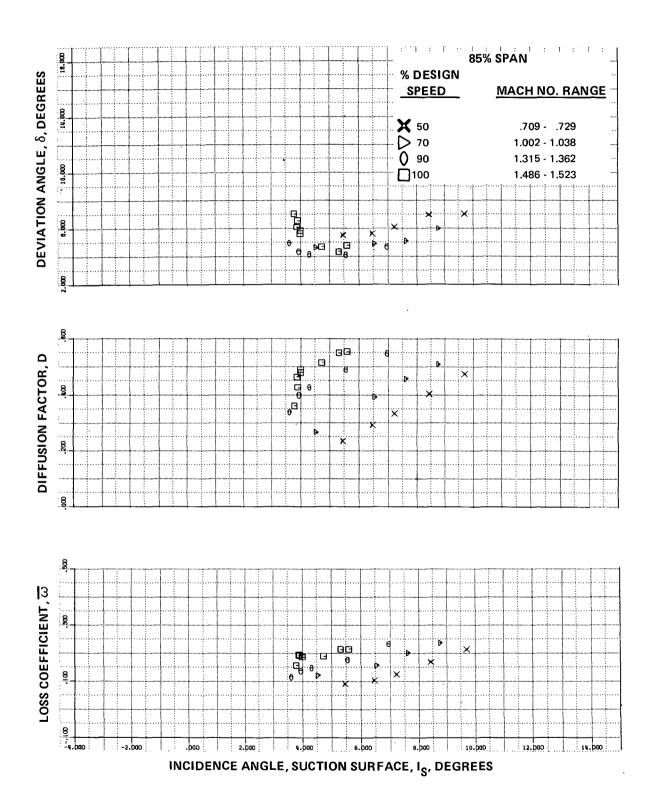


Figure 15g Blade Element Data - Rotor

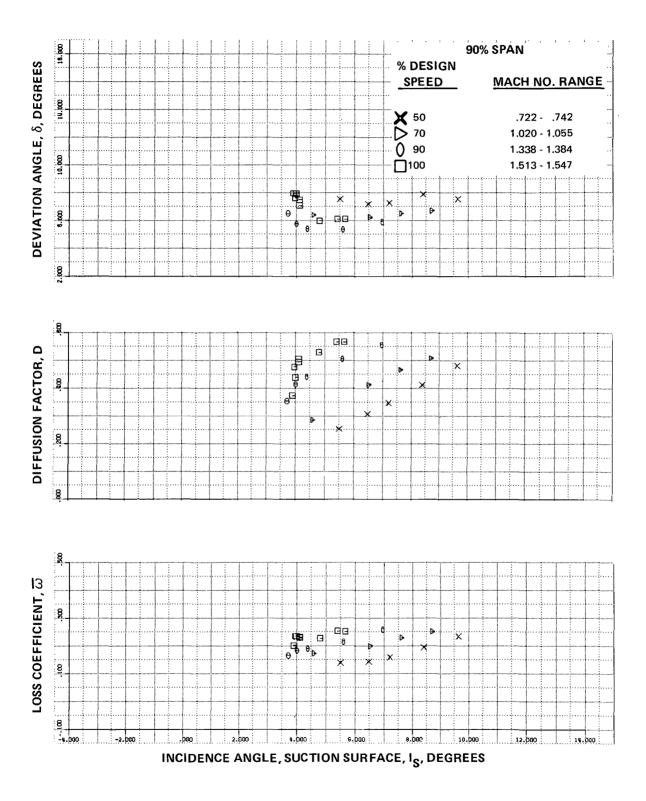


Figure 15h Blade Element Data - Rotor

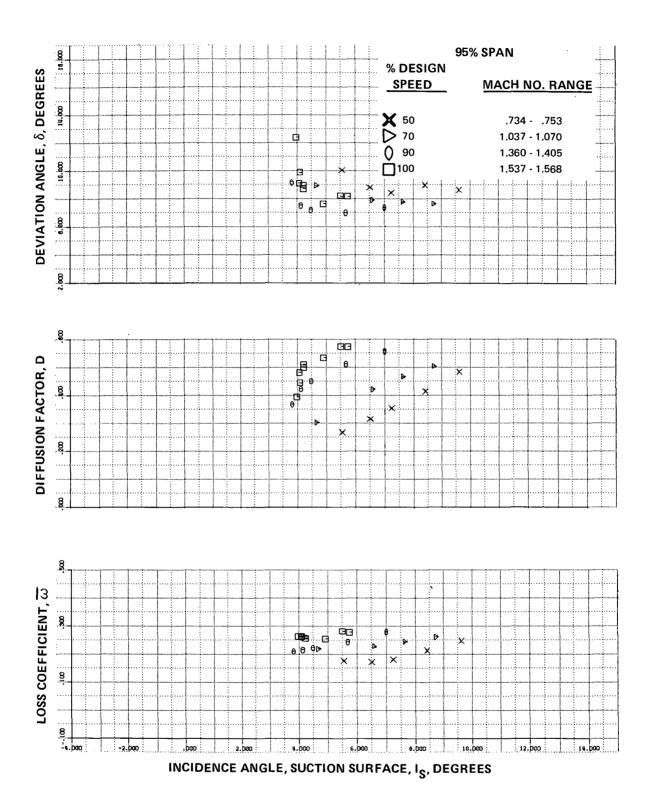


Figure 15i Blade Element Data - Rotor

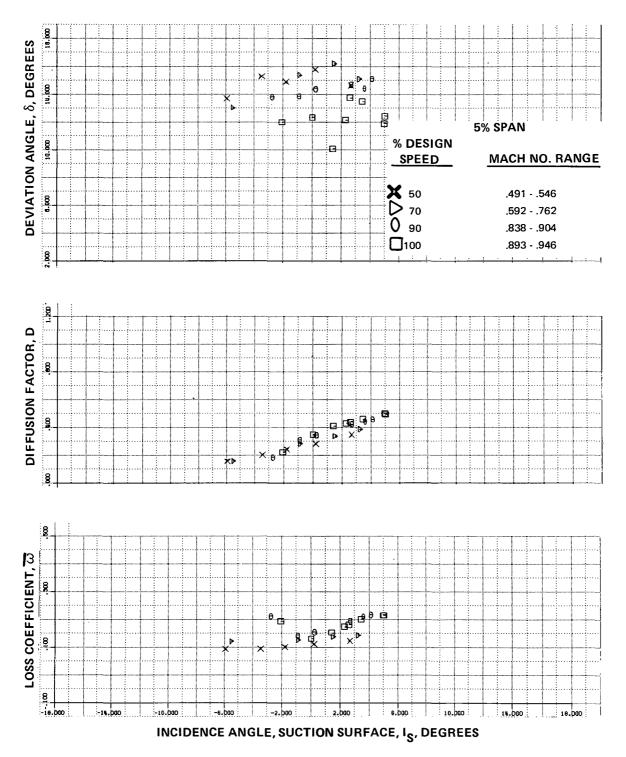


Figure 16a Blade Element Data - Baseline Stator

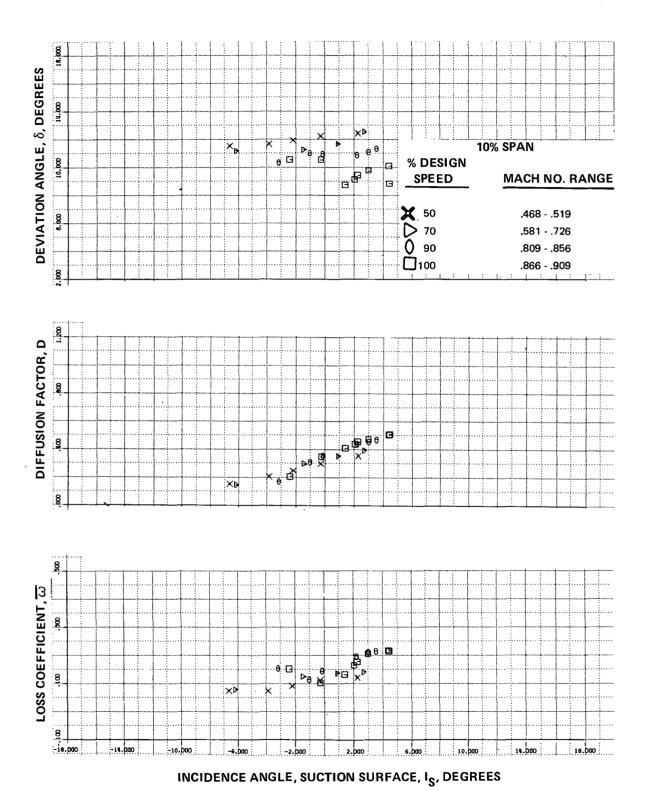
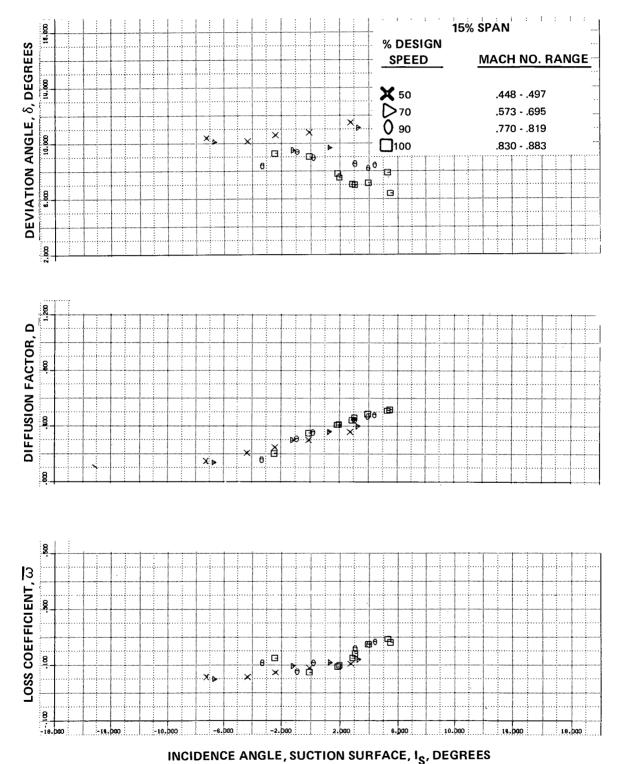
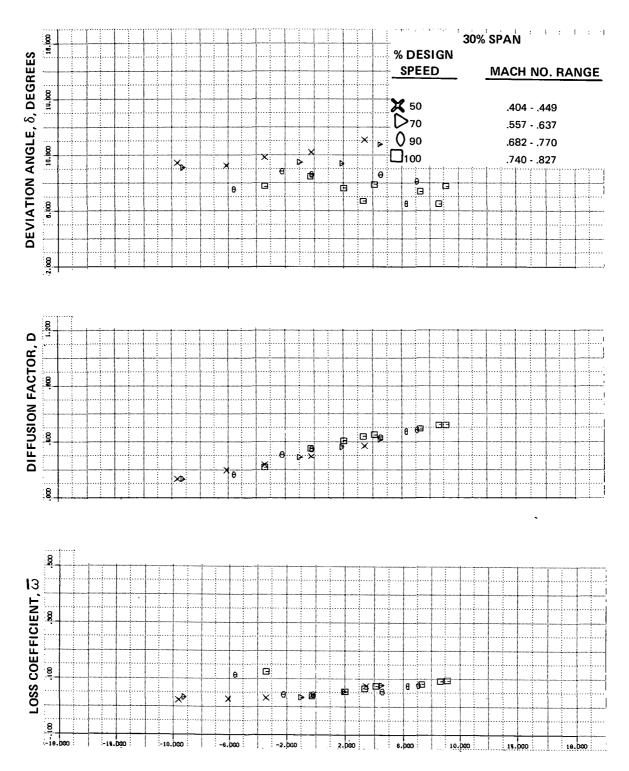


Figure 16b Blade Element Data - Baseline Stator



INCIDENCE ANGLE, SOCTION SORFACE, 18, DEGREES

Figure 16c Blade Element Data - Baseline Stator



INCIDENCE ANGLE, SUCTION SURFACE, I_S , DEGREES

Figure 16d Blade Element Data - Baseline Stator

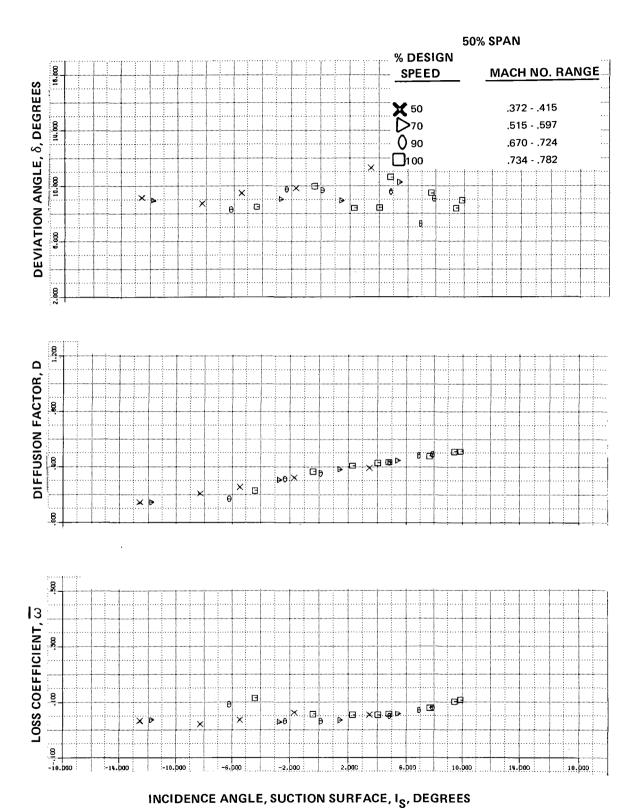


Figure 16e Blade Element Data - Baseline Stator

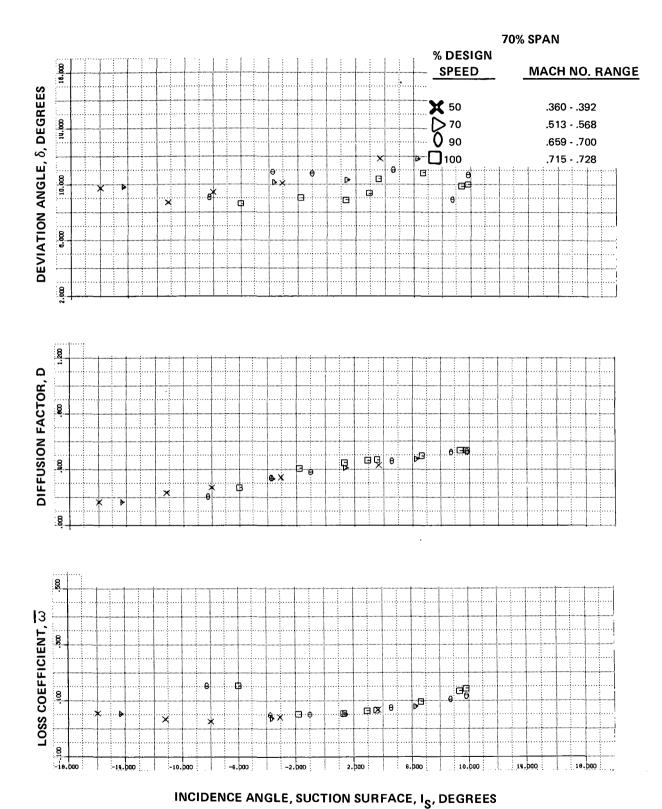
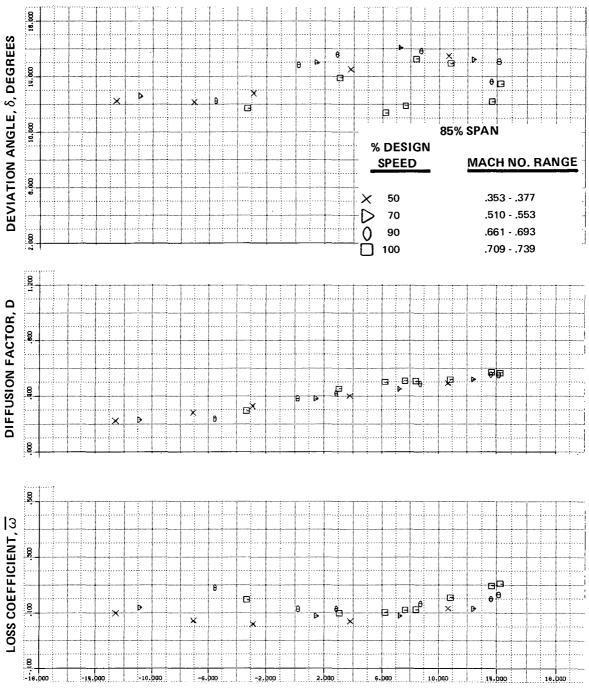
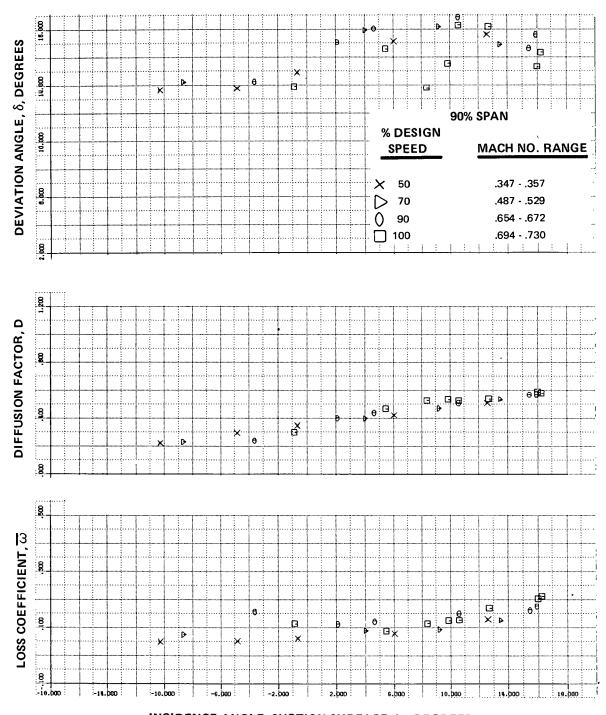


Figure 16f Blade Element Data - Baseline Stator



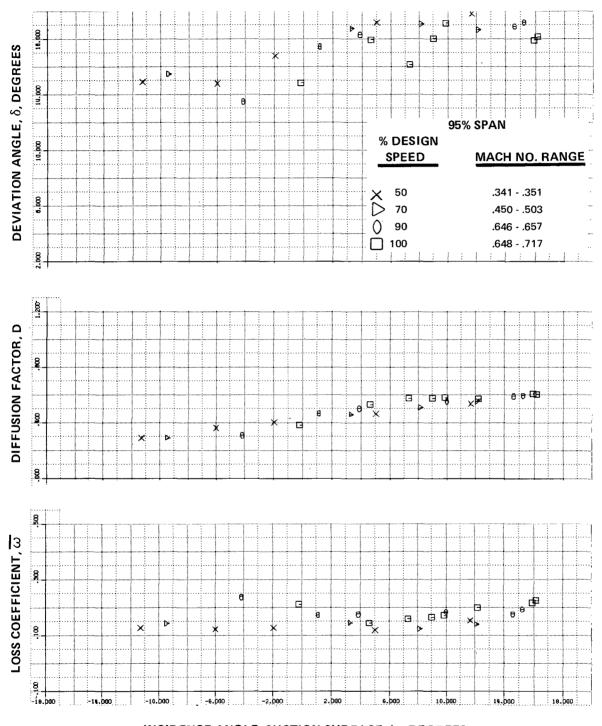
INCIDENCE ANGLE, SUCTION SURFACE, I_S , DEGREES

Figure 16g Blade Element Data - Baseline Stator



INCIDENCE ANGLE, SUCTION SURFACE, I_S , DEGREES

Figure 16h Blade Element Data - Baseline Stator



INCIDENCE ANGLE, SUCTION SURFACE, I_S , DEGREES

Figure 16i Blade Element Data - Baseline Stator

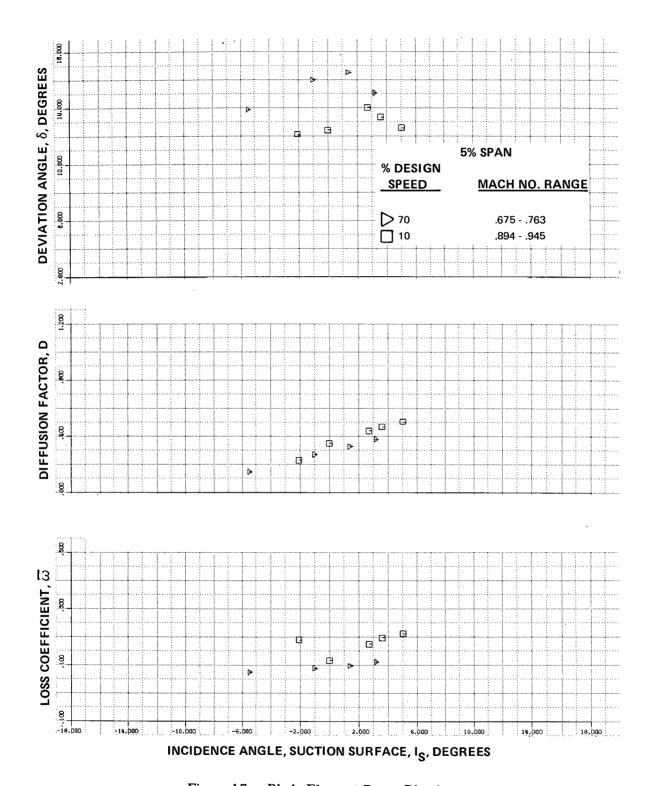


Figure 17a Blade Element Data - Blowing

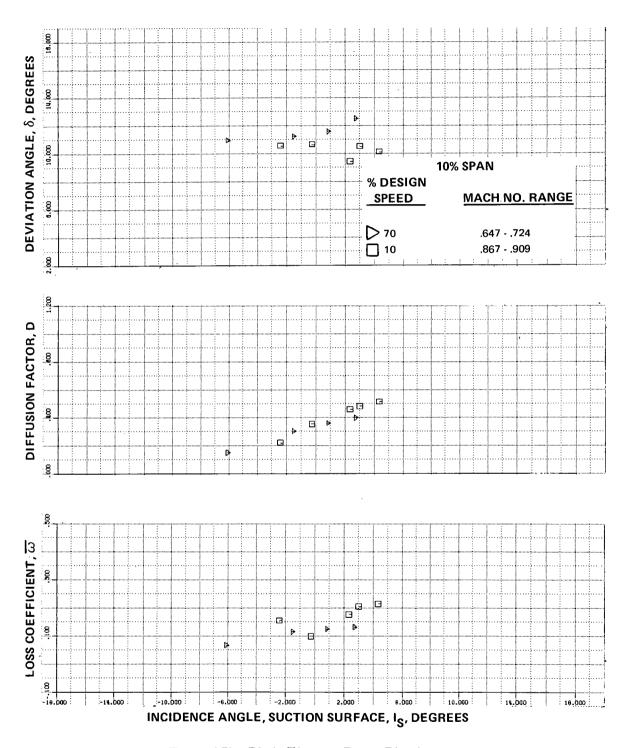


Figure 17b Blade Element Data - Blowing

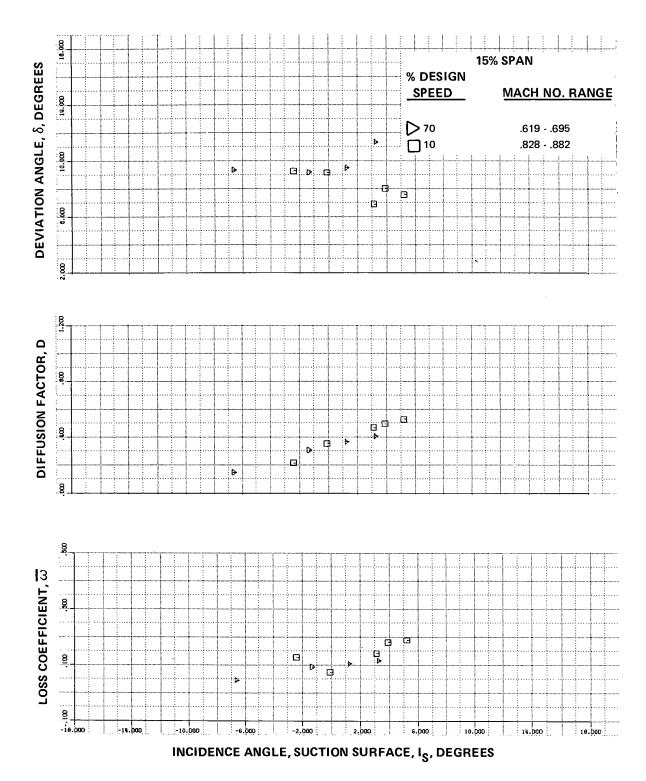


Figure 17c Blade Element Data - Blowing

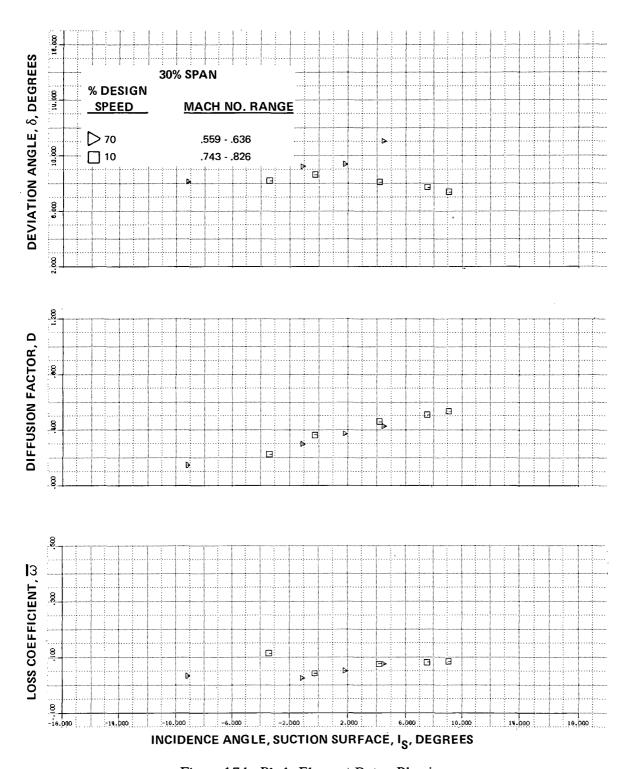


Figure 17d Blade Element Data - Blowing

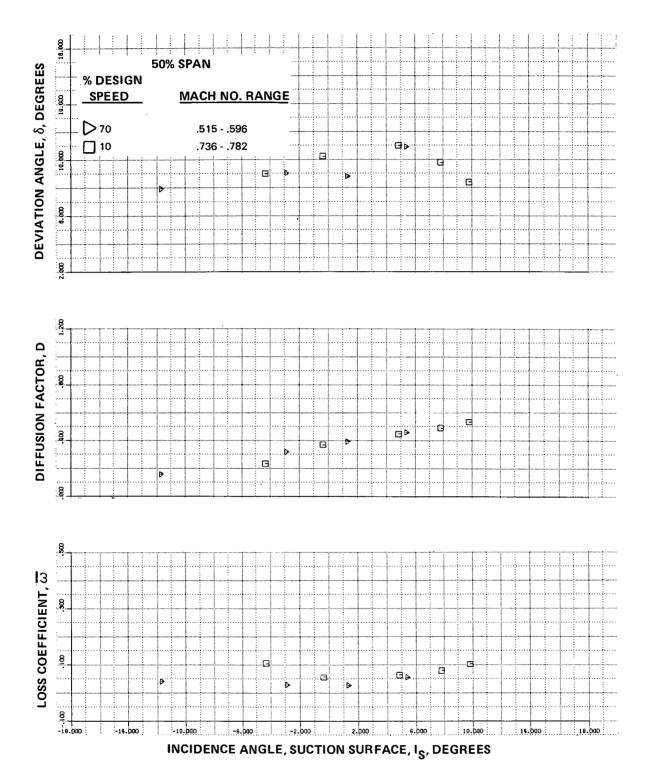


Figure 17e Blade Element Data - Blowing

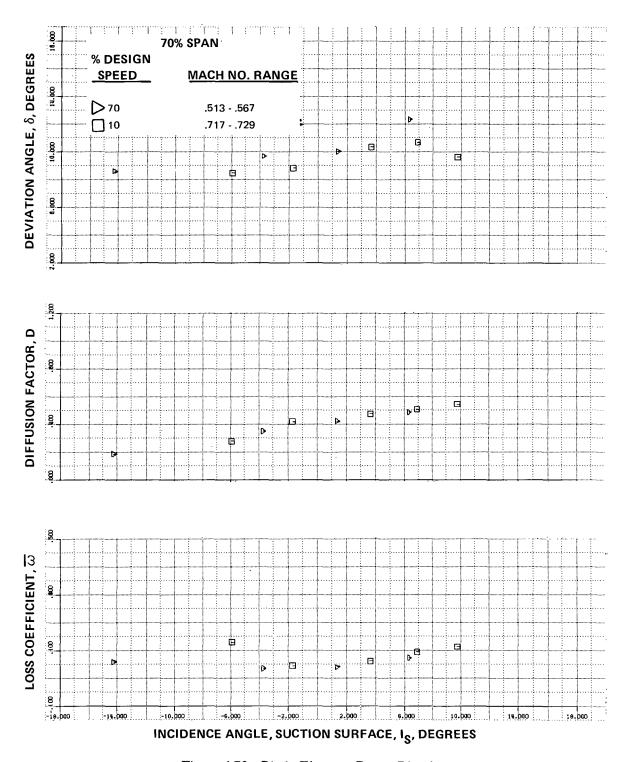


Figure 17f Blade Element Data - Blowing

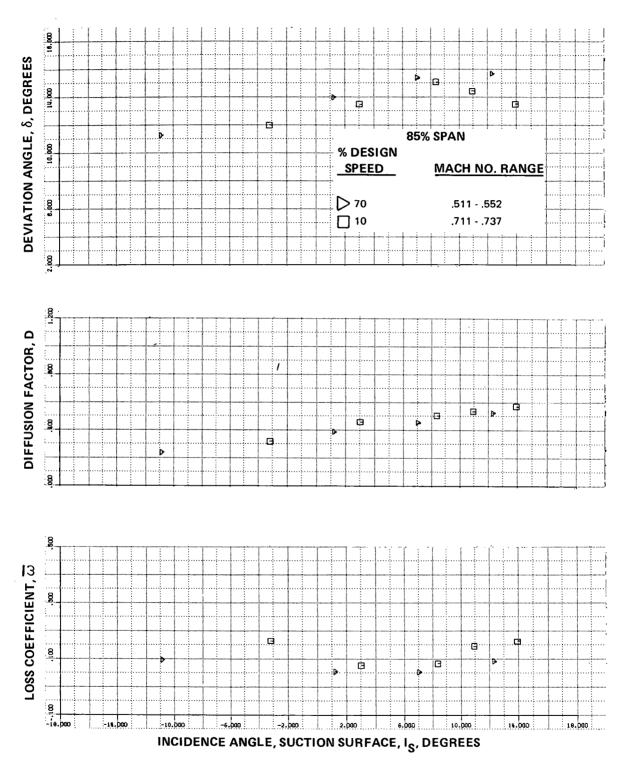


Figure 17g Blade Element Data - Blowing

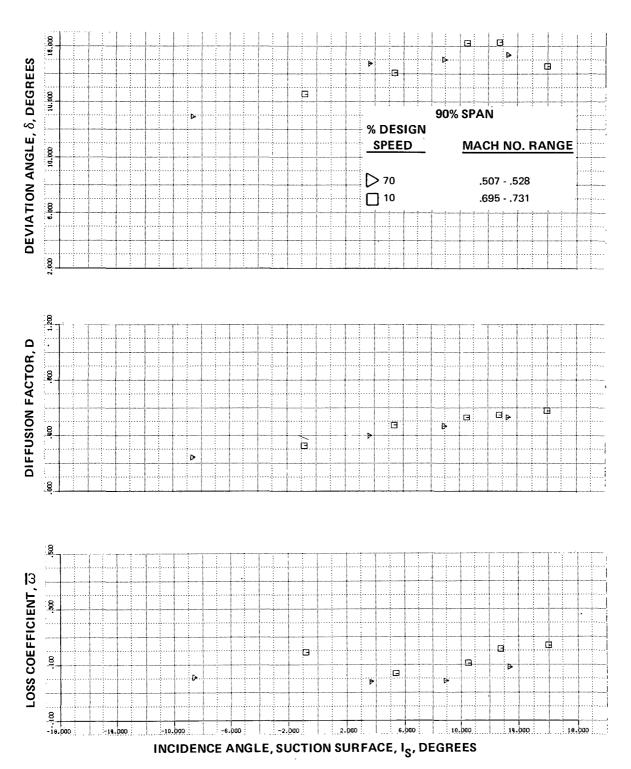


Figure 17h Blade Element Data - Blowing



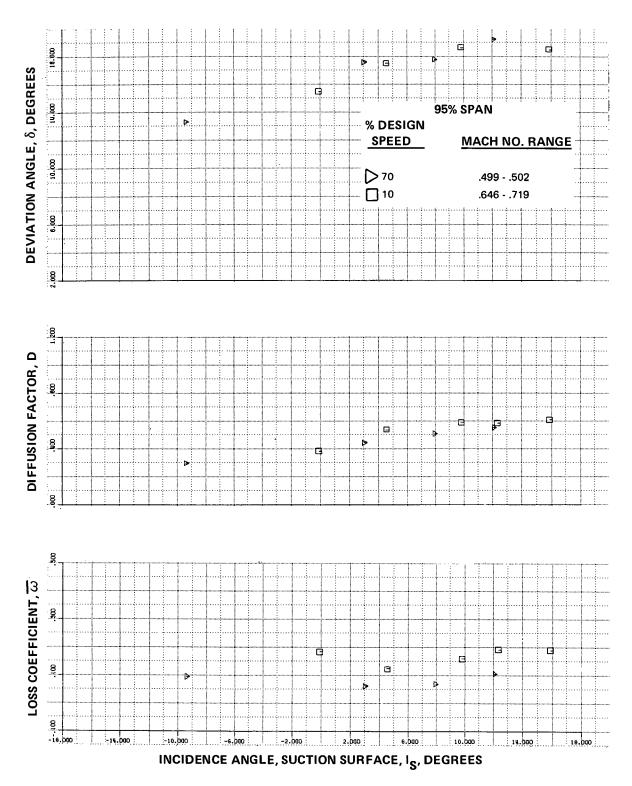
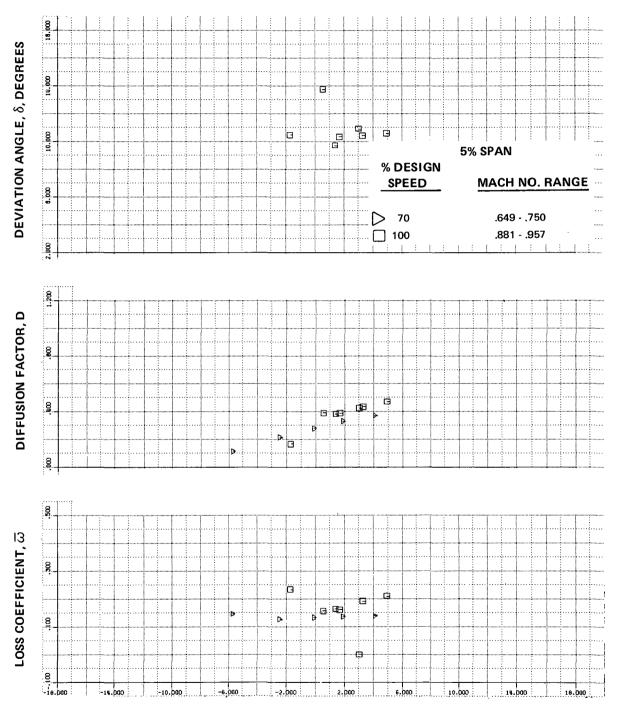
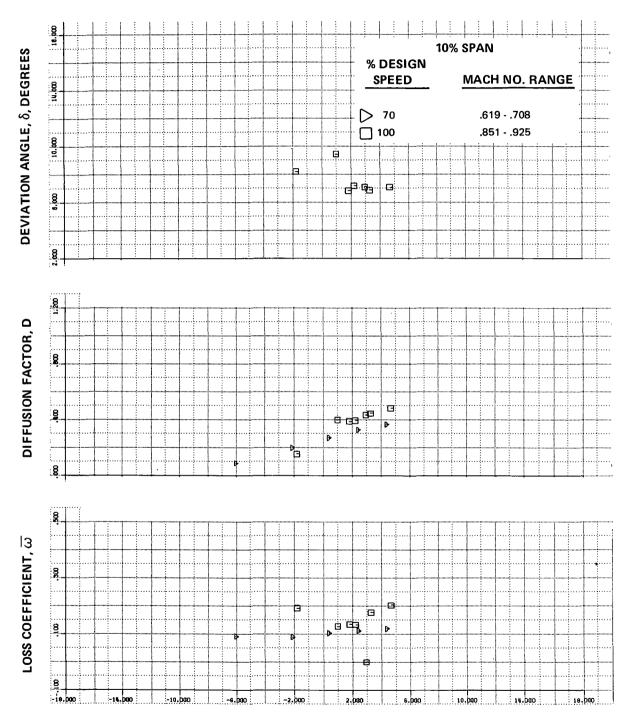


Figure 17i Blade Element Data - Blowing



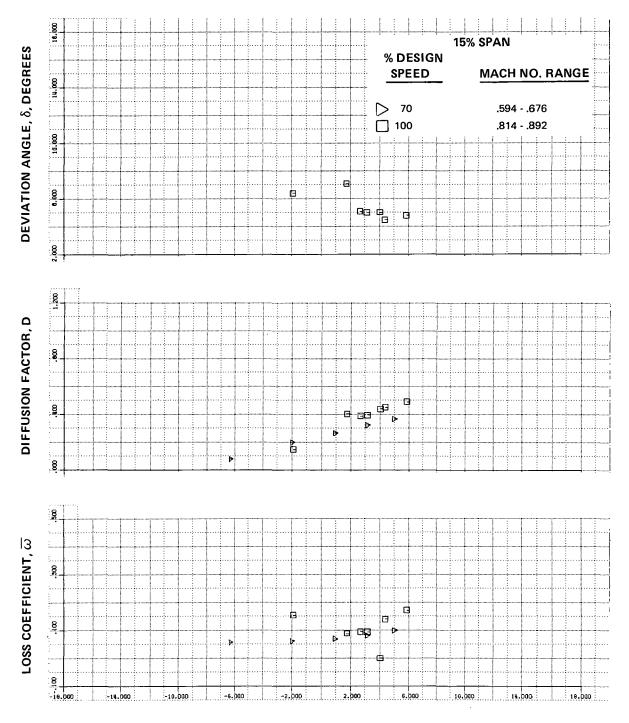
INCIDENCE ANGLE, SUCTION SURFACE, I_S , DEGREES

Figure 18a Blade Element Data - Suction



INCIDENCE ANGLE, SUCTION SURFACE, I_S , DEGREES

Figure 18b Blade Element Data - Suction



INCIDENCE ANGLE, SUCTION SURFACE, I_S , DEGREES

Figure 18c Blade Element Data - Suction

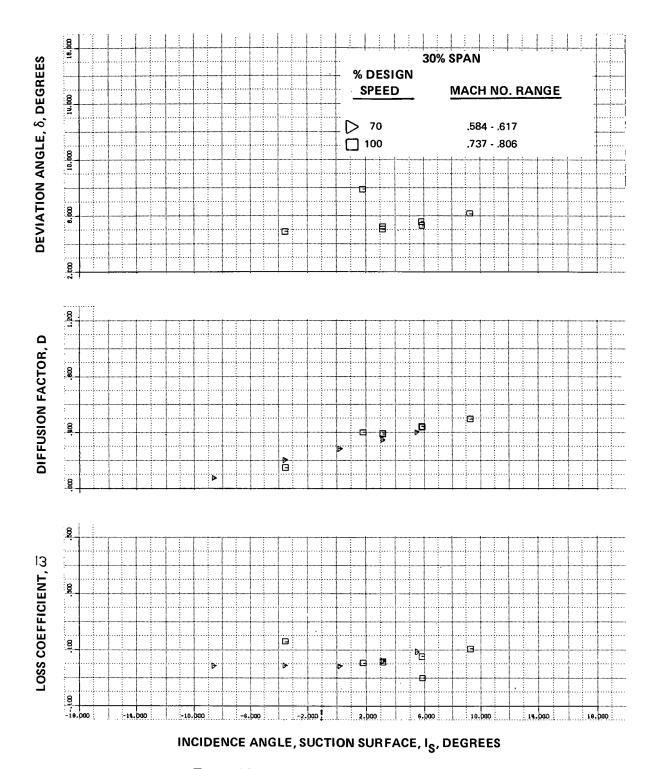


Figure 18d Blade Element Data - Suction

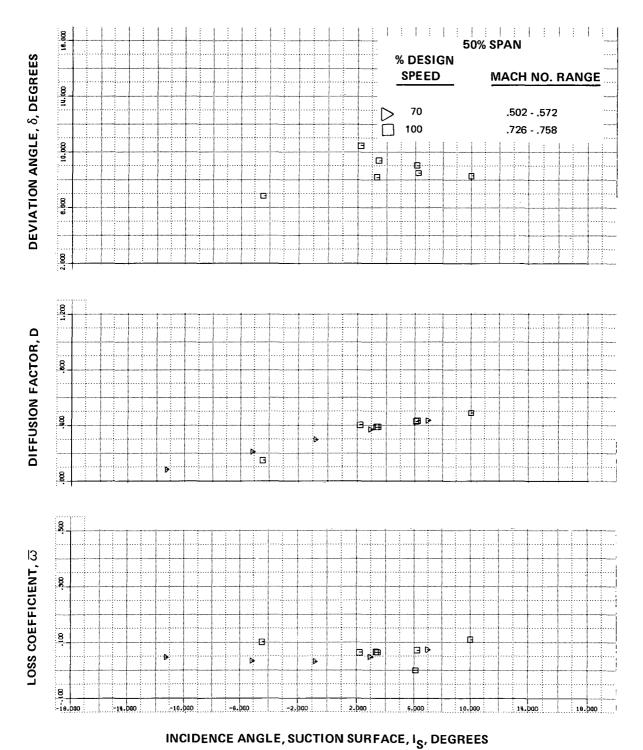


Figure 18e Blade Element Data - Suction

59

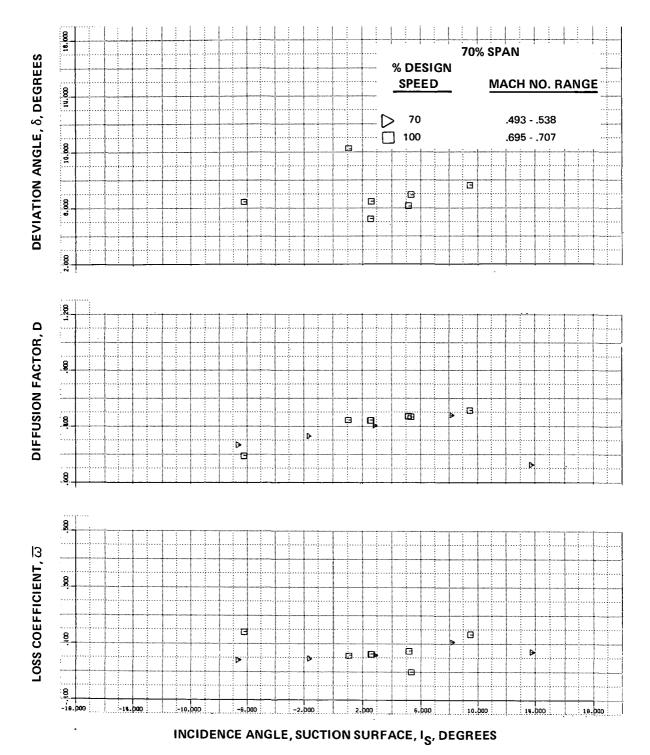
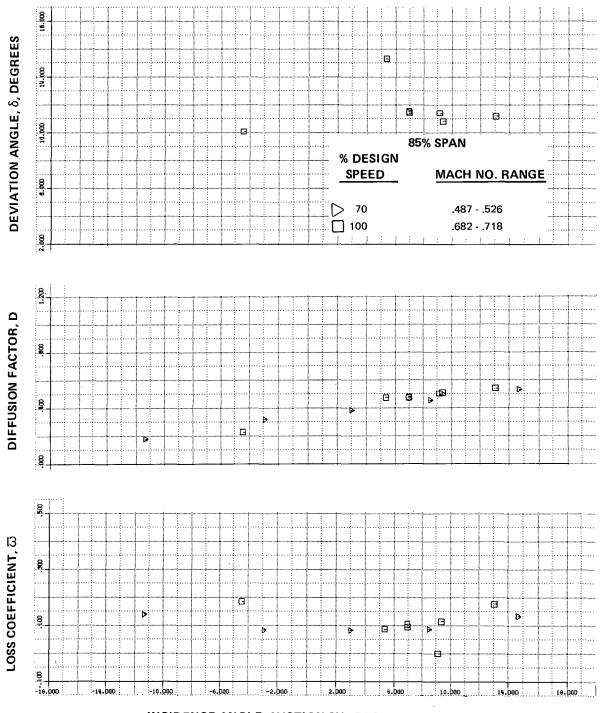


Figure 18f Blade Element Data - Suction



INCIDENCE ANGLE, SUCTION SURFACE, I_S, DEGREES
Figure 18g Blade Element Data - Suction

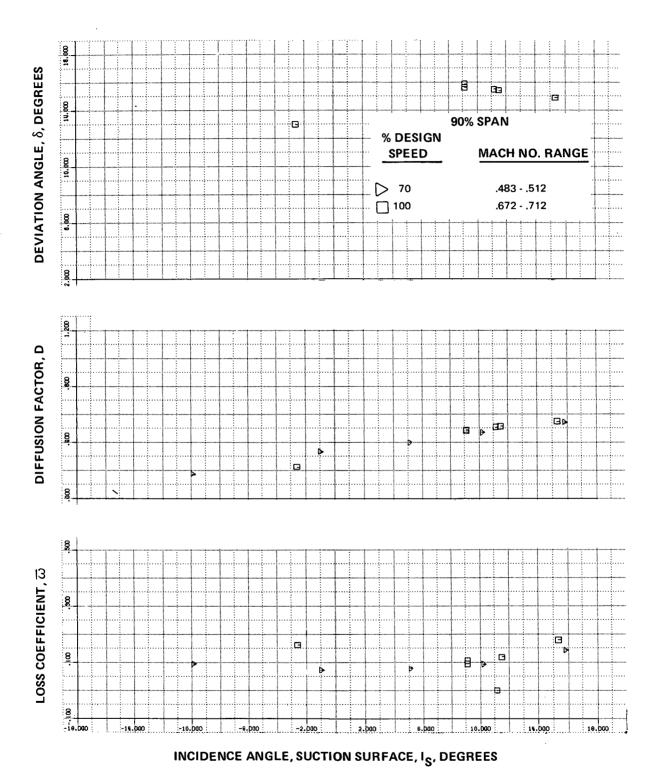


Figure 18h Blade Element Data - Suction

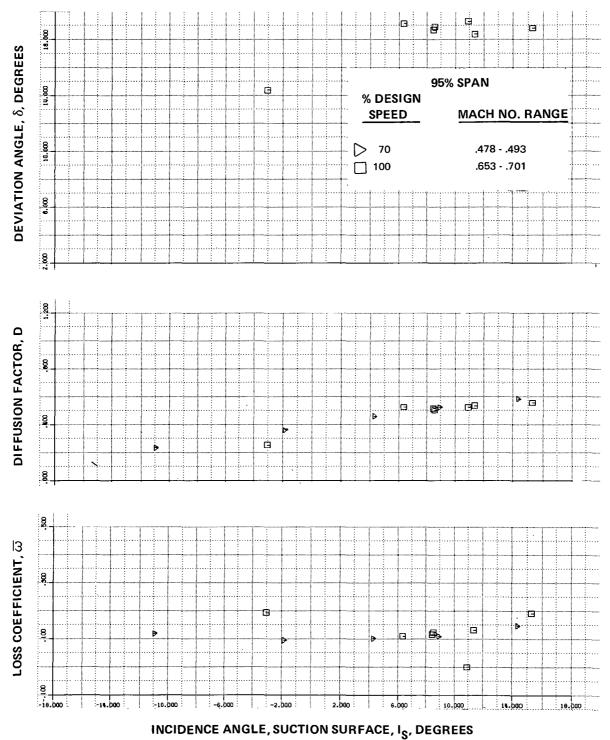


Figure 18i Blade Element Data - Suction

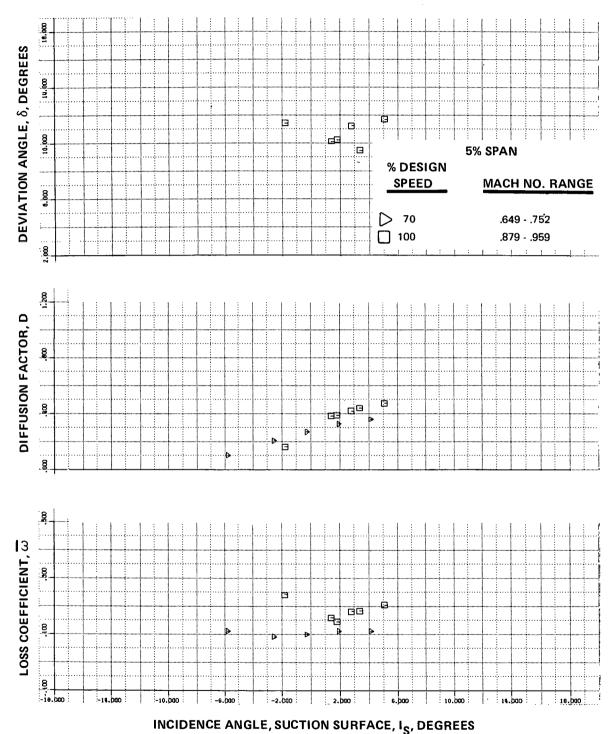


Figure 19a Blade Element Data - Combined

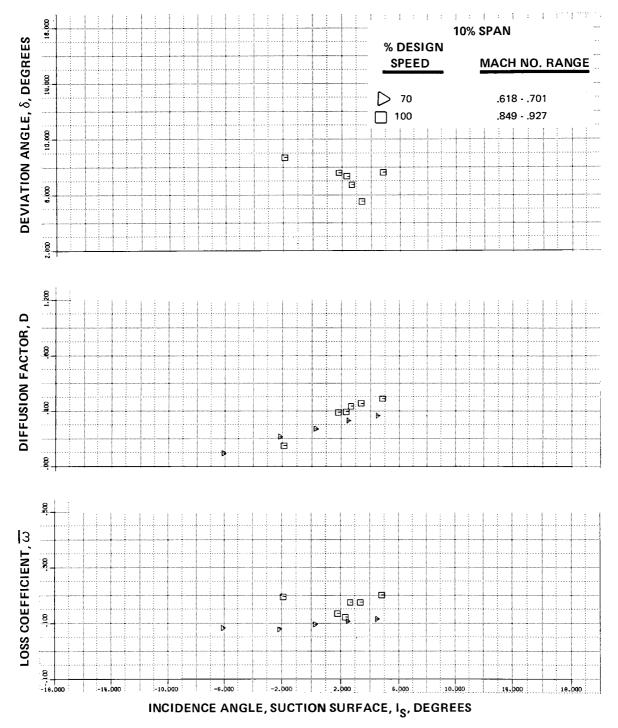
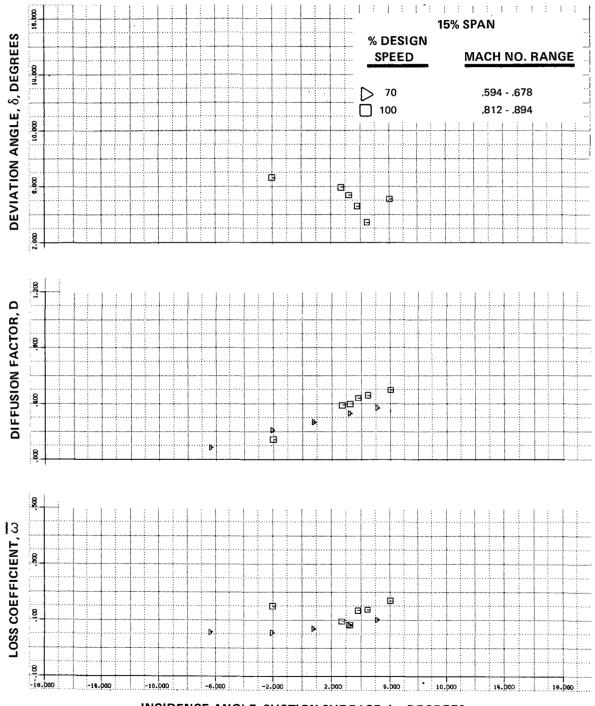


Figure 19b Blade Element Data - Combined



INCIDENCE ANGLE, SUCTION SURFACE, I_S, DEGREES
Figure 19c Blade Element Data - Combined

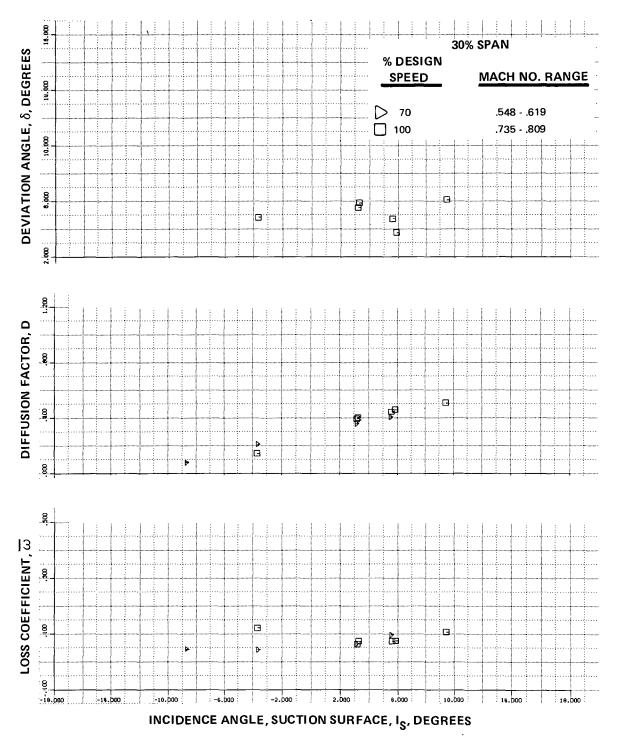


Figure 19d Blade Element Data - Combined

67

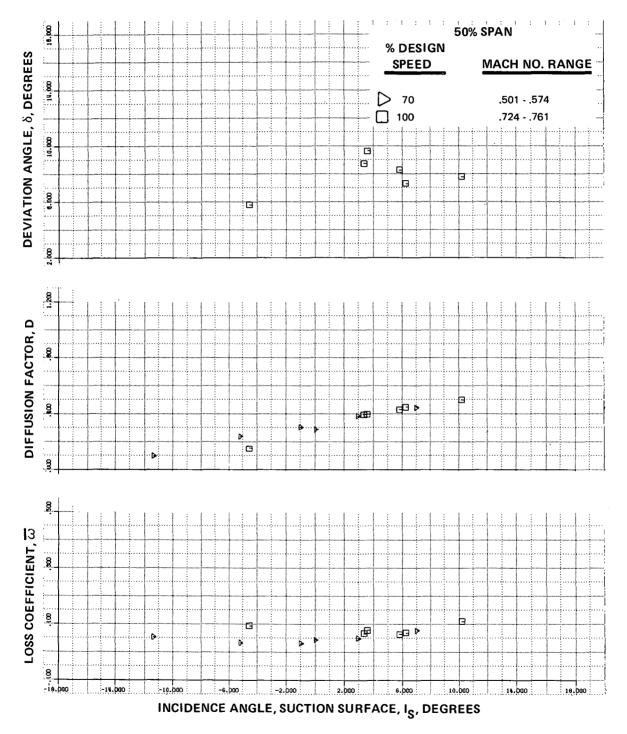


Figure 19e Blade Element Data - Combined

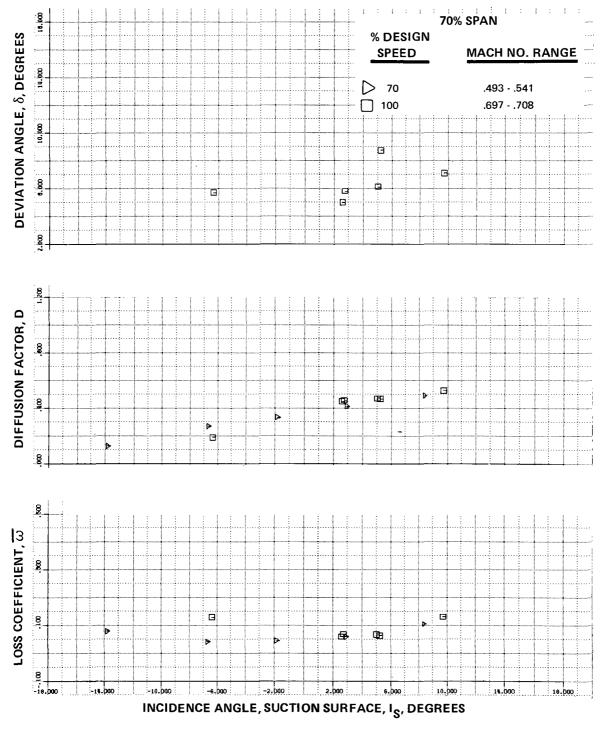


Figure 19f Blade Element Data - Combined

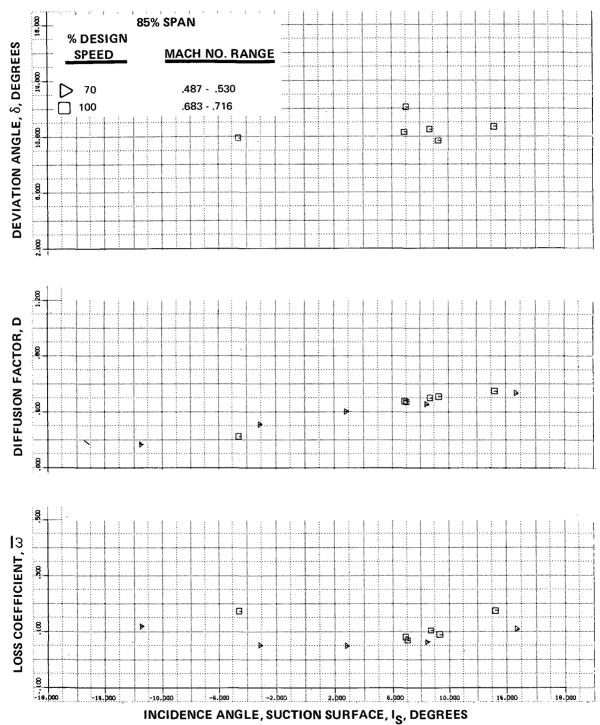


Figure 19g Blade Element Data - Combined

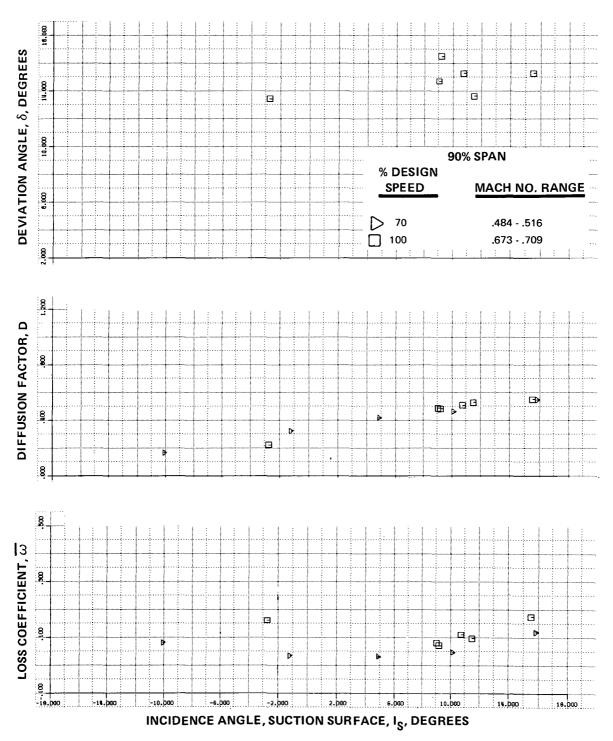


Figure 19h Blade Element Data - Combined

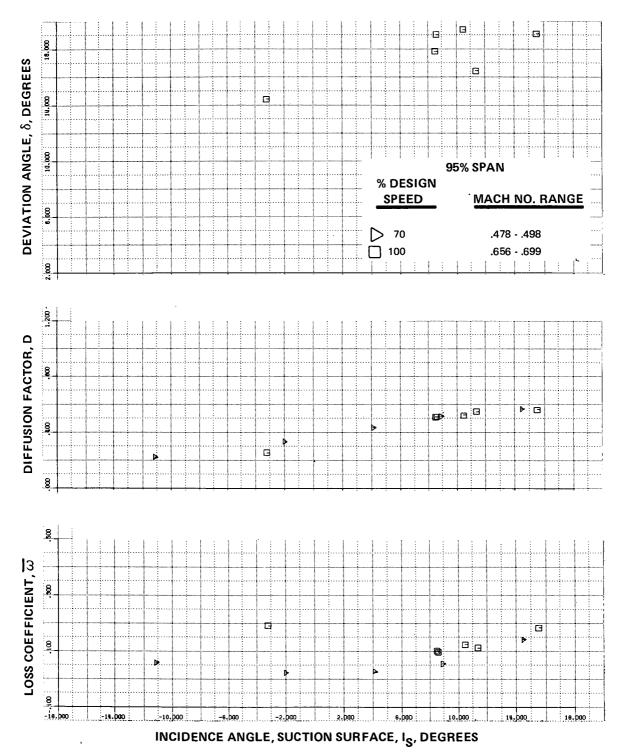


Figure 19i Blade Element Data - Combined

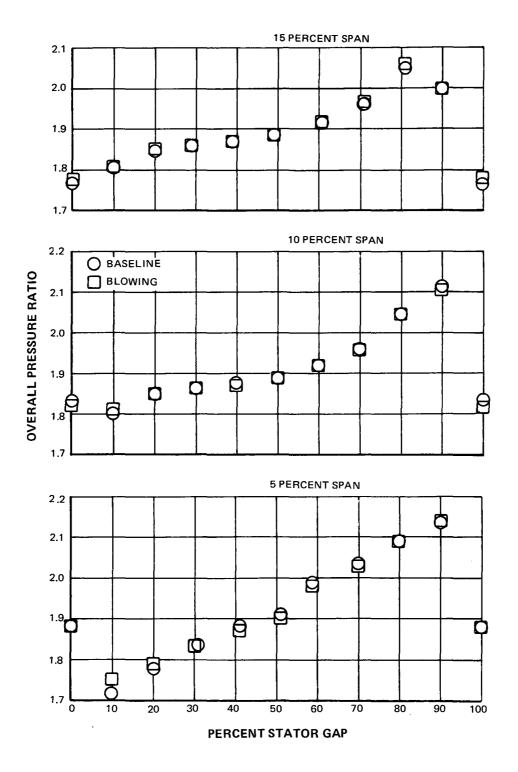


Figure 20a Stator Total Pressure Wake, Baseline and Blowing - 100% Design Speed, Near Surge

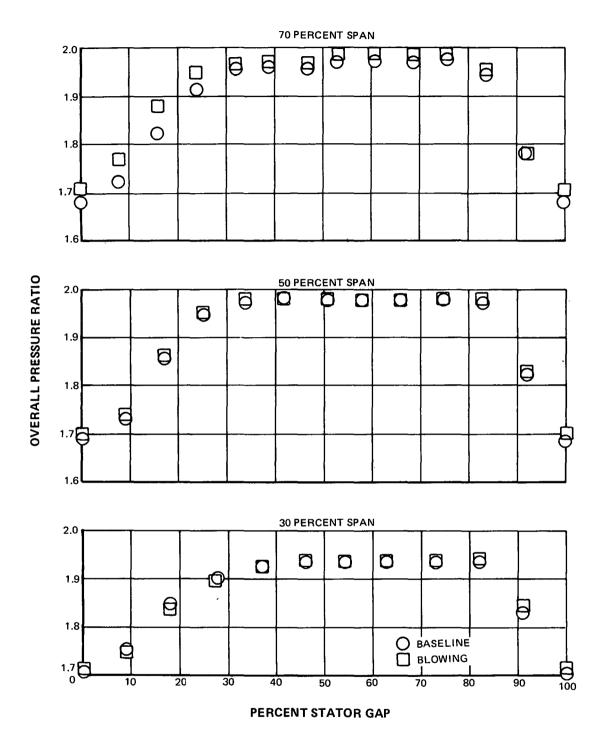


Figure 20b Stator Total Pressure Wake, Baseline and Blowing - 100% Design Speed, Near Surge

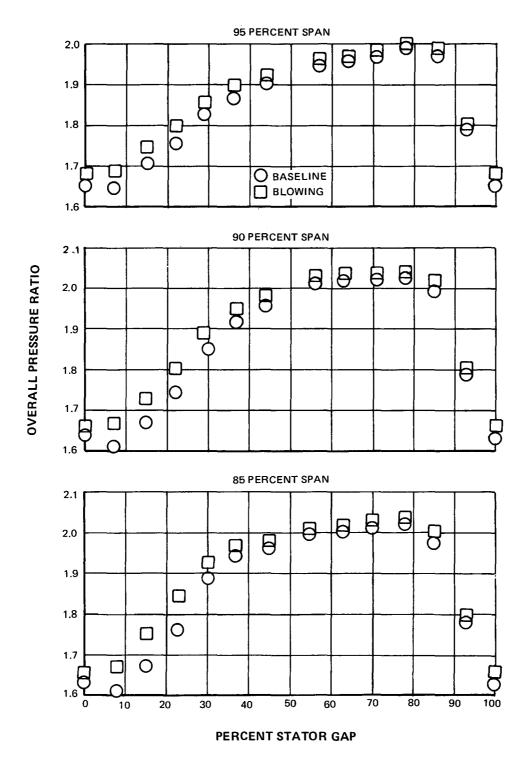


Figure 20c Stator Total Pressure Wake, Baseline and Blowing - 100% Design Speed, Near Surge

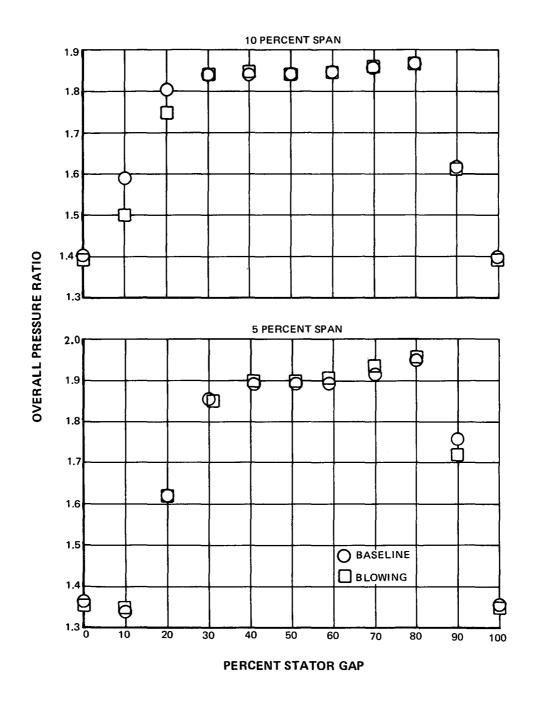


Figure 21a Stator Total Pressure Wake, Baseline and Blowing - 100% Design Speed, Wide Open

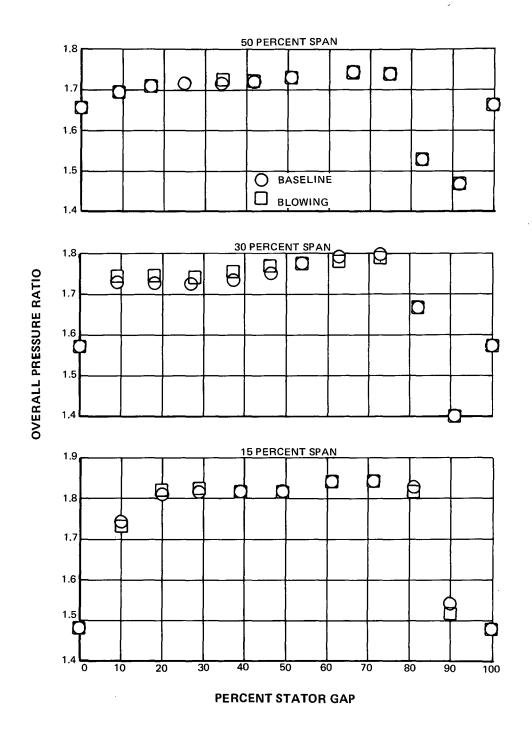


Figure 21b Stator Total Pressure Wake, Baseline and Blowing - 100% Design Speed, Wide Open

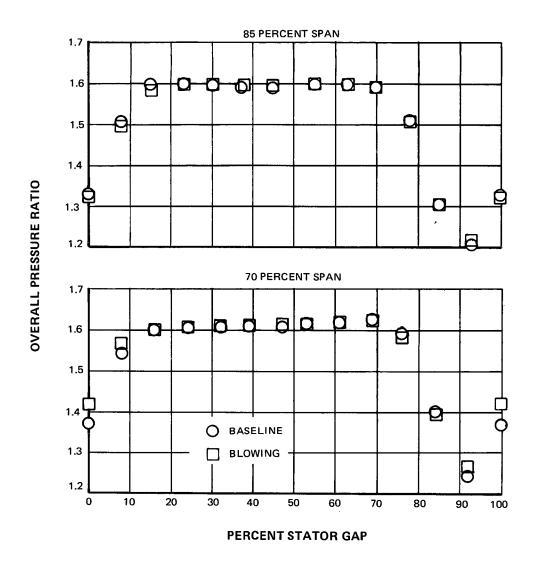


Figure 21c Stator Total Pressure Wake, Baseline and Blowing - 100% Design Speed, Wide Open

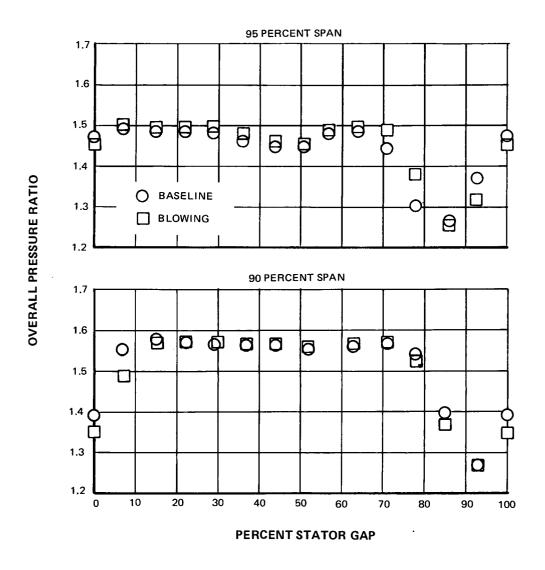


Figure 21d Stator Total Pressure Wake, Baseline and Blowing - 100% Design Speed, Wide Open

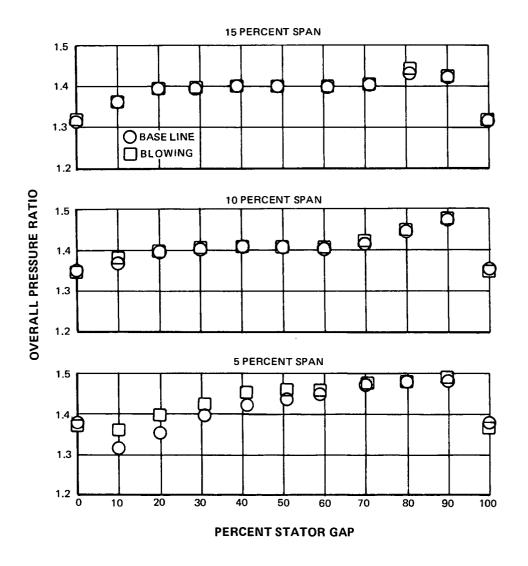


Figure 22a Stator Total Pressure Wake, Baseline and Blowing - 70% Design Speed, Near Surge

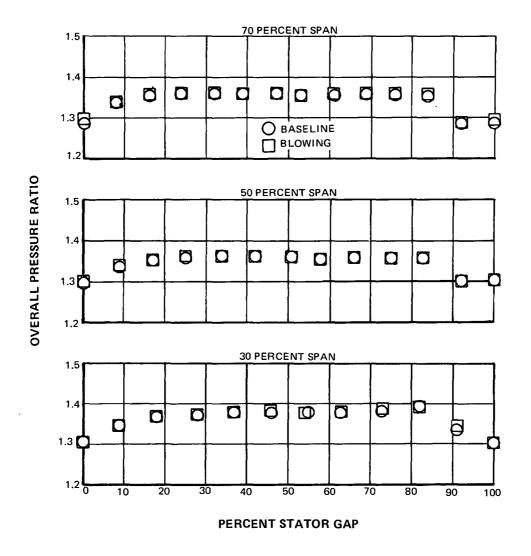


Figure 22b Stator Total Pressure Wake, Baseline and Blowing - 70% Design Speed, Near Surge

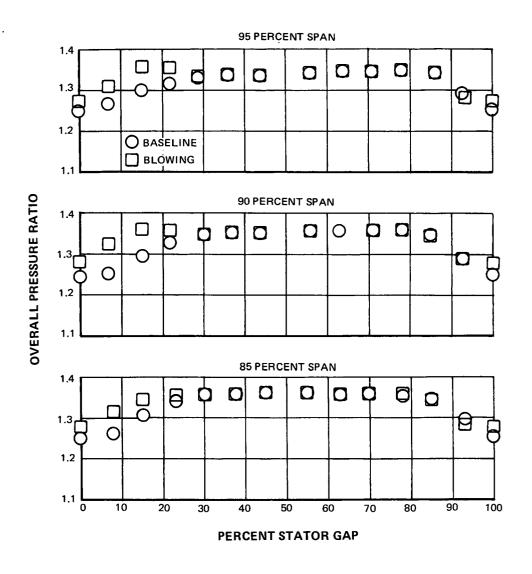


Figure 22c Stator Total Pressure Wake, Baseline and Blowing - 70% Design Speed, Near Surge

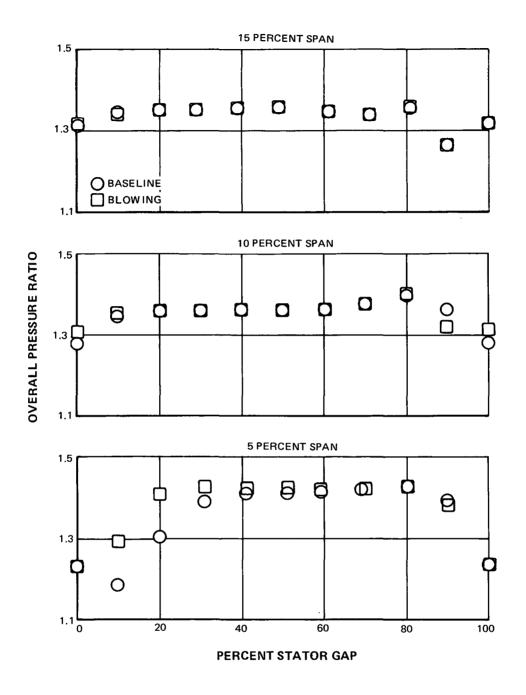


Figure 23a Stator Total Pressure Wake, Baseline and Blowing - 70% Design Speed, Wide Open

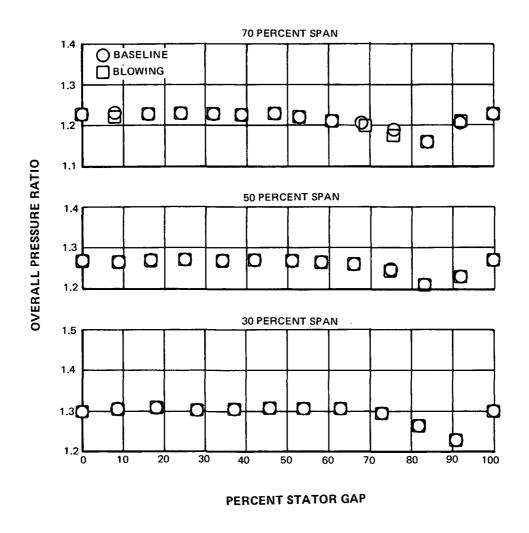


Figure 23b Stator Total Pressure Wake, Baseline and Blowing - 70% Design Speed, Wide Open

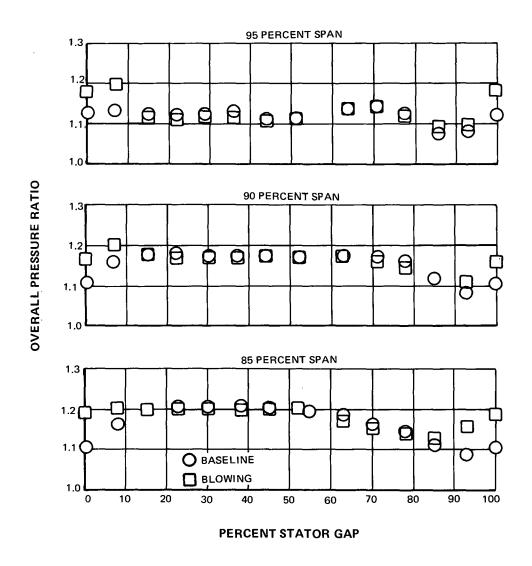


Figure 23c Stator Total Pressure Wake, Baseline and Blowing - 70% Design Speed, Wide Open

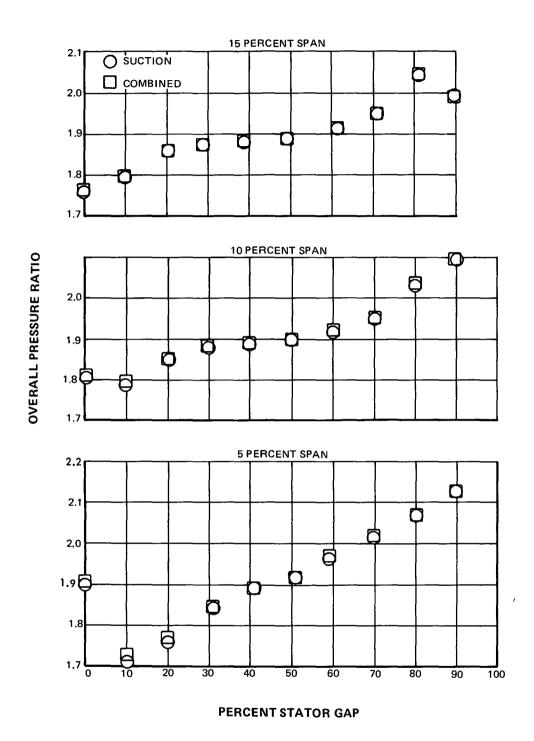


Figure 24a Stator Total Pressure Wake, Suction and Combined - 100% Design Speed, Near Surge

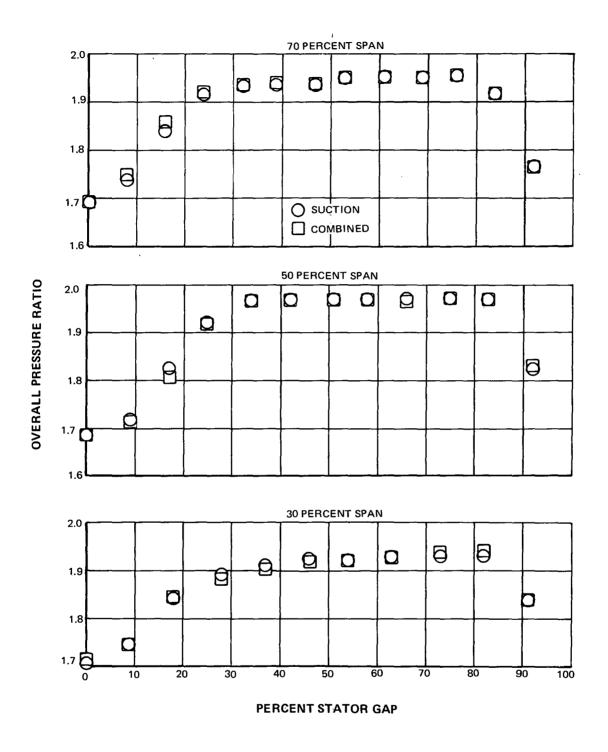


Figure 24b Stator Total Pressure Wake, Suction and Combined - 100% Design Speed, Near Surge

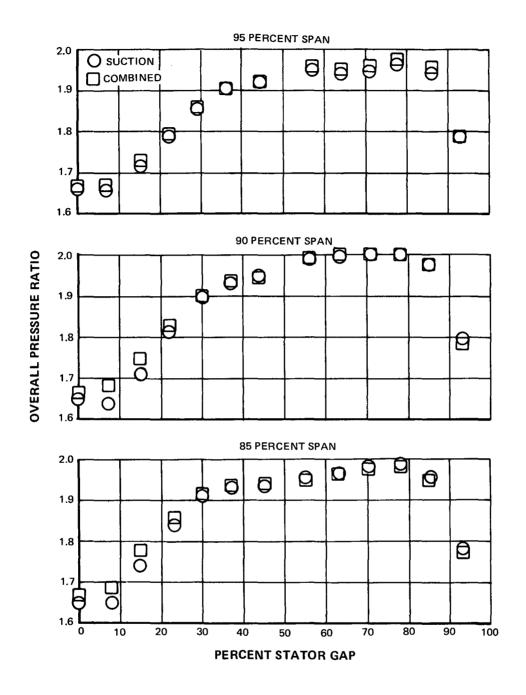


Figure 24c Stator Total Pressure Wake, Suction and Combined - 100% Design Speed, Near Surge

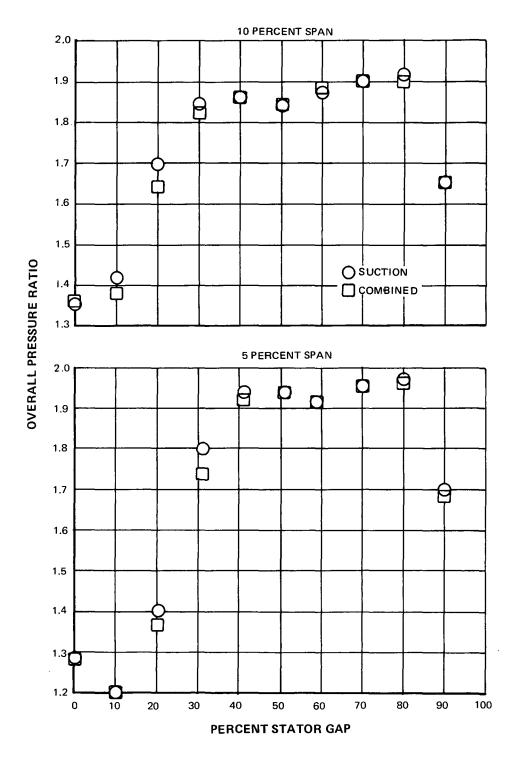


Figure 25a Stator Total Pressure Wake, Suction and Combined - 100% Design Speed, Wide Open

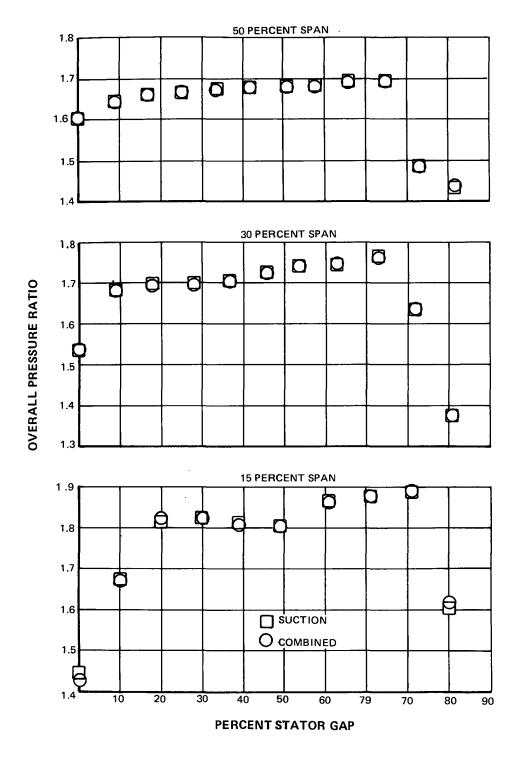


Figure 25b Stator Total Pressure Wake, Suction and Combined - 100% Design Speed, Wide Open

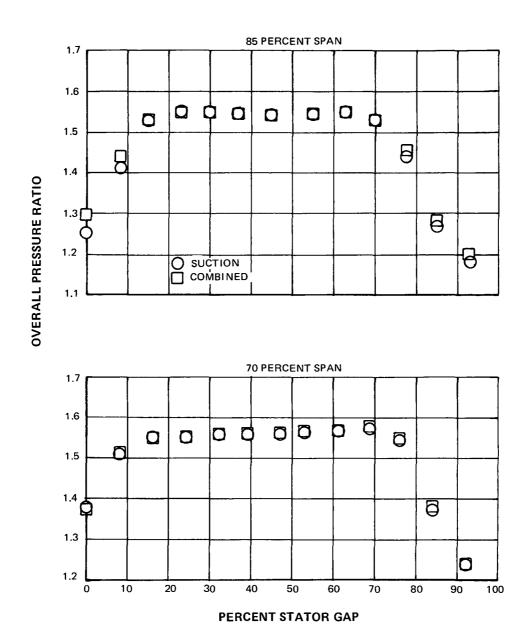


Figure 25c Stator Total Pressure Wake, Suction and Combined - 100% Design Speed, Wide Open

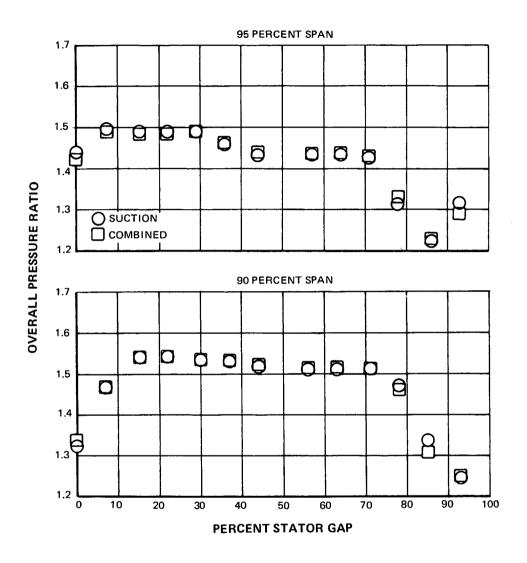


Figure 25d Stator Total Pressure Wake, Suction and Combined - 100% Design Speed, Wide Open

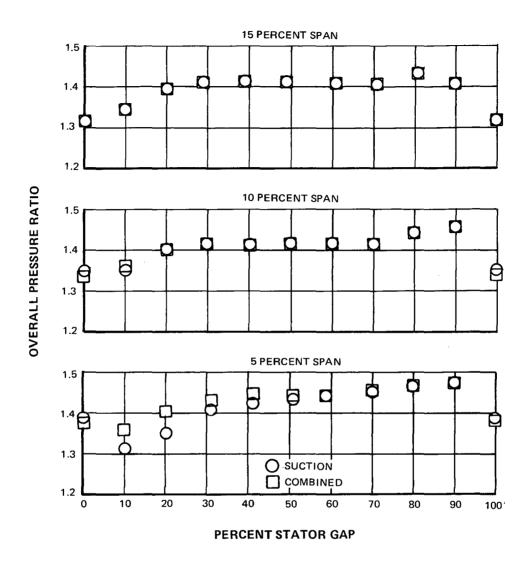


Figure 26a Stator Total Pressure Wake, Suction and Combined - 70% Design Speed, Near Surge

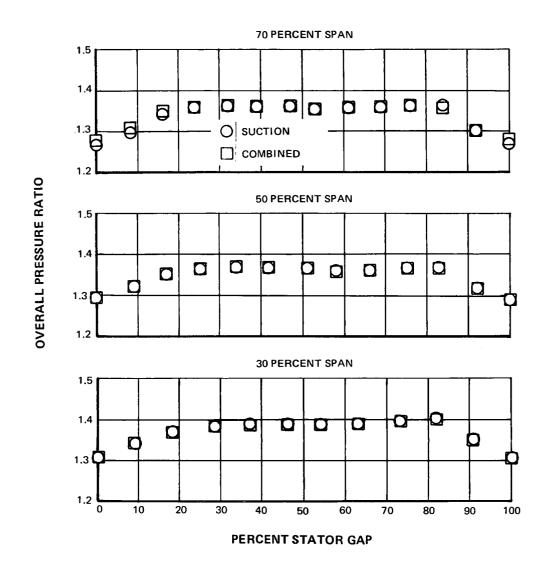


Figure 26b Stator Total Pressure Wake, Suction and Combined - 70% Design Speed, Near Surge

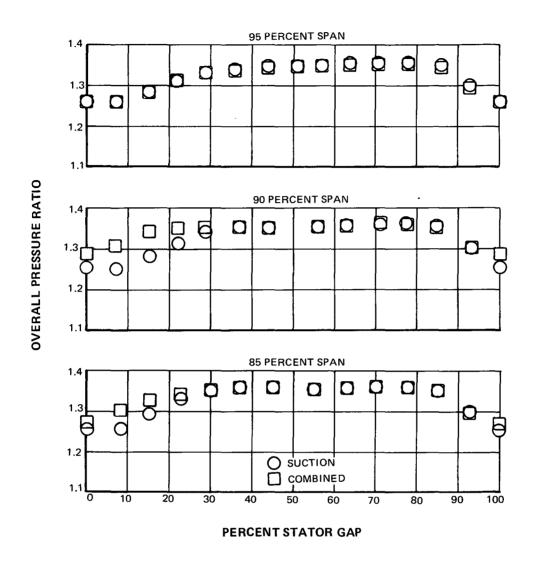


Figure 26c Stator Total Pressure Wake, Suction and Combined - 70% Design Speed, Near Surge

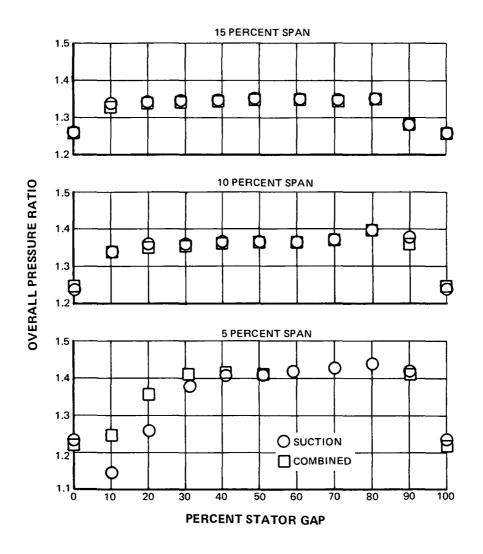


Figure 27a Stator Total Pressure Wake, Suction and Combined - 70% Design Speed, Wide Open

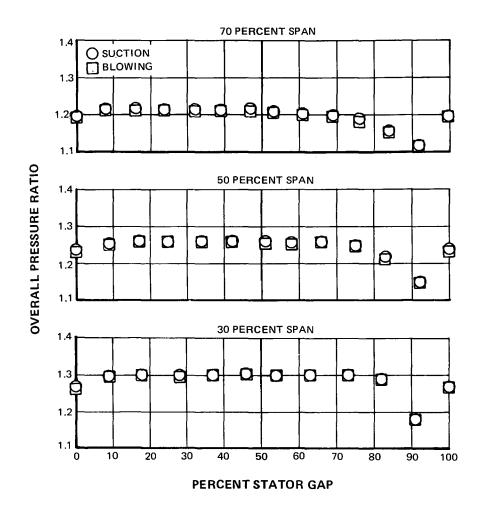


Figure 27b Stator Total Pressure Wake, Suction and Combined - 70% Design Speed, Wide Open

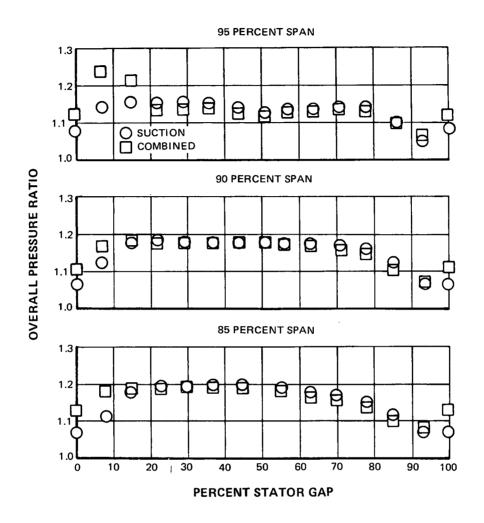
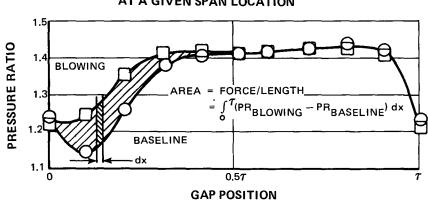


Figure 27c Stator Total Pressure Wake, Suction and Combined - 70% Design Speed, Wide Open

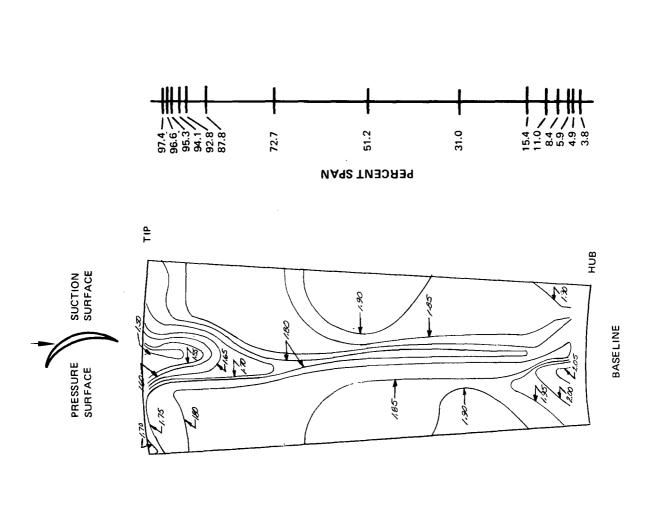
70% DESIGN SPEED WIDE OPEN THROTTLE

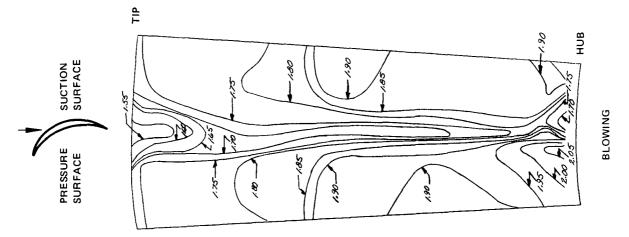
A TYPICAL STATOR WAKE PROFILE AT A GIVEN SPAN LOCATION

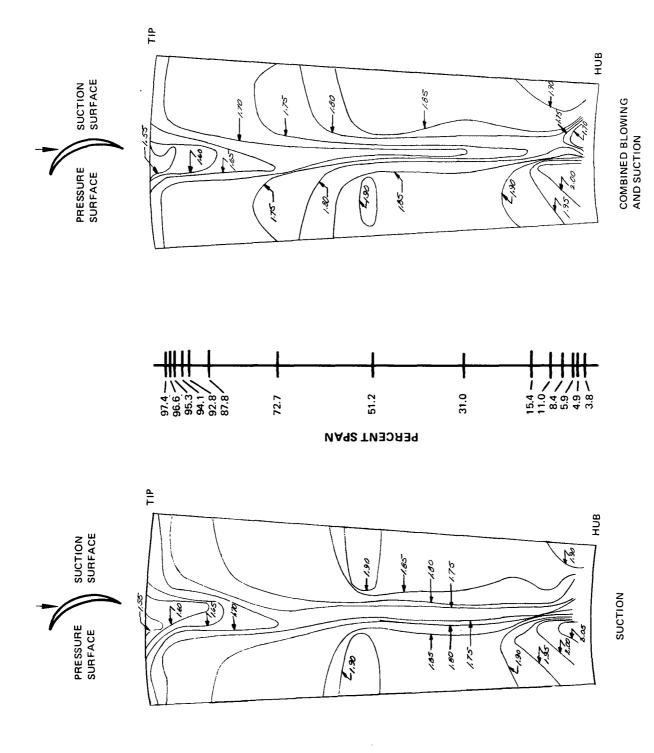


SPANWISE DISTRIBUTION OF TOTAL PRESSURE GAIN DUE TO BLOWING 10.04 THIS AREA IS OBTAINED FROM INTEGRATION OF WAKES AS INDICATED ABOVE 10.01 THIS AREA = (PR JET - PR BASELINE) X A JET 10.01 THIS AREA = (PR JET - PR BASELINE) X A JET 10.01 THE PRESSURE GAIN DUE TO BLOWING

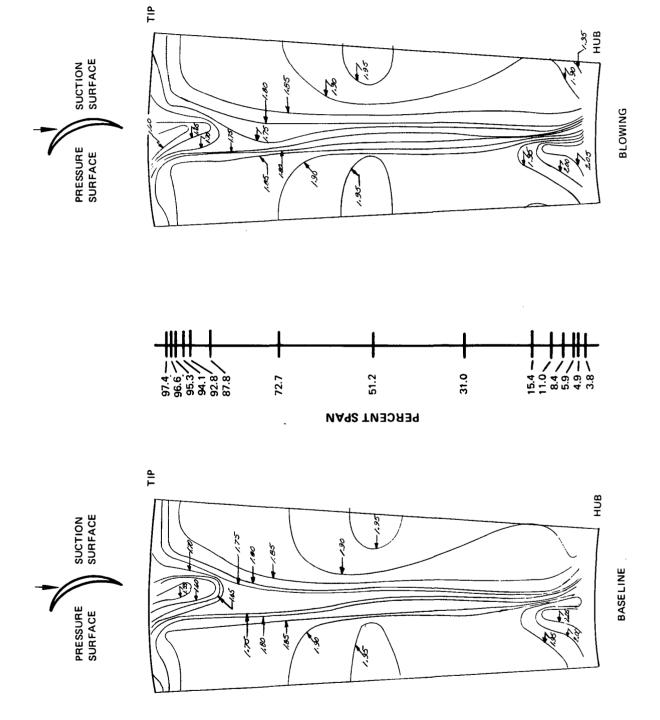
Figure 28 Integrated Net Gain in Wake Total Pressure With Blowing

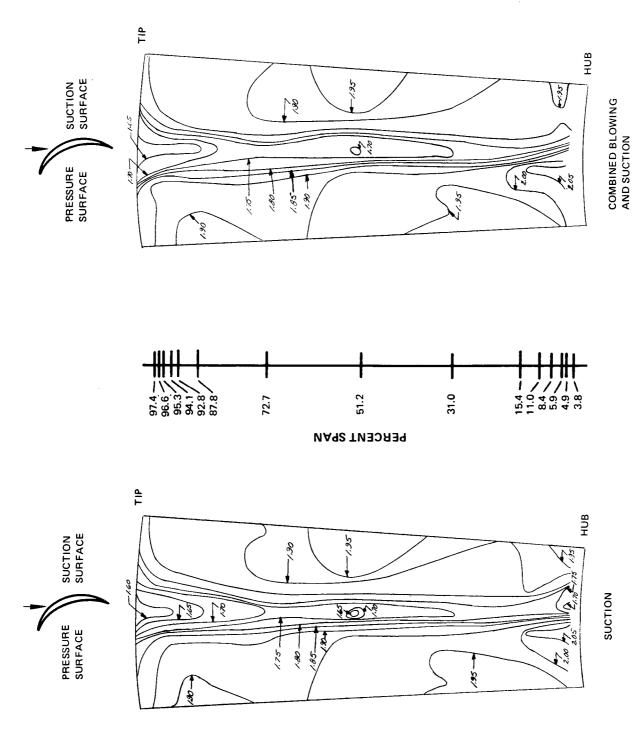




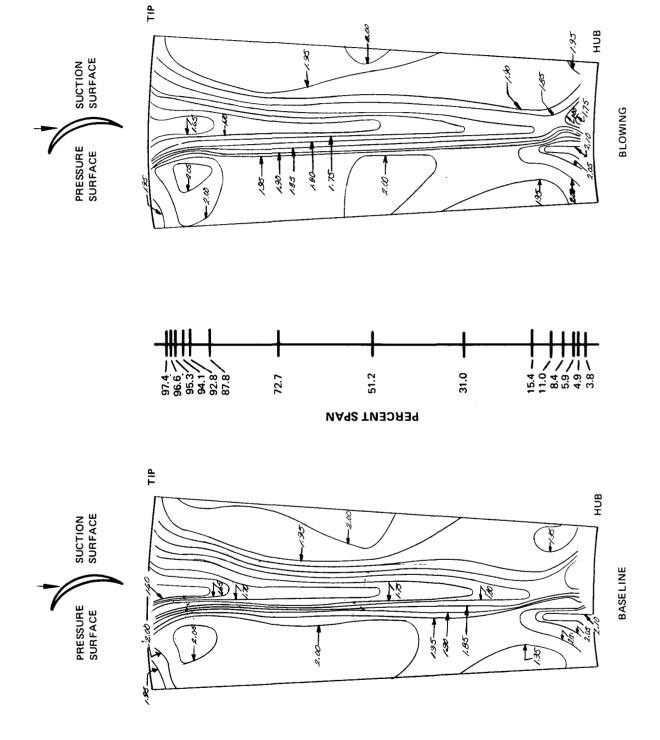


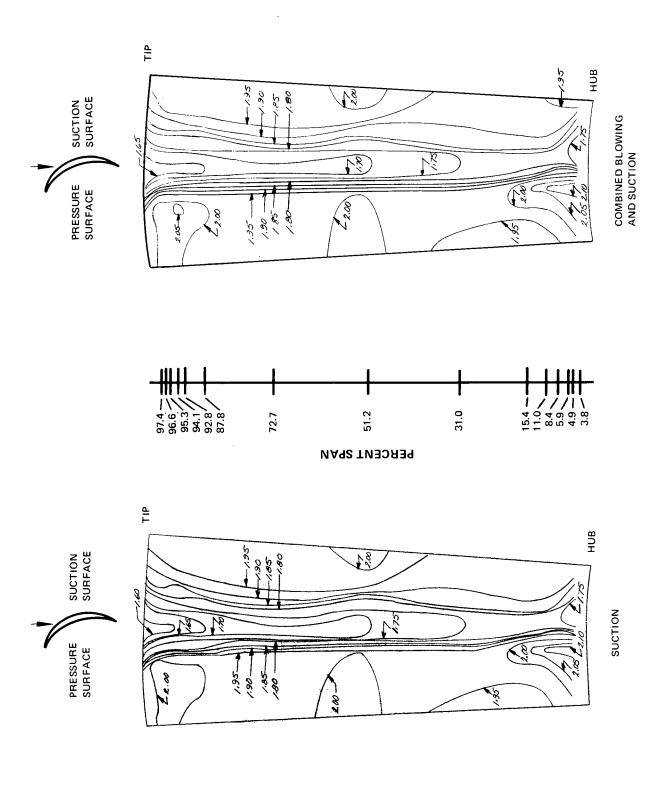
Stator Exit Total Pressure Ratio Contour Plots at 100% Design Speed - Total Inlet Corrected Airflow = 180.63 lb/sec Rotor Pressure Ratio = 1.8862 Figure 29



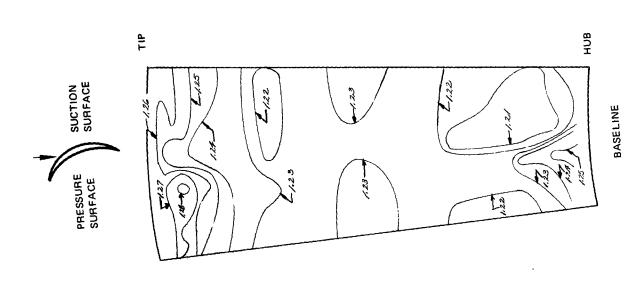


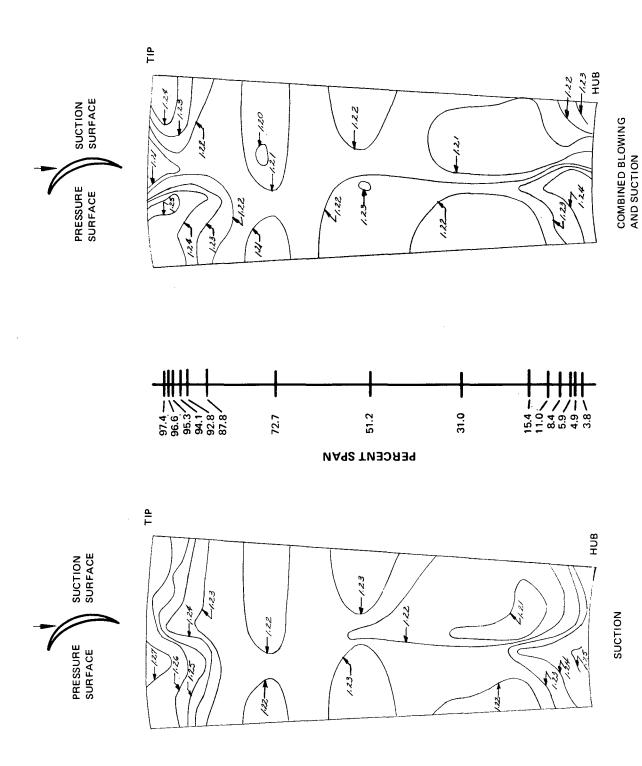
Stator Exit Total Pressure Ratio Contour Plots at 100% Design Speed — Total Inlet Corrected Airflow = 179.86 lb/sec Rotor Pressure Ratio = 1.9079 Figure 30



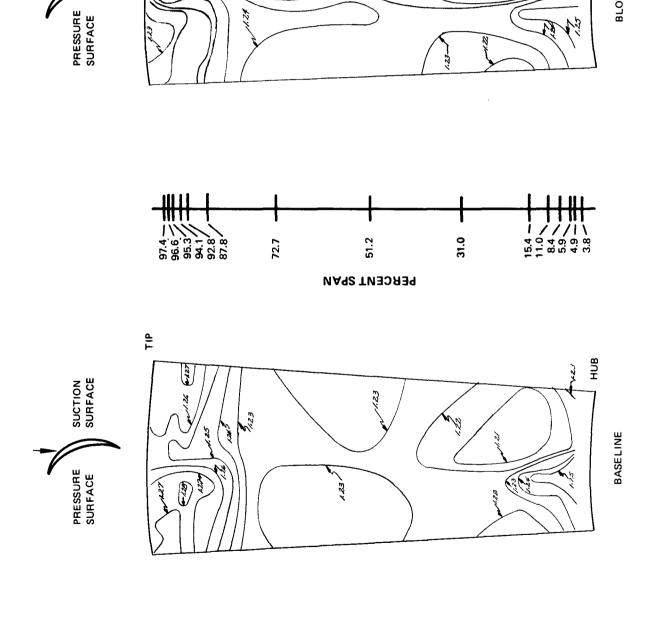


Stator Exit Total Pressure Ratio Contour Plots at 100% Design Speed - Total Inlet Correct Airflow = 171.52 lb/sec Rotor Pressure Ratio = 2.0123Figure 31





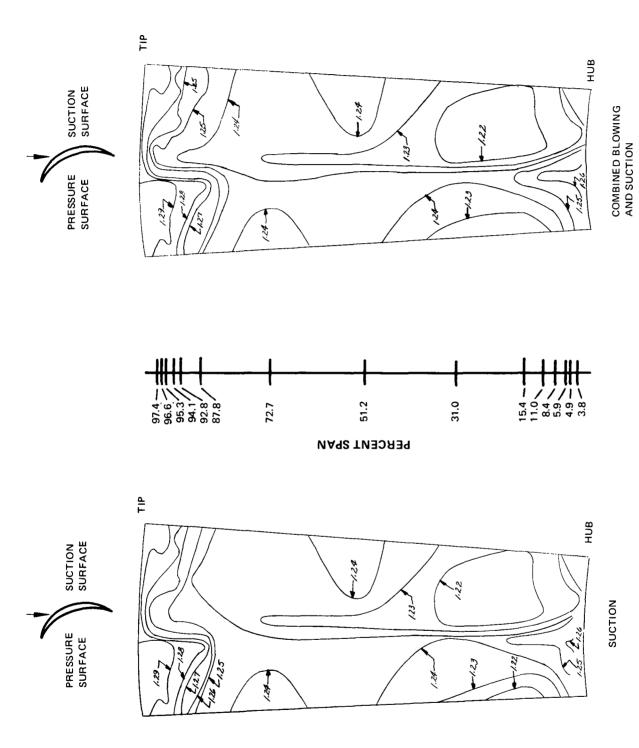
Stator Exit Total Temperature Ratio Contour Plots at 100% Design Speed - Total Inlet Corrected Airflow = 180.63 lb/sec Rotor Pressure Ratio = 1.8862 Figure 32



BLOWING

TIP 82.75

SUCTION SURFACE

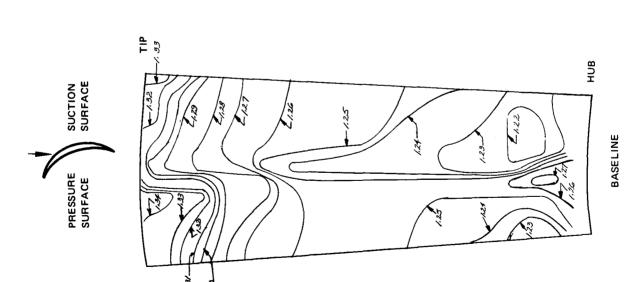


Stator Exit Total Temperature Ratio Contour Plots at 100% Design Speed – Total Inlet Corrected Airflow = 179.86 lb/sec Rotor Pressure Ratio = 1.9079 Figure 33

BLOWING

15.4 11.0 8.4 5.9 7 7 8.5 3.8 3.8

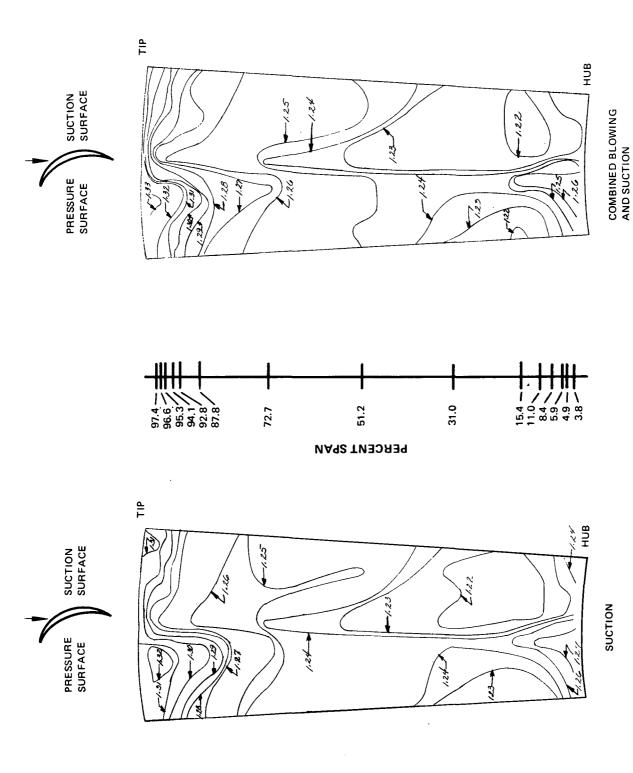
31.0



PERCENT SPAN

72.7

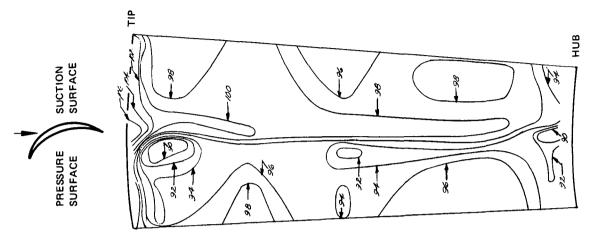
97.4 96.6. 95.3 94.1 87.8

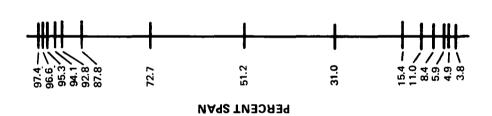


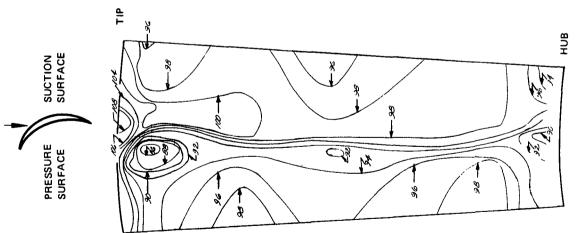
Stator Exit Total Temperature Ratio Contour Plots at 100% Design Speed - Total Inlet Corrected Airflow = 171.52 lb/sec Figure 34

Rotor Pressure Ratio = 2.0123



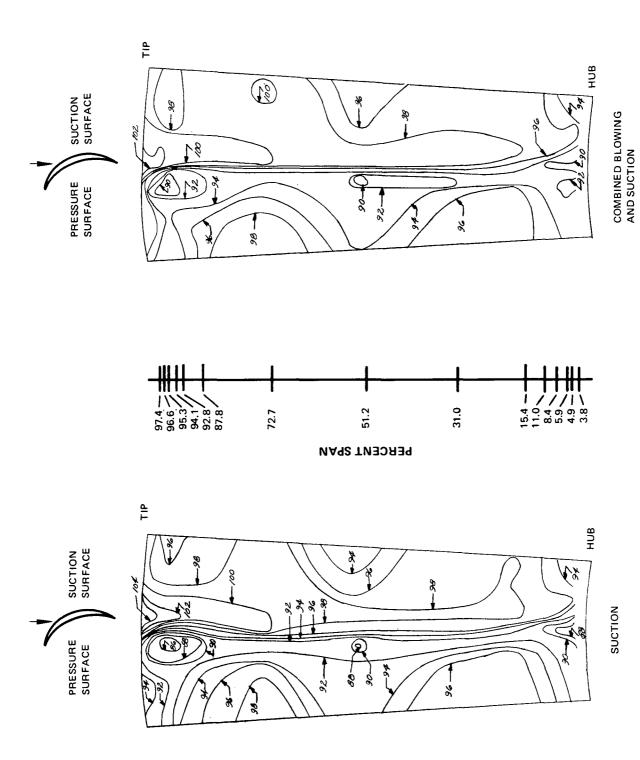




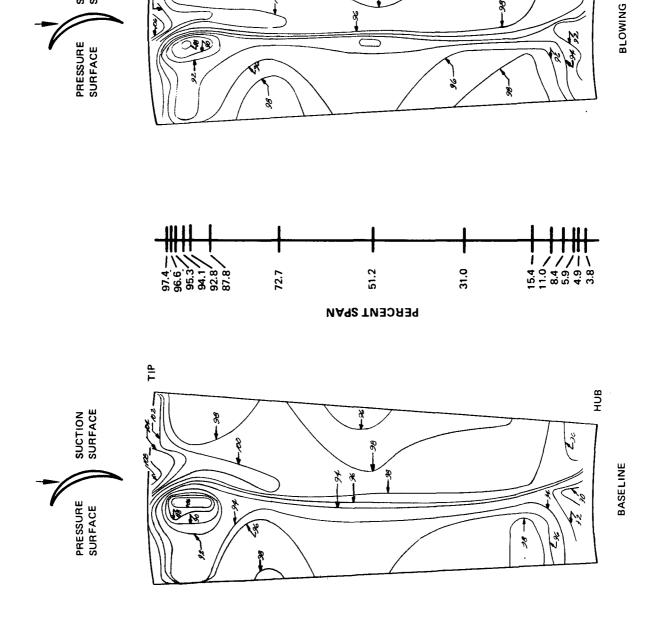


BASELINE





Stator Exit Total Absolute Air-Angle Contour Plots at 100% Design Speed - Total Inlet Corrected Airflow = 180.63 lb/sec Rotor Pressure Ratio = 179.86 Figure 35

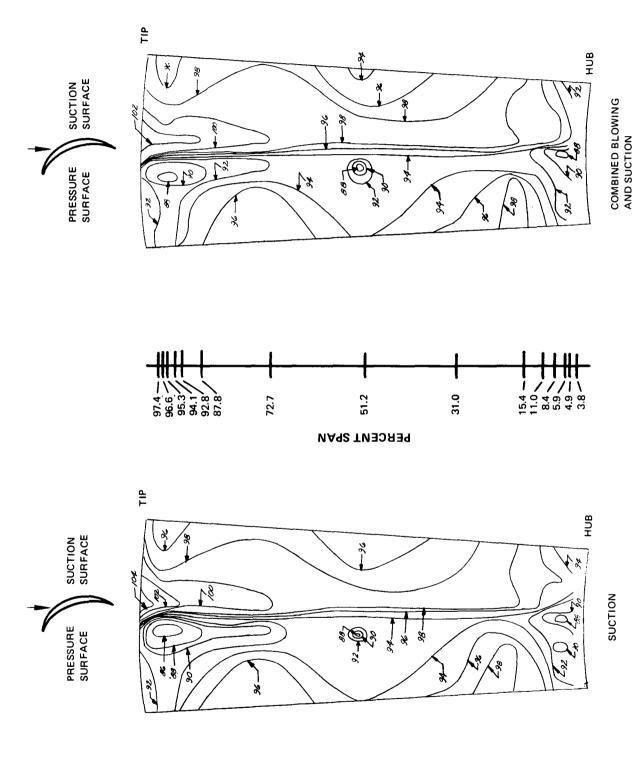


HUB

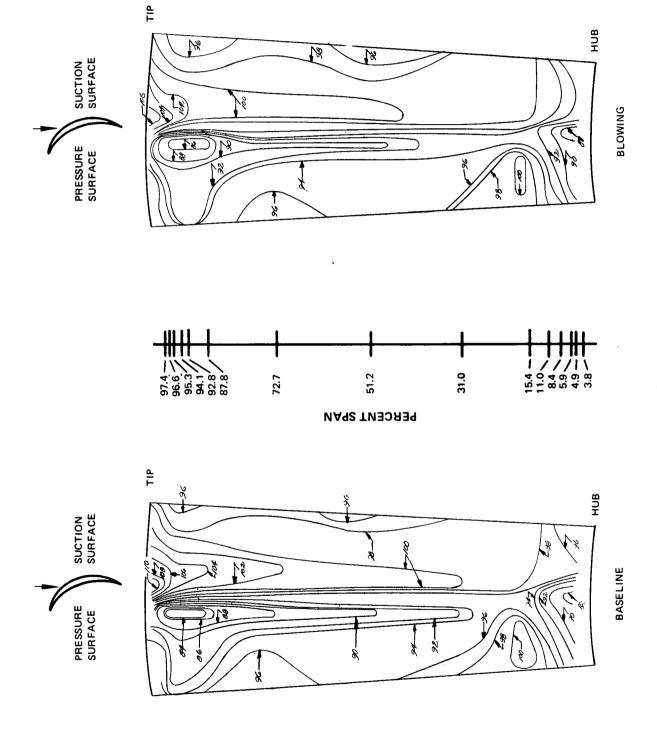
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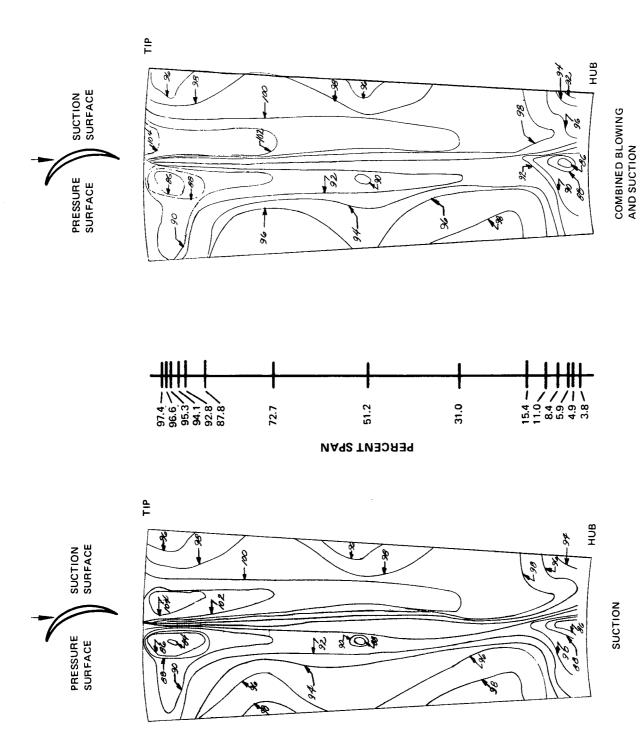
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SUCTION SURFACE

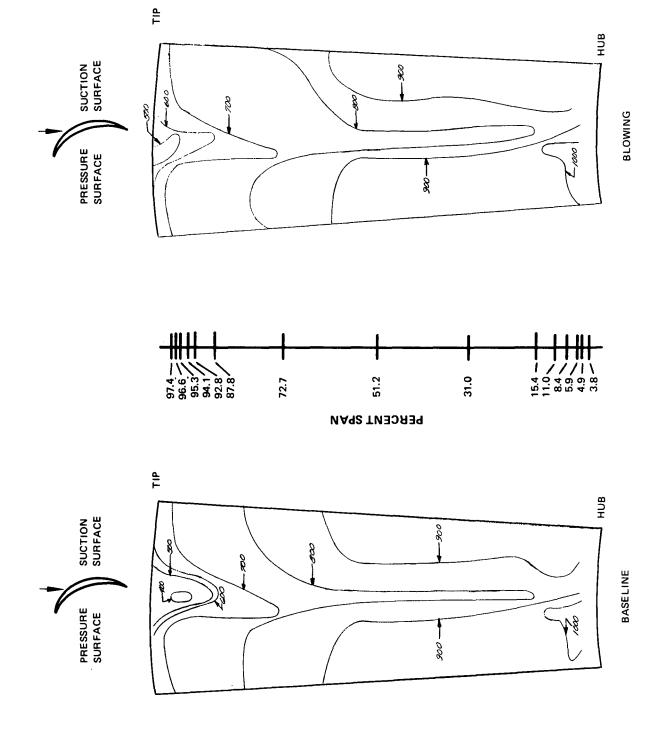


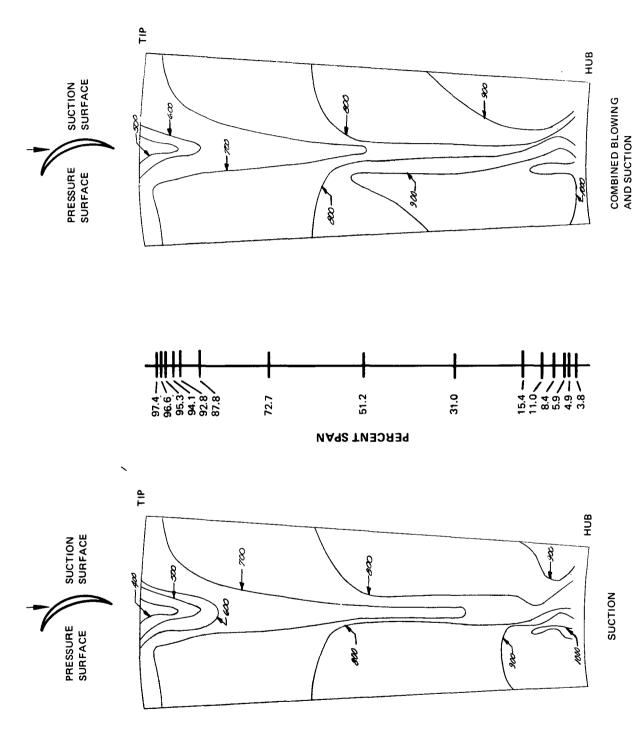
Stator Exit Total Absolute Air-Angle Contour Plots at 100% Design Speed — Total Inlet Corrected Airflow = 179.86 lb/sec Rotor Pressure Ratio = 1.9079 Figure 36



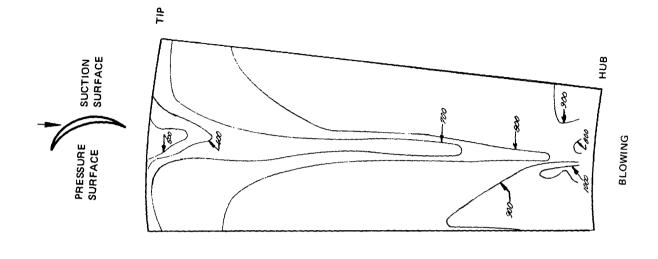


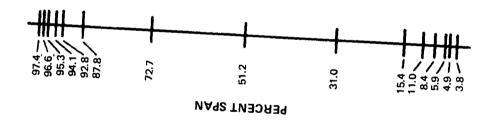
Stator Exit Total Absolute Air-Angle Contour Plots at 100% Design Speed - Total Inlet Corrected Airflow = 171.52 lb/sec Rotor Pressure Ratio = 2.0123 Figure 37

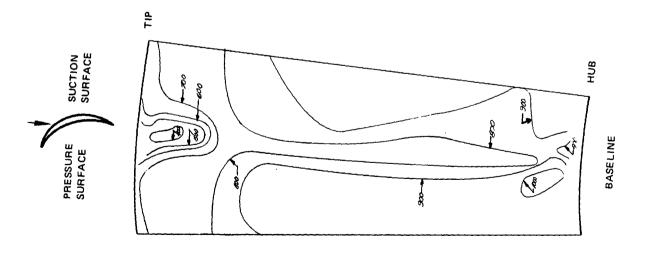


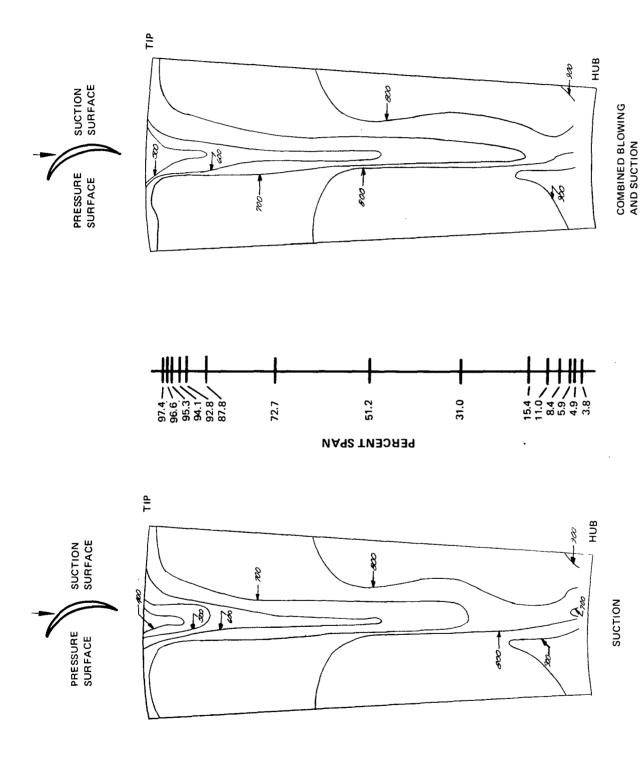


Stator Exit Meridional Velocity Contour Plots at 100% Design Speed – Total Inlet Corrected Airflow = 180.63 lb/sec Rotor Pressure Ratio = 1.8862 Figure 38

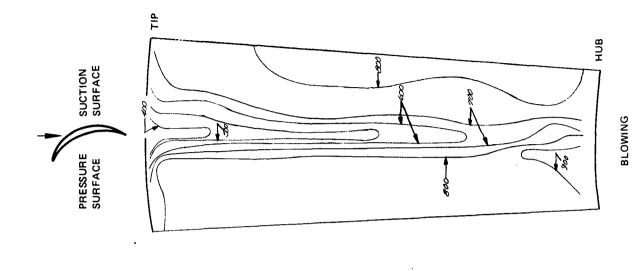


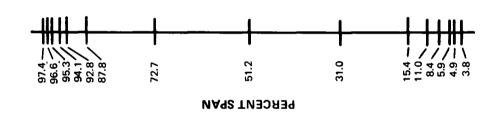


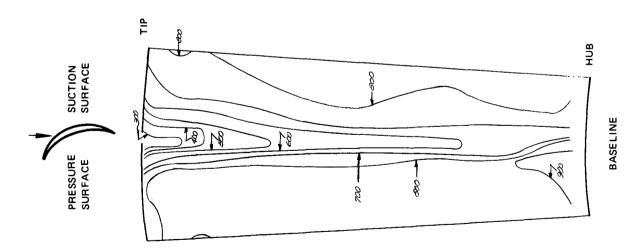


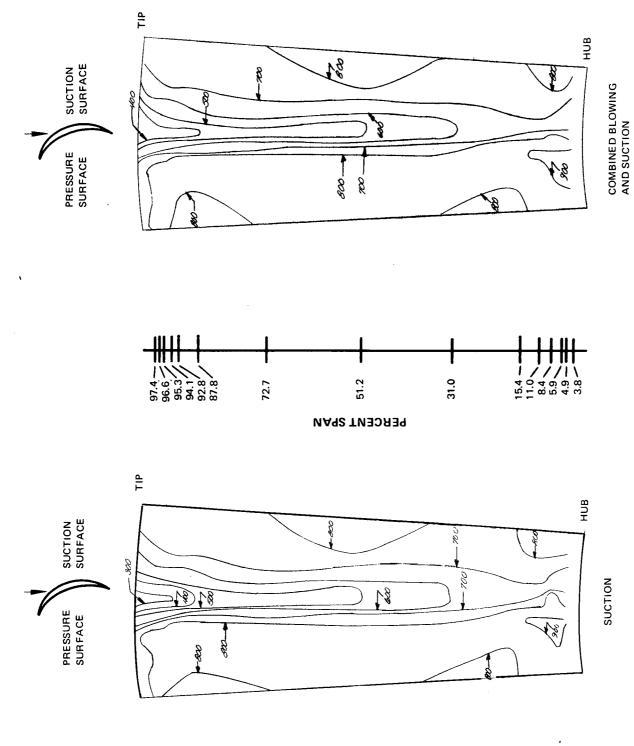


Stator Exit Meridional Velocity Contour Plots at 100% Design Speed - Total Inlet Corrected Airflow = 179.86 lb/sec Rotor Pressure Ratio = 1.9079 Figure 39

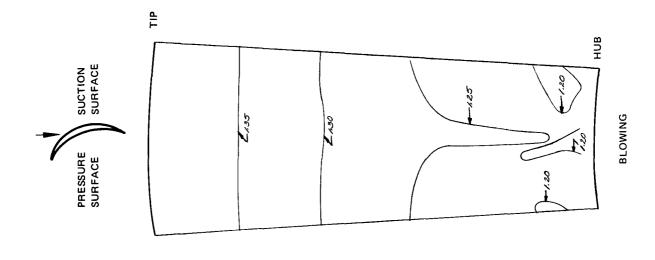




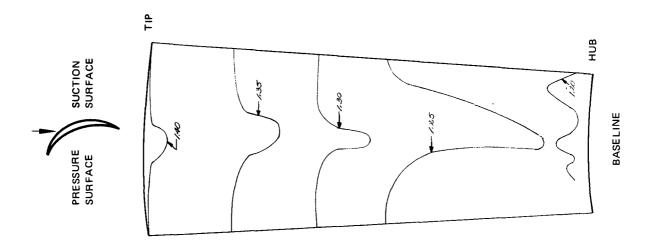


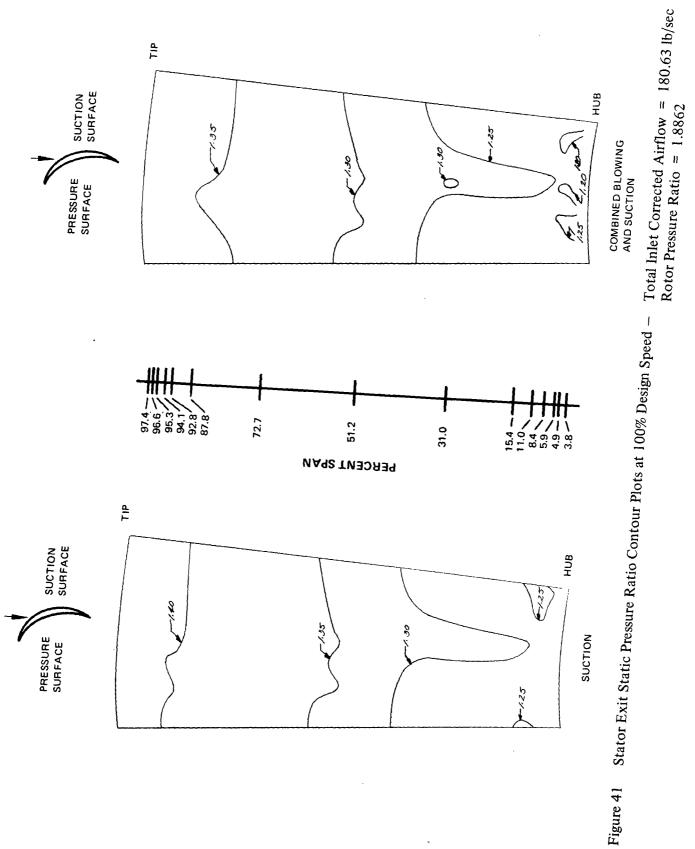


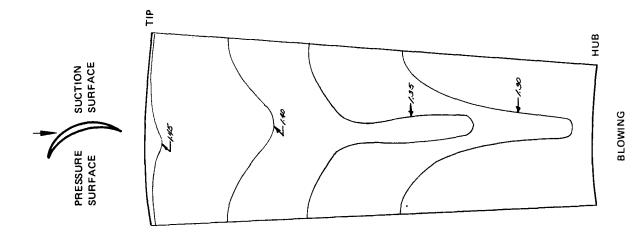
Stator Exit Meridional Velocity Contour Plots at 100% Design Speed — Total Inlet Corrected Airflow = 171.52 lb/sec Rotor Exit Meridional Velocity Contour Plots at 100% Design Speed — Total Inlet Corrected Airflow = 171.52 lb/sec Figure 40

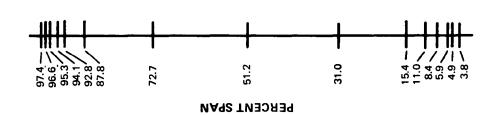


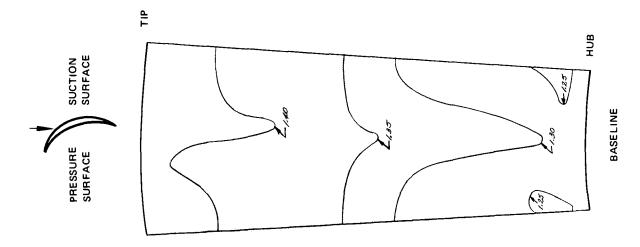


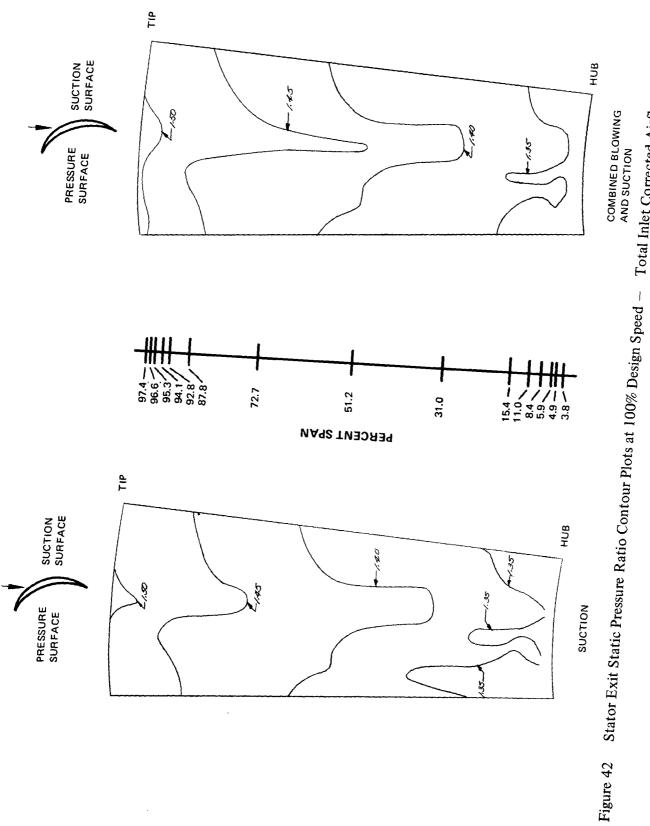




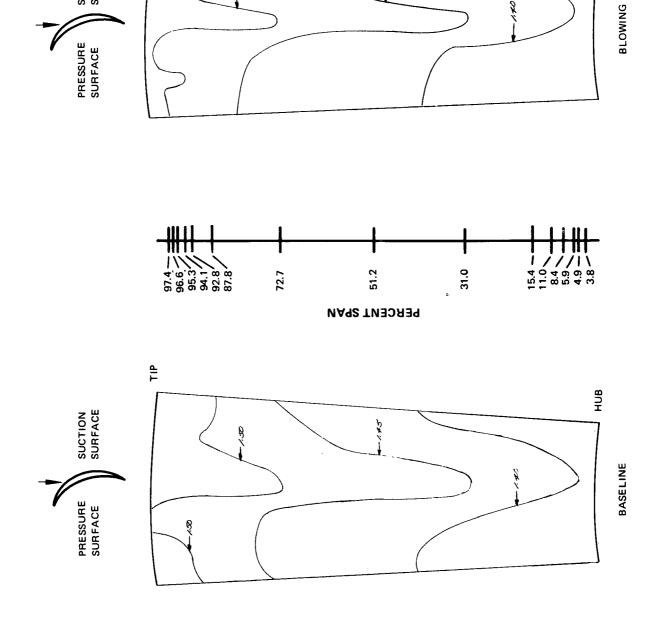








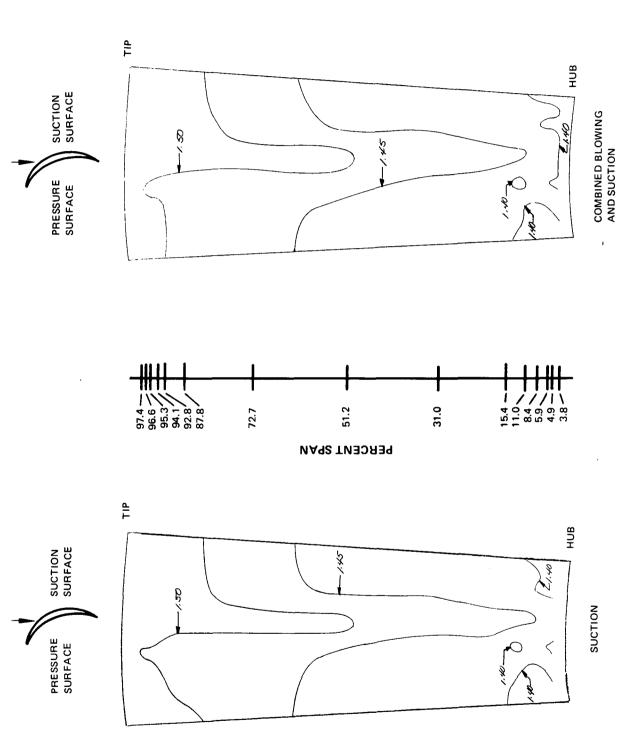
Total Inlet Corrected Airflow = 179.86 lb/sec Rotor Pressure Ratio = 1.9079



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SUCTION SURFACE



Total Inlet Corrected Airflow = 171.52 lb/sec Stator Exit Static Pressure Ratio Contour Plots at 100% Design Speed -Figure 43

Rotor Pressure Ratio = 2.0123

Figure 44 Stator Exit Total Pressure Ratio Contour Plots

Stator Exit Total Temperature Ratio Contour Plots

Figure 45

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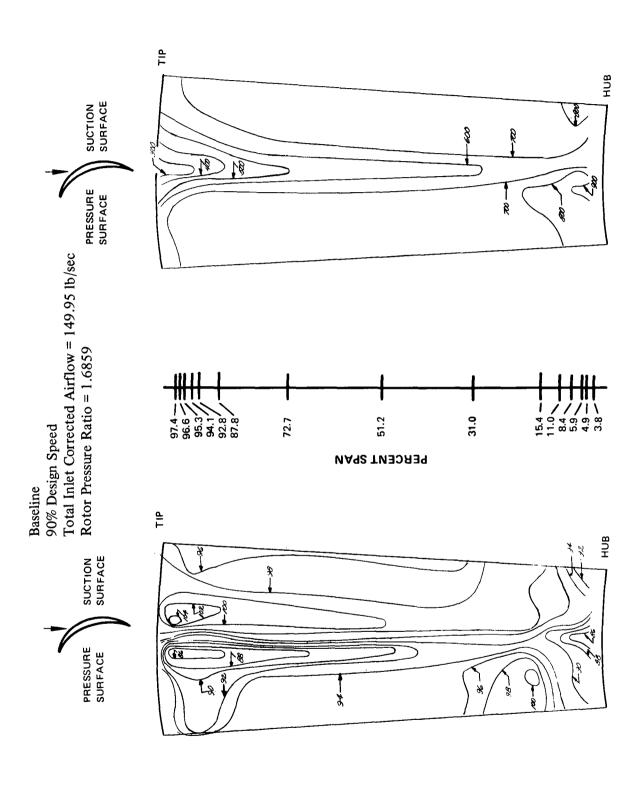


Figure 46 Stator Exit Absolute Air-Angle Contour Plots

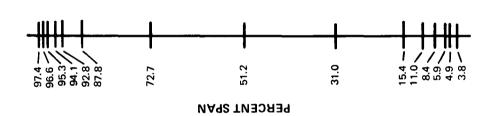
Stator Exit Meridional Velocity Contour Plots

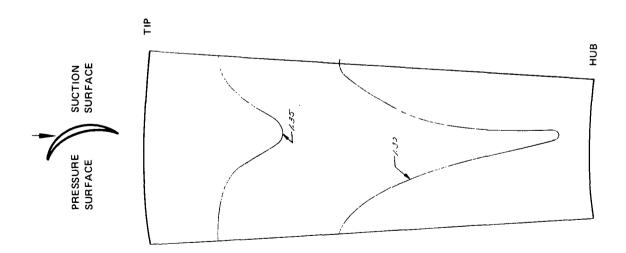
Figure 47

131

Figure 48 Stator Exit Static Pressure Ratio Contour Plots







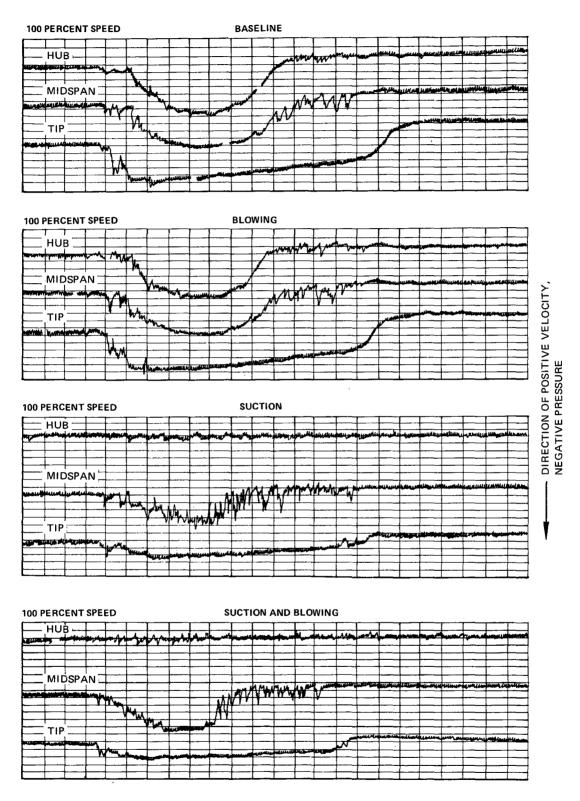


Figure 49 Hot Film Oscillograph Trace of Surge Cycle

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Appendix A

PERFORMANCE PARAMETERS

Relative total temperature a)

$$T'_{8} = t_{8} \left[1 + \frac{\gamma - 1}{2} (M'_{8})^{2} \right]$$
 (rotor in)
 $T'_{9} = T'_{8} + \left[\frac{(\omega r_{8})^{2} - (\omega r_{9})^{2}}{\frac{2\gamma}{\gamma - 1} Rg_{c}} \right]$ (rotor out)

Incidence angle based on mean camber line b)

$$i_{m} = \beta'_{8} - \beta'^{*}_{8}$$

$$i_{m} = \beta_{10} - \beta^{*}_{10}$$
(stator)

Deviation c)

$$\boldsymbol{\delta}^{\bullet} = \boldsymbol{\beta}^{\dagger}_{9} - \boldsymbol{\beta}^{\dagger}_{9} \tag{rotor}$$

$$\delta^{\circ} = \beta_{11} - \beta^{*}_{11} \qquad (stator)$$

d) Diffusion factor

$$D = 1 - \frac{V'_9}{V'_8} + \frac{r_9 V_{\theta 9} - r_8 V_{\theta 8}}{(r_8 + r_9) \sigma V'_8}$$
 (rotor)

$$D = 1 - \frac{V_{11}}{V_{10}} + \frac{r_{10}V_{\theta 10} - r_{11}V_{\theta 11}}{(r_{10} + r_{11})\sigma V_{10}}$$
 (stator)

Loss coefficient
$$\frac{P'_{8} \left[\frac{T'_{9}}{T'_{8}}\right] \frac{\gamma}{\gamma - 1}}{P'_{8} - p_{8}} - P'_{9}$$
(rotor)

$$\overline{\omega} = \frac{P_{10} - P_{11}}{P_{10} - P_{10}}$$
 (stator)

f) Loss parameter

$$\frac{\overline{\omega}\cos\beta'9}{2\sigma} \tag{rotor}$$

$$\frac{-\overline{\omega}\cos\beta_{11}}{2\sigma}$$
 (stator)

g) Polytropic efficiency

1)
$$\eta_{\rm p} = \frac{\frac{\gamma - 1}{\gamma} \ln \left[\frac{P_9}{P_7} \right]}{\ln \left[\frac{T_9}{T_0} \right]}$$
 (rotor)

2)
$$\eta_{p} = \frac{\frac{\gamma - 1}{\gamma} \ln \left[\frac{p_{11}}{p_{10}}\right]}{\ln \left[\frac{t_{11}}{t_{10}}\right]}$$
 (stator)

h) Adiabatic efficiency

$$\eta_{\text{ad}} = \frac{\begin{bmatrix} P_9 \\ P_7 \end{bmatrix} \frac{\gamma - 1}{\gamma}}{\begin{bmatrix} \frac{T_{12}}{T_0} \end{bmatrix} - 1}$$
(rotor)

$$\eta_{\text{ad}} = \frac{\left[\frac{P_{12}}{P_7}\right] \frac{\gamma - 1}{\gamma}}{\left[\frac{T_{12}}{T_0}\right] - 1}$$
(stage)

i) Wake blockage factor

$$\overline{K} = \frac{\sum_{i=\rho}^{n} \rho AV}{n} / \rho AV_{avg}$$

where n is number of tangential traverse points equally spaced across a stator gap and ρAV_{avg} is calculated from mass flow averaged values of P, p, and T at that radius

For stage efficiency, stage pressure ratio, and stator recovery see Appendix B.

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APPENDIX B

STAGE EFFICIENCY, STAGE PRESSURE RATIO, AND STATOR RECOVERY CALCULATION PROCEDURE FOR CORNER-BLOWING AND WALL-SUCTION ENDWALL BOUNDARY LAYER CONTROL TREATMENTS

The procedures used for calculating overall stage efficiency with the corner-blow, wall-suction, and combined corner-blow and wall-suction boundary layer control devices account for the flow that is added or extracted between the rotor inlet and stator exit. A schematic of the control volume used in the calculation procedure is shown in Figure 50. The various flows entering and leaving are shown for different conditions.

Overall stage efficiency is defined in the conventional manner

$$\eta_{\text{STAGE}} = \frac{\text{Ideal Work}}{\text{Actual Work}}$$

Ideal work is the net work required for all flow that reaches the stator exit, including the high-pressure blowing flow added at the stator endwalls. Actual work includes the rotor work done on the flow that reaches the stator exit and on the suction flow extracted at the stator inlet.

CORNER-BLOW STATOR CONFIGURATION

From Figure 51, the expression for calculating ideal and actual work used in the overall stage efficiency calculation is

$$\frac{\text{Ideal Work}}{T_{\text{INLET, AVG.}}} = \sum_{n=1}^{5} W_n C_p \left(\frac{T_{\text{IDEAL EXIT}}}{T_{\text{INLET, AVG.}}} - 1 \right)$$

The subscripts assigned to each of the flows entering or leaving the conical volume are defined in Figure 52. W is the measured flow rate into the compressor rotor (n = 1) or through a set of blowing nozzles (n = 2 through n = 5). The average total temperature resulting from adiabatic mixing of all flows entering the control volume $(T_{INIFT,AVG})$ is determined from

$$T_{\text{INLET, AVG.}} = \frac{\sum_{n=1}^{5} W_n T_n}{\sum_{n=1}^{5} W_n}$$

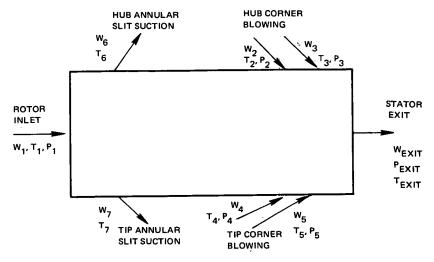


Figure 50 Control Volume for Compressor Performance Parameter Calculations

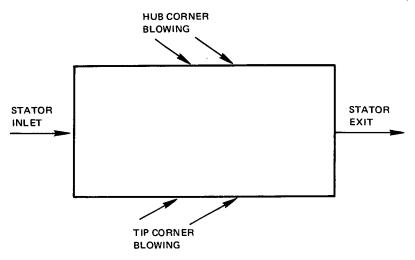


Figure 51 Control Volume for Stator Recovery Calculations

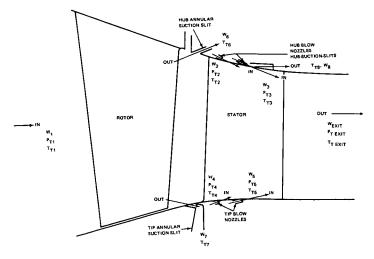


Figure 52 Control Volume for Corner Blow, Wall Suction, and Combined Boundary Layer Treatments

The ideal-exit total temp (T_{IDFAL EXIT}) is determined from

$$T_{\text{IDEAL EXIT}} = T_{\text{INLET, AVG.}} \left(\frac{Pt_{\text{EXIT}}}{P_{\text{INLET, AVG.}}} \right) \frac{\gamma - 1}{\gamma}$$

Pt EXIT is the mass flow averaged total pressure measured at the stator-exit during blowing. P INLET, AVG. is an average inlet total pressure resulting from an isentropic mixing of all flows entering the control volume. P INLET, AVG. is determined from rearranging the expression

Change in Enthalpy =
$$0 = \sum_{n=1}^{5} W_n \left[C_p \ln \frac{T_{INLET, AVG.}}{T_n} - R \ln \frac{P_{INLET, AVG.}}{P_n} \right]$$

to the equation

$$\ln P_{\text{INLET, AVG.}} = \frac{\sum_{n=1}^{5} W_n \left[\left(\frac{\gamma}{\gamma - 1} \right) \ln \frac{T_{\text{INLET, AVG.}}}{T_n} + \ln P_n \right]}{\sum_{n=1}^{5} W_n}$$

For n = 1, P_n is the measured inlet total pressure during blowing; for n = 2 through 5, P_n is the blowing nozzle exit total pressure obtained from the measured pressure in the blowing manifold and the calibrated value of $Pt_{NOZZLE}/Pt_{MANIFOLD}$ for each choked nozzle. For n = 1, T_n is the measured inlet plenum total temperature; and for n = 2 through 5, T_n is the measured nozzle plenum total temperature with blowing.

$$\frac{\text{Actual Work}}{T_1} = W_1 \text{ Cp} \left[\frac{T_{\text{EXIT}}}{T_1} - 1 \right]$$

 T_{EXIT} is the stator exit total temperature measured without blowing flow, and T_1 is the rotor inlet total temperature measured without blowing flow. Temperatures are taken at the same compressor operating point where data are taken without blowing flow.

Overall Stage Pressure Ratio =
$$\frac{P_{EXIT}}{P_{INLET, AVG}}$$

This is the value already calculated for Ideal Work.

Stator Total Pressure Recovery =
$$\frac{P_{EXIT}}{P_{STATOR EXIT, AVG.}}$$

 P_{EXIT} is the mass averaged stator exit total pressure during blowing as defined previously. $P_{\text{STATOR EXIT, AVG.}}$ is the isentropic average total pressure based on stator inlet main flow and on blowing flow conditions. It is calculated with the equation used previously to calculate ln values for $P_{\text{INLET, AVG.}}$ except that P_{1} and T_{1} are the mass average values for stator inlet values instead of rotor inlet.

WALL-SUCTION-STATOR CONFIGURATION

Ideal Work =
$$\left[W_1 - W_6 - W_7\right]$$
 $C_p \left[\frac{T_{IDEAL EXIT}}{T_1} - 1\right]$

where:

W₁ = measured compressor inlet flow and

W_{6.7} = measured I.D. and O.D. annular slit flow rates

$$\frac{T_{\text{IDEAL EXIT}}}{T_{\text{1}}} = \left(\frac{P_{\text{EXIT}}}{P_{\text{1}}}\right) \frac{\gamma - 1}{\gamma}$$

where $P_{\text{EXIT}}/P_{\text{1}}$ is the mass averaged overall stage total pressure ratio measured with wall suction.

$$\frac{\text{Actual Work}}{T_{1}} = \begin{bmatrix} W_{1} - W_{6} - W_{7} \end{bmatrix} C_{p} \begin{bmatrix} \frac{T_{\text{EXIT}}}{T_{1}} - 1 \end{bmatrix} + W_{6} C_{p} \begin{bmatrix} \frac{T_{6}}{T_{1}} - 1 \end{bmatrix} + W_{7} C_{p} \begin{bmatrix} \frac{T_{7}}{T_{1}} - 1 \end{bmatrix}$$

$$+ W_{7} C_{p} \begin{bmatrix} \frac{T_{7}}{T_{1}} - 1 \end{bmatrix}$$
Stator Total Pressure Recovery =
$$\frac{P_{\text{EXIT}}}{P_{\text{STATOR INLET}}}$$

 P_{EXIT} is the mass averaged stator exit total pressure with suction, and $P_{\text{STATOR INLET}}$ is the mass averaged pressure downstream of annular slits, not rotor exit pressure.

COMBINED CORNER-BLOW AND WALL-SUCTION CONFIGURATION

$$\frac{\text{Ideal Work}}{T_{\text{INLET, AVG.}}} = \left[W_1 + W_2 + W_3 + W_4 - W_6 - W_7 \right] C_p \left[\frac{T_{\text{IDEAL EXIT}}}{T_{\text{INLET, AVG.}}} - 1 \right]$$

The Ideal Work calculation is the same for blowing except for the subtraction of work done on suction flows. T $_{\text{INLET}}$ and $T_{\text{IDEAL EXIT}}$ are the same as defined by the equations for the corner-blow-stator configuration.

$$\frac{\text{Actual Work}}{T_{1}} = \left[W_{1} - W_{6} - W_{7} \right] C_{p} \left[\frac{T_{EXIT}}{T_{1}} - 1 \right] + W_{6} C_{p} \left[\frac{T_{6}}{T_{1}} - 1 \right] + W_{7} C_{p} \left[\frac{T_{7}}{T_{1}} - 1 \right]$$

All temperatures are measured with suction but without blowing at the same compressor operating points where data are taken with combined treatments.

Overall Stage Pressure Ratio =
$$\frac{P_{EXIT}}{P_{INLET,AVG}}$$

This ratio is calculated the same as for the blowing configuration where P_{EXIT} is the mass averaged stator exit total pressure with combined suction and blowing.

Stator Total Pressure Recovery =
$$\frac{P_{EXIT}}{P_{STATOR\ INLET,\ AVG.}}$$

The Pt_{STATOR INLET, AVG}. is the isentropic average based on stator inlet main flow and blowing flow conditions. It is calculated using the $P_{\text{INLET, AVG}}$ equation for the corner-blow-stator configuration with stator inlet flow $(W_1 - W_6 - W_7)$ instead of rotor inlet flow (W_1) ; P_1 and T_1 are the mass averaged stator inlet (downstream of annular suction slits) values in steady of rotor inlet values.

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APPENDIX C

BLADE ELEMENT AND PERFORMANCE DATA (Computer Printouts)

IDENTIFICATION OF ROTOR BLADE ELEMENT AND PERFORMANCE PRINTOUT HEADINGS

U-2 FT/SEC	°	M, 2	ູ ຫ ∑			
U-1 FT/SEC	2	Μ'-1	, α Σ			
VO'-2 FT/SEC	θ,\	M-2	δ.			
VO'.1 FT/SEC	٧, ه	₩-	& ¥			
V'.2 FT/SEC	, a >	EFF.P STATIC	ت و			
V'.1 FT/SEC	`»	EFF.AD	$\eta_{ m ad}$			
B'.2 DEGREE	β',	// EFF-P TOTAL	η p			
8'.1 DEGREE	. ra	P02/	986' 99 89 89 89 89 89 89 89 89 89 89 89 89			
B-2 DEGREE C	%	LOSS-P PROFILE	(ගි-යි _ක) cosp' _, 2			
B-1 DEGREE C	8 8	LOSS-P TOTAL	200000 2000000000000000000000000000000			
V0-2 FT/SEC D	β 6 ₉	LOSS-P OMEGA-B TOTAL	3			
VO-1		D-FAC	۵	EFF.P INLET	*	η_{p}
	8 0 ^	O-MEGA-B SHOCK	เล	EFF.AD INLET	×	$\eta_{ m ad}$
VM-2 FT/SEC	6E >	CAMBER	, g	PO/PO INLET		
VM-1 FT/SEC	8 >	TURN C. DEGREE D				യിം
V-2 FT/SEC	> ⁶		β	TO/TO INLET		卢마
V-1 FT/SEC	, & >	DEV E DEGREE	ွတ်			
DIA-2 IN	2r ₉	INCM DEGREE	 E			
	2,8	INCS % SPAN DEGREE	. <u>.</u> %			
DIA-1 % SPAN IN	5 15 30 30 70 70 85	% SPAN	5 10 15 30 70 70 85 90 95			

IDENTIFICATION OF STATOR BLADE ELEMENT AND PERFORMANCE PRINTOUT HEADINGS

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J.F.	ြိ	M, -2	Σ			
U-1 FT/SEC		M'-1	,M 01		_	
VO'.2 FT/SEC	۷, م	M-2	۶ -		D PO/PO	<u>-</u> 2
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V'.2 FT/SEC	` -	EFF.P STATIC	e sq		WBLOW PO/PO WTOTAL INLET ADJ.	wo 1-1-0
v'.1 FT/SEC	, > 10	EFF.AD	$\eta_{ m ad}$			WBLOW W
8'-2 Degree	β'11	2/ EFF.P 1 TOTAL	ε		WBLEED WTOTAL	WBLEED
B'-1 DEGREE	β′,0	PO2/ PO1	$\frac{(\overline{\omega}\cdot\overline{\omega}_h)\cos\beta'_{11}}{2\sigma} \frac{P_{11}}{P_{10}}$			
B-2 DEGREE	β11	LOSS-P PROFILE	(E) (E) (S) (S) (S) (S) (S) (S) (S) (S) (S) (S			
B-1 DEGREE	β 10	LOSS-P TOTAL	ώcosβ' ₁₁ 2 σ	1		
VO-2 FT/SEC	٧ ا	OMEGA-8	[3		WC/A-1 LBM/SEC SOFT	WVB SAgn
VO-1 FT/SEC	θ,	v-B D-FAC	۵		O EFF.P	η_{p}
VM-2 FT/SEC F	, 1 ₁₀	A OMEGA-B S SHOCK	3 ^{ta}	TERS	EFF.AD INLET %	$\eta_{ m ad}$
VM-1 V FT/SEC F	, v m10	CAMBER	•β 4	PARAMETERS	PO/PO INLET	0ء اح
V-2 VI FT/SEC FT		TURN DEGREE	84	STAGE	TO/TO INLET	卢무
	>	DEV DEGREE	8°11		WCORR INLET LBM/SEC	$\frac{\sqrt{w}}{\delta}$
DIA-2 V-1 IN FT/SEC	2'11 V ₁₀	INCM DEGREE	ت 10		INCORR INLET RPM	z 🎘
	2,10 2r,1	INCS DEGREE	- 10 - 10 - 10			
DIA-1 % SPAN IN	2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	% SPAN	. 01 02 03 05 05 05 05 05 05 05 05 05 05 05 05 05			

Rotor Pressure Ratio

ROTOR BLADE ELEMENT AND OVERALL PERFORMANCE AND DESIGN DATA

PLON M 31:SPEED CODE SO.POINT M 11:PAGE FT/SEC FT/	FUND 8 31:SFEED CODE 50:POINT 8 13:SFEED CODE 50:POINT 8 13:SFEED CODE 50:POINT 8 1		ROTOR ANGLES	46LES					ATRFC	TIL AERI	HANADO	AIRFOIL AERODINARIC SUMBANI	N L MAL LA			*	0019017			1 / 4 1 6 3
PHYSEC FT/SEC PEGREE DEGREE DEGREE FT/SEC FT	PHYSEC FYSEC PIGREE DEGREE FYSEC FT/SEC FT/S	Z	ASA ENGL	.15H (S	SPEC1AL)									S S	31.	SPEED C	00E 50,1	POINT	I PAGE	36.01
9427.5	7437.5 0 343.6 0 0 40.56 56.02 13.17 508.0 449.4 4421.3 -102.4 4121.5 -102.4 4121.5 -102.4 4121.5 -102.4 4121.5 -102.4 4121.5 -102.4 4121.5 -102.4 4121.5 -102.4 4121.5 -102.4 4121.5 -102.4 412.5 -102.4 4121.5 -102.4 4121.5 -102.4 4121.5 -102.4 4121.5 -102.4 4121.5 -102.4 4121.5 -102.4 4121.5 -102.4 412.5 -102.4 412.5 -102.4 412.5 -102.4 412.5 -102.4 412.4 412.5 -102.4 412.4 412.5 -102.4 412.4 412.5 -102.4 412.4	* SPA	NIN NIN		7/5EC F	V-2	1	VM-Z	VO-I	V0-2	B-1 GREE D	B-Z EGREE D	EGREE D	EGREE F	T/SEC F	7/SEC F	V0*=T" 1/SEC F1	70**2 [/SEC F1	Vel	7.8EC
9 427.6 .0 343.6 .00 38.77 57.02 19.16 531.0 453.1 445.4 -148.6 445.4 4 9 415.3 .0 315.4 .00 37.18 57.99 54.79 553.7 495.6 -348.2 1972.2 469.5 5 9 379.0 .0 249.9 .00 37.56 60.66 57.99 553.7 495.6 -348.2 1972.2 469.5 5 9 379.0 .0 249.9 .00 27.55 66.69 55.99 760.4 638.1 -698.3 -529.0 698.3 6 9 266.6 .0 148.2 .00 22.55 66.69 55.99 760.4 638.1 -698.3 -529.0 698.3 6 1 260.3 .0 142.2 .00 22.55 66.69 55.99 760.4 638.1 -698.3 -529.0 698.3 6 1 260.3 .0 142.2 .00 28.70 69.75 66.96 835.5 665.3 -769.0 -596.6 769.0 76	9427.6 .0 343.6 .00 38.77 57.02 19.16 531.0 453.1 -445.4 -148.6 5815.3 -192.2 415.3 .0 315.4 .00 32.56 60.6 37.82 617.4 495.6 -469.5 -192.2 3391.0 .0 193.5 .0 0 22.55 66.6 55.82 617.4 495.6 -588.2 -230.4 0 37.82 .0 193.5 .0 193.5 .0 0 22.55 66.6 55.9 760.4 638.1 -698.3 -522.0 331.2 .0 148.2 .0 0 22.55 66.6 55.9 760.4 638.1 -698.3 -522.0 296.6 .0 148.2 .0 0 22.55 66.8 55.9 760.4 638.1 -698.3 -522.0 296.6 .0 148.2 .0 0 22.55 66.8 55.9 760.4 638.1 -698.3 -522.0 296.6 .0 142.2 .0 0 22.55 66.8 55.9 760.4 638.1 -698.3 -522.0 296.6 .0 142.2 .0 0 22.55 66.8 59.8 622.1 666.6 -769.0 -596.6 .0 142.2 .0 0 22.55 66.8 9 55.9 760.4 638.1 -698.3 -522.0 .0 28.70 69.75 66.9 8135.5 665.3 -763.9 -612.0 .0 28.70 69.75 66.9 8135.5 665.3 -763.9 -612.0 .0 28.70 69.75 66.9 8135.5 665.3 -763.9 -612.0 .0 28.70 69.75 66.9 8135 .2756 .3754 .9 28.0 68.0 .0 0091 .0		5-17-46;		283.	-575.9-	٠	437.5	P.	374.5	00.	46:04	\$6.02	12:17	-308:0	1.6.	-421.3	102.4	421.3	4.4.4
915.3 0 315.4 00 37.18 57.99 24.79 553.7 458.6 6469.5 = 192.2 469.5 5 5 5 5 6 6 6 6 37.8 2 617.4 495.6 -538.2 = 304.0 538.2 5 5 5 6 6 6 6 5 5 6 5 6 5 5 6 5 5 6 5 6 5 5 6 5 6 6 6 6 5 5 5 6 6 6 6 5 5 5 6	915.3 0 315.4 0 0 37.18 57.99 24.79 553.7 458.6 -946.5 -192.2 304.0	_	196.81 0	7. 20,408	289.0	548.6	289.0	427.6	•	343.6	00.	38.77	57.02	19.16	531.0	453.1	-445.4	9.841-	445.4	492.2
391.0 .0 249.9 .00 32.56 60.66 37.82 617.4 495.6 -538.2 -304.0 538.2 5 374.1 .0 193.5 .0 193.5 .0 193.5 .0 193.5 .0 193.5 .0 193.5 .0 193.5 .0 193.5 .0 193.5 .0 193.5 .0 193.5 .0 193.5 .0 193.5 .0 193.5 .0 193.5 .0 193.5 .0 193.5 .0 193.5 .0 193.5 .0 194.2 .0 193.5 .0 194.2 .0 194.3 .0 194.4 .0 194.5 .0 194.	391.0 . 0 249.9 . 00 32.56 60.66 37.82 617.4 495.6 -538.2 -304.0 374.1 . 0 193.5 . 00 27.33 63.83 48.40 693.1 364.2 -622.1 -422.0 25.64 55.64 55.04 65.01 -594.1 -698.3 -592.0 148.2 . 00 23.13 68.80 60.38 804.6 670.1 -754.8 -582.3 256.9 . 0 142.2 . 00 25.63 69.30 63.54 822.1 666.6 -769.0 -592.0 256.3 69.30 63.54 822.1 666.6 -769.0 -592.0 256.3 69.30 63.54 822.1 666.6 -769.0 -592.0 256.3 -793.7 -793.8 8477 -253.7 -612.0 25.00 28.70 69.75 66.96 835.5 665.3 -773.7 -612.0 25.00 28.70 69.75 66.96 835.5 665.3 -773.7 -612.0 270.0 28.88 -0691 -0178 1.1894 .9377 .9360 .8283 .2653 -4898 -0000 .3078 .0078 .0179 1.1074 .9175 .9169 .8283 .2253 .4898 -2000 .3078 .0194 .0194 .11943 .88650 .8835 .7975 .2737 .4135 .0000 .2706 .0684 .0139 .0194 1.1443 .88650 .8835 .7975 .2756 .3744 .0000 .2259 .0480 .0001 1.0091 1.1026 .8777 .8778 .8778 .8319 .2756 .3754 .0000 .2252 .1383 .0263 .0263 1.0617 .5052 .5007 .5009 .2620 .2252	- 	5 19,467	7 21.047	293.5	521.6	1	415.3	0.	. 915.4 ··	00.	37,18	- 57,99-	24.79	-553.7-	-9-85h		-192.Z	-469.5	- 507 . 6
354.6	374.1 . 0 193.5 . 00 27.33 63.83 48.40 693:1 564.2 -622.1 -422.0 1956.6 . 0 148.2 . 00 22.55 66.69 55.99 760.4 638.1 -698.3 -529.0 256.5 . 0 142.2 . 00 23.13 68.38 809.6 66.6 -769.0 -596.6 266.3 . 0 142.2 . 00 25.13 68.30 60.38 809.6 666.6 -769.0 -596.6 266.3 . 0 142.2 . 00 25.63 66.30 63.54 822.1 666.6 -769.0 -596.6 260.3 . 0 142.2 . 00 28.70 69.75 66.96 815.5 665.3 -763.9 -612.0 0 142.2 . 00 28.70 69.75 66.96 815.5 665.3 -763.9 -612.0 2600 . 2888 . 0891 . 0149 . 0149 1.2046 . 9540 . 9528 . 8477 . 2573 . 912.0 . 0000 . 3145 . 0000 . 3145 . 0194 . 0194 1.144 . 8860 . 8835 . 7975 . 2737 . 4898 . 0000 . 2706 . 0684 . 0139 . 0194 1.144 . 8860 . 8835 . 7975 . 2737 . 4135 . 0000 . 2706 . 0684 . 0139 . 0194 1.144 . 8860 . 8835 . 7975 . 2737 . 4135 . 0000 . 2259 . 0480 . 0001 . 0001 . 1002 . 3144 . 6178	•••	0 22.314	1 22.964	302.4	464.1		391.0	•	249.9	00.	32,56	99.09	37,82	617.4	495.6	-538.2	-304.0	538.2	553.9
356.6 0 148.2 00 22.55 66.69 55.99 760.4 638.1 -698.3 -529.0 698.3 6 296.6 1 148.2 00 23.13 68.80 60.38 809.6 670.1 -759.8 -582.3 754.8 1 266.9 0 142.2 00 28.50 69.30 63.5 1 666.6 -769.0 -596.6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	356.6 . 0 148.2 . 00 22.55 66.69 55.99 760.4 638.1 -698.3 -529.0 296.9 . 0 141.1 . 00 23.13 68.80 60.38 809.6 -670.1 -754.8 -582.3 296.9 . 0 142.2 . 00 25.63 69.30 63.54 822.1 666.6 -769.0 -596.6 . 256.3 . 0 142.2 . 0 28.70 69.75 66.96 835.5 665.3 -763.9 -612.0 0 28.70 69.75 66.96 835.5 665.3 -763.9 -612.0 0 28.70 69.75 66.96 835.5 665.3 -763.9 -612.0 0 28.70 69.75 66.96 835.5 665.3 -763.9 -612.0 0 28.70 69.75 66.96 835.5 665.3 -763.9 -612.0 0 28.70 69.75 66.96 835.5 665.3 -763.9 -612.0 0 28.00 0.3038 0.081 0.0178 0.0178 1.0174 0.954 8835 0.9149 0.8048 0.263 0.9139 0.01	1	0 25.79	1.25,520	305.7	421.3	4	374.1	0.	193.5	00.	27,33	63,83	- 48 .4Q-	693:1-		-	-422.0	622:1-	615.5
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1 260.3 0 142.2 0.00 28.70 69.75 66.96 835.5 665.3 -763.9 -612.0 783.9 7 7 9.00	1 260.3 ,0 142.2 ,00 28.70 69.75 66.96 835.5 665.3 -783.9 -612.0 OHEGA-8 D-FAC OHEGA-8 LOSS-P LOSS-P PO27 EFF-P EFF-AD EFF-P H-1 H-2 SHOCK TOTAL PROFILE POI TOTAL TOTAL STATIC STATIC TOTAL STATIC ST	ď	31.88	30.630	290.6	327.2	290.6	296.9	0	142.2	00.	25,63	69,30	63,54	822.1	9.999	- 169.0 -	-596.6	769.0	738.8
OHEGA-B D-FAC GHEGA-B LOSS-P LOSS-P PO27 EFF-P EFF-AD EFF-P H-11 H-2 H*-1 H S-HOCK SHOCK 0000 2808 0691 0178 0179 1:2046 9546 9558 8477 2573 55146 9679 9 0000 3003 0814 0178 0178 1:1894 9377 9360 8283 2624 9898 9679 91000 3008 0814 0178 0178 1:1894 9377 9960 8835 2624 9689 9679 91000 2008 0814 0178 0178 1:1894 9377 9960 8835 7775 2624 9689 9689 9689 9680 8835 7775 2670 3378 9689 9689 9775 97000 2259 0099 1:1821 8775 8775 8775 8775 3776 9378 9319 2776 9369 9789 9776 9776 9776 9776 9776 9776 97	0HEGA-B 0-FAC CHEGA-B LOSS-P LOSS-P PO2/ EFF-P EFF-AD EFF-P H-1 H-2 5HOCK 5HOCK 20000 .2888 .0891 .0149 .0149 1.2046 .9540 .9528 .8477 .2573 .5146 7 .0000 .3038 .0841 .0178 .0178 1.1894 .9377 .9360 .8283 .2624 .4898 7 .0000 .3048 .0911 .0194 .0194 .11443 .8860 .8835 .7975 .2737 .4135 8 .0000 .2706 .0684 .0139 .0139 1.1221 .8775 .8753 .8135 .2756 .3754 .0000 .2259 .0480 .0091 .0199 1.1221 .8775 .8778 .8753 .8135 .2756 .3754 .0000 .2257 .0918 .0159 1.1026 .877 .8778 .878 .8319 .2708 .3494 .0000 .2252 .0393 .0263 1.0617 .5052 .5007 .5009 .2620 .2630		5 32,49	31.271	289.1	296.6	289.1	260.3	•	142,2	00.	28,70	. 64.75	. 96.99	835.5	~	-183.9-	-612.0	-783.9	754.2
2 HOCK	SHOCK		•	7	7.6	NO.				1.0.4.0.1	9	- 9-50						7.8		7.0
2 0000 2008 0691 0149 0149 1.2046 9540 9528 6447 2573 55146 94690 96528 0800 2003 2024 4898 4879 9000 2000 2003 0814 0178 1.1894 9977 9949 8048 2663 4689 91000 2000 20145 08911 00194 01194 1.1843 8865 8835 7775 2705 2705 11974 01194 1.1843 8865 8835 7775 2705 2705 0194 1.1843 8865 8875 8775 8775 8775 8775 8775 8775	2 0000 2888 0691 0149 0178 1.1246 9540 9528 8477 25573 5146 9600 3038 08447 22573 5146 9640 9528 8477 25573 5146 9659 0000 3038 0814 0178 1.189 9377 9169 82643 2662 4898 1 0000 3145 08947 0207 1.0743 9169 9169 9149 8048 2663 4653 1 0000 3078 0911 0199 1.1443 8860 8835 7775 2737 9135 1 0000 2706 0689 0139 1.1221 8875 8758 8758 8135 2756 3759 1 0000 2259 0980 0091 1.0026 8877 8778 8773 8135 2756 3759 1 0000 2252 1383 0229 1.0515 1.0026 8178 6133 5742 2640 3265 1 0000 2522 1383 0229 1.0517 1 0617 5052 5007 5009 2267 22630	% SPA	N. DEGEN	10 10 10	FAREE DE				יא יין	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7 4 7	2023-F	100	DIAI	OTALS	1411		ı •		•
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30 2.91 6.80 7.98 22.84 24.03 .0000 .3078 .0911 .0194 .0194 1.1443 .8860 .8835 .7975 .2737 .4135 .5664 . 50 4.33 6.90 6.12 15.43 14.67 .0000 .2706 .0684 .0139 .0139 1.1221 .8775 .8753 .8135 .2756 .3754 .6313 . 51.25 7.03 5.18 10.70 8.84 .0000 .2259 .0480 .0001 1.1026 .8797 .8778 .8319 .2708 .3444 .6893 . 51.25 7.03 5.18 10.70 8.84 .0000 .2245 .0180 .0105 .0105 .0105 .0174 .6178 .2172 .2620 .2925 .7415 . 50 5.46 6.69 5.55 7.54 5.73 .0000 .2542 .1383 .0229 1.0617 .5052 .5007 .5007 .2607 .2630 .7525 .	30 2.91 6.80 7.98 22.84 24.03 .0000 .3078 .0911 .0194 .0194 1.1443 .8860 .8835 .7975 .2737 .4135 . 50 4.33 6.90 6.12 15.43 14.67 .0000 .2706 .0684 .0139 .0139 1.1221 .8775 .875 .875 .875 .2756 .3754 . 70 5.25 7.03 5.18 10.70 8.84 .0000 .2259 .0041 .0091 1.1026 .877 .877 .877 .878 .8319 .2708 .3494 . 85 5.46 6.49 6.55 7.5 6.73 .0000 .2542 .1383 .0259 1.0417 .5052 .5007 .5009 .2607 .2630 .	. =	19.1		12.01	33.20	37.74	0000	3145	2460	.0207	.0207	1.1743	6916	6616	;•	. 2663		- \$006	-1404
60 4,33 6,90 6,12 15,43 14,67 ,0000 ,2259 ,0480 ,0139 ,0139 1,1221 ,8775 ,8753 ,8135 ,2756 ,3754 ,6313 . 70 5,25 7,03 5,18 10,70 8,84 ,0000 ,2259 ,0480 ,0091 ,0091 1,1026 ,8797 ,8778 ,8319 ,2708 ,3444 ,6893 . 85 5,46 6,69 5,52 8,43 7,26 ,0000 ,2345 ,0918 ,0165 ,0165 1,0881 ,7471 ,7436 ,6817 ,2640 ,3255 ,7273 . 80 5,49 6,56 7,54 5,75 6,73 ,0000 ,2522 ,1383 ,0229 1,0744 ,6178 ,6133 ,5742 ,2620 ,2725 ,7715 . 81 5,49 6,56 7,54 5,79 6,38 ,0000 ,2671 ,1770 ,0263 ,0263 1,0617 ,5052 ,5007 ,5009 ,2607 ,2630 ,7525 .	60 4,33 6,90 6,12 15,43 14,67 ,0000 ,2706 ,0084 ,0139 ,0139 1,1221 ,8775 ,8753 ,8135 ,2756 ,3354 , 70 5,25 7,03 5,18 10,70 8,84 ,0000 ,2259 ,0480 ,0009 1,1026 ,8797 ,8778 ,8319 ,2708 ,3444 , 85 5,49 6,59 7,52 8,43 7,26 ,0000 ,2345 ,0165 1,0881 ,7471 ,7435 ,6817 ,2640 ,3205 , 86 5,49 6,59 7,59 6,38 ,0000 ,2522 ,1383 ,0229 ,0229 1,0774 ,6178 ,6133 ,5742 ,2620 ,2630 , 87 5,55 6,46 10,04 2,79 6,38 ,0000 ,2671 ,1770 ,0263 ,0263 1,0617 ,5052 ,5007 ,5009 ,2607 ,2630 ,	ň	2.91		7.98	22.84	24.03	0000	3078	1160.	4610.	+610.	1.1443	.8860	.8835	.7975	.2737	. 4 1 35	.5664	9144.
70 5,25 7,03 5,18 10,70 8,84 .0000 .2259 .0480 .0091 .0091 1,1026 .8797 .8778 .8319 .2708 .3444 .6893 .85 5,46 6,69 5,52 8,43 7,26 .0000 .2345 .0918 .0165 .0165 1,0881 .7471 .7436 .6817 .2640 .3265 .7273 .8745 .88 5,49 6,56 7,54 5,75 6,73 .0000 .2522 .1383 .0229 1.0744 .6178 .6133 .5742 .2620 .2925 .7415 .88 5,49 6,54 10,04 2,79 6,38 .0000 .2671 .1770 .0263 .0263 1.0617 .5052 .5007 .5009 .2607 .2607 .2617 .7525 .	70 5,25 7,03 5,18 10,70 8,84 ,0000 ,2259 ,0480 ,0091 ,0091 1,1026 ,8797 ,8778 ,8319 ,2708 ,3444 ,85 5,46 6,69 5,52 8,43 7,26 ,0000 ,2345 ,0918 ,0165 ,0165 1,0881 ,7471 ,7436 ,6817 ,2640 ,3205 80 5,49 6,56 7,54 5,75 6,73 ,0000 ,2522 ,1383 ,0229 ,0229 1,0744 ,6178 ,6133 ,5742 ,2620 ,2725 80 5,49 6,46 10,04 2,79 6,38 ,0000 ,2671 ,1770 ,0263 1,0617 ,5052 ,5007 ,5009 ,2607 ,2630 95		i	-	6.12	15.43	14.67	0000	.2706	.0684	.0139	.0139	1.1221	8775	8753	. 8135	5126	-3754	-6313-	-, 5028-
85 5,46 6,69 5,52 8,43 7,26 ,0000 ,2345 ,0918 ,0165 ,0165 1,0881 ,7471 ,7436 ,6817 ,2640 ,3255 ,7273 ,895 5,49 6,56 7,54 6,13 ,574 2,79 6,38 ,0000 ,2671 ,1770 ,0263 ,0063 1,0617 ,5052 ,5007 ,5007 ,2607 ,2607 ,2630 ,7525 ,	85 5,46 6,69 5,52 8,43 7,26 ,0000 ,2345 ,0918 ,0165 ,0165 1,0881 ,7471 ,7436 ,6817 ,2640 ,3265 , 80 5,49 6,56 7,54 5,75 6,73 ,0000 ,2522 ,1383 ,0229 1,024 ,6178 ,6178 ,6133 ,5742 ,2620 ,2725 , 85 5,49 6,56 7,54 5,79 6,38 ,0000 ,2671 ,1770 ,0263 ,0263 1,0617 ,5052 ,5007 ,5009 ,2607 ,2630 ,	*	5,25	7.03	5.18	10.70	8.84	0000	,2259	.0480	.0091		1,1026	.8797	8778	.8319	.2708	3444	6883	.5690
80 5,49 6,56 7,54 5;75 6,73 ,0000 ,2522 ,1383 ,0229 1,0744 ,6178 ,6133 ,5742 ,2620 ,2925 ,7415 , 855,556,46 10,04 2,79 6,38 ,0000 ,2671 ,1770 ,0263 ,0263 1,0617 ,5052 ,5007 ,5009 ,2607 ,2610 ,7525 ,	80 5,49 6,56 7,54 5;75 6,73 ,0000 ,2522 ,1383 ,0229 1,0744 ,6178 ,6133 ,5742 ,2620 ,2925 ; 85 5,55 6,46 10,04 2,79 6,38 ,0000 ,2671 ,1770 ,0263 ,0263 1,0617 ,5052 ,5007 ,5007 ,2607 ,2630 ;		5.46	69.9	5.52	8.43	7.26	0000	2345	8160	-0165	:_	1.0881	7471	7436	-4189	2640	3205	:7273	. 5968
85 - 5.55 6.46 10.04 2.79 6.38 .0000 .2671 .1770 .0263 .0263 1.0617 .5052 .5007 .5007 .2607 .2607 .2630 .7525 .	855.556.46i0.04 2.796.380000267i177002630263 .061750525007500726072630	đ	5,45	6.56	7.54	5:75	6.73	.0000	.2522	.1383	.0229		1.0744	.6178	.6133	.5742	.2620	.2925	:7415	.5921
		8	5,55	i	10.04	~	6.38	0000	.2671	1770	.0263	.0263	1.0617	. 5052	.5007	. 5004	.2607	.2630	. 7525	5898

TG/TO PO/PO EFF-P INLET INLET INLET 1.0406 1.1273 85.84 86.10

ROTOR ANGLES	2				AIRFO	IL AERO	DYNAMIC	AIRFOIL AERODYNAMIC SUMMARY PRINT	RY PRIN		-		23:00:40		JULY 1251971	17974
NASA ENGLISH	(SPECIAL)	2								₹ 20	31,	SPEED C	31'SPEED CODE SO,POINT	POINT .	2,PAGE	36.01
DIA-I	1-A Z-Y	2=1	L	VM-2	1-01	V0-2 8-1	1-8	8-2	1=18	82	I-A	1 - 0 A 2 - A	101	Z=+0A	1-5	7.0
X SPAN IN IN	N IN FT/SEC FT/SEC	FT/SEC F	SEC	T/SEC FI	FT/SEC FT/SEC FT/SEC DEGREE DEGREE DEGREE DEGREE FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC	15Ec DE	GREE DE	GREE DE	GREE D	EGREE F	T/SEC F	T/SEC F	1/SEC F	T/SEC F	T/SEC FT	/SEC
487	1	3 558 .9	268.3	408.8	P.	381.1	00.	66.24	57.54	13.26	4.46	ZOOD	4Z0.0-421.8-420.5	2000	421.0	1
18.467		273.1 528.6 2	273.1.	394.8	•	351,5	00.	41.67	58.52	19.69	522.9	419.7	0.954-	C . [b l =	0.94	472.B
19.467 21	1	3 504.4	277.3	385.0	0.	325,7	00	40.20	59.47	75.32	-8.5.6	426.9	426.9 -470.1 -182.	-182.6-	-470-1-	508:3-
	22,964 285.7	_	285.7	365.2	0	266.9	00.	36.14	62.06	38,19	606.6	465.2	465.2 -538.9 -287.	-287.7	538.9	554.6
_	25,520 289.0	* 60h	289.0	346.4	0	216.1	00	31.95	65.11	80.46	989.	-529.4.	686.6 529.4 -622.8 -400.	- 400+-	. 9.229	616.3
		3 377.1	284.8	333.4	•	176.2	00.	27,85	67.83	56,37	755.0	602.6	602.6 -699.2 -501.8	-501.8	699.2	678.0
مأ	29,993 277.9	356.8	277.9	311.8	0.	173.5	00.	29.09	18.69	66.48	2:508	633.7	433.2 -755.8 -551.0	-5515G-	-755.8	-7243
90 31,883 30	30,630 276.0	335,3	276.0	285.1	0	176.4	00.	31.79	70.28	63,16	817.9	631.5	631.5 -770.0 -563.3	-563.3	170.0	739.7
- 85 32,499 31	31.271 274.4	316.1	274.4	260.7	0.	176.8		34.16	70.73	-65.73	831°4	634.5	634.5 -784.8 -578.	-578.4		755.2
													•			-
INCS	INCS INCH DEV TURN CAHBER	TURM .		MEGA-B	OMEGA-B D-FAC OMEGA-B LOSS-P LOSS-P	EGA-B'L	1. d-SSO	.d-SS0	P02/	EFF-P EFF-ADEFF-P	FF-A0-		H-1-H	H-2	-H1-H2-	H-2-H
MSPAN DEGREE DEGREE DEGREE DEGREE	REE DEGREE	DEGREE (SHOCK	TOTAL PROFILE	10	TAL PF		P01 T	POI TOTAL TOTAL STATIC	OTAL S	TATIC		į		
5 2,23	8,66-13,0	44:28	48:85	0000	-339Z	.0820	-0134	ı	.2103	-6096	9656		1	2430 . 4984	***	-37.46
2.64	_	_	43,39	.0000	3606	.0874	.0191		1.1940	.9364	.9347	.8467	. 2477	6026	4800	.3738
3,06	8,72 12,55		37.76	0000	1	1	.0205	_	1817	.9222	. 9202	.8348	. 2513	4489	*10S*	3800
4.28		.4	24.03	0000	.3569		•0184	.0184	1.1575	.004	.8982	.8328	.2583	. 4021	.5586	.4135
	8.16 6.79	16:03	99.41	.0001	3244	.0769	.0154		1:1374	.8785	.8760	8228	. 2604	.3628	06240	4104
6.36	8,15 5,56	11.	8.86	.0000		1650	0111		1.1224	.8766	.8743	.8362	. 2565	1326.	.6826	5355
94.9	7.71 5.6.	3 9.32	7.26	0000	2905	1036	9810	0186	1.1122	7887	7647	.7150	. 2507	.3164	-1236	-5195
Z++9 06	5 7	7 12	6.76	0000		.1436	.0241	.0241	1.1029	.6817	.6767	.6352	.2488	.2968	1987	.5589
15.4	7,43 8,80	00.5	6.38	0000	.3159	.1716	.0268	.0268	1.0948	99190	6019.	. 5841	2474	.2784	.7477	. 5607
		T0/T0 66/780		EFFEAR FFFE	9											
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	- !	1.0452 1.1433	- 1	86.39 86,	86.67											

ROTOR ANGLES	פרבצ					7 1 K L	JIL AER		AIRFOLD AEROGINAMIC SCHMANT PRIN		-						
NASA ENGLISH	SH	(SPECIAL)	_								NO.	-	31. SPEED C	CODE 50. POINT	POINT #	# , PAG	4,PAGE 36.01
SPANIN 1	D1A-2	FT/SEC FT/SEC FT/S	77/5EC #	TVSEC F	T/SEC F	EC F1/SEC F1/SEC F1/SEC DEGREE DEGREE DEGREE F1/SEC F1/SEC F1/SEC F1/SEC F1/SEC F1/SEC	V6-2	B-1 EGREE D	B-Z EGREE D	EGREE D	BY-Z EGREE F	7/SEC F	7/5EC F	1/5EC F	7/SEC F	1/5EC F	U=2 1/5EC
5 17.467	19.769	258	557.5	1	393.0	9	388.3	00.	44.66	58.56	12.85	0.544	1030	£ 22h=	1.68	22.3	0.84
10 18.467	20.406	262.7	523.8		381.2	•	354.1	00.	43:58	54.52	14.40	516.1		0	M	0 1	7
15 19:467:21:04	21.047	286.8	9.864	266.8	370.1	0.	334:1	00.	42.05	-90.42	25.24	241.0		-470.7	-174.8	-4.0.4	208
30 22,314	22.964	274.7	443.9	274.7	345.0	•	279.2	00.	38,97	43,00	38.61	605.4	442.1	539.5	-276.0	539,5	555.2
50 -25.791	25,520	277.8	.9°50h	- 277.8	332,8	0.	231.7	.00	34,83		- # P . 1 4	-9.289-	-509.3"	623.6"-385	-385.3	623.6	-617.0-
70 28.954	28,076		373.3	273,7	319.1	•	193,5	00.	31,22	68.63	56.63	751.7	580.9	-700.0 -485.	-485.3	700.0	678.8
١.	29.993	7.67	353:3	767:1	293.5	0.	196.5	00.	33,81	70.55	-96:09-	905.4	-604:1	404.7 - 756.6 - 528	-528.6	156.6	-1.552
31,883	30,630	265.3	336.2	265,3	272.3	0	200.4	8	36,38	71.00	63.24	815.2	605.0	605.0 -770.8 -540.	-540.1	770.8	7 +0 .5
96 32:499		. 263.8	324.4	263.8	254.5	0.	201.1	-00	38.34	-71;44 65,36	65.36	828.8	828;8 610,5 4,9	.785.7	6.4.65.	-785.7-	756:0
		TACS INCH DEV TON CARS	102	4 1	H L C A P B	A CALLER DEFAUL CHICANE COUNTY TO THE TAIL TO THE TAIL TH	1864931	1000	41.000	1001				E	i . E		
*SPANDEGREE DEGREE DEGREE	DEGREE	DEGREE L	8		E SHOCK		Ĕ,	TOTAL P	PROFILE	POI TOTAL	DTAL T	TOTALS	STATIC				1
5 3,25	89.6	89.21 89.6	1201	48.82	0000	3701	0150.	0110	0110 1.2169	1.2169	0494	1966	PC V	2337	1246	44518	1450
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15 4.05	1	2.46	35.22	. 37,75	0000	3965	.0835	.0182	.0182	1 1 8 9 5	9339	. 932F	.8635	1142.	. 4433	144	30.40
30 5.22	Ī	8.76	24.39	24.03	.0001	.3959	.0958	.0202	.0201	1.1646	.8965	. 8941	.8328	.2482	.3940	.5542	. 3923
İ		48.9	16,84		+000	1569	.0791	- 9510	.0157	171490	8845	8820	8361	-2052-	3597	6619	4517
			12+00	8.86	.0002	3131	.0672	.0126	.0125 1.1345	1,1345	.8731	8705	.8340	5469	.3310	64143	2515
85 7.21	8.46	9.10	09.6	7.26	1000	3338	-1254	.0222	.0222 1.1252	1-1252	.7532	-1486	-2002	2403	+21C+	120+	12347
90 7.20	8.28	7,27	7:76	6.77	.0001	.3475	.1596	.0267	.0267	1.1189	.6891	.6836	.6399	,2391	.2986	.7329	.5341
	8	8.43	60.0	6.38	1000	.3537	1816	.0287	.0287	7,1135	0649	. 6380	.6020	-2377-	. 286U	7448-	5385
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		-	1.0484 1.1540	_	84.34 86	86.63											
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BOTDS INE FE	7
(SPECIAL)	RUN # 31,5
Tale 2-8 1-8 Z-00 I-00 Z-MV I-00 Z-00 I-00 Z-00 I-00 Z-00 I-00 I-00	nest mess verse reverse reverse reverse reverse reverse reverse
F1/3EC F1/3EC F1/3EC	GATE T-VARE T-VA
78-51 11.00 £3-94 00 8-245 0 0-146 5-245 4 00-15-5-2	280.52.0.22.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.
8 246.7 514.7 246.7 364.2 ,0 364.0 ,00 44.78 61.03 17.51	27.0
	0-389.2-470.3-168.0-470.3-
2,314 22,964 257,9 432,3 257,9 320,4 ,0 290,1 ,00 42,15 64,42 39,51	6 415,8
91.25.520. 260.4 400.0 260.4 313.0 313.0 249.0 34.50 38.50 67.32 49.54	.5 -623.1
8,954 28,076 255.7 370.6 255.7 299.0 ,0 219.0 ,00 36.21 69.91 56.91	69.91 56.91 744.8 548.2 -699.5 -459.3 699.5 678.3
249.0 351.5 249.0 263.7 61.82	796.0 558.5 - 756.1 - 492.3 - 756.1
1,883 30,630 247,3 341,9 247,3 247,6 ,0 235,8 ,00 43,62 72,20 63,85	
31.271 245.7 331.4 245.7 232.2 0 236.5 00 45.53 72.61 65.89	i
*SPANDEGREE DEGREE DEGR	
ANT 14/78 10 16 10 10 10 10 10 10 10 10 10 10 10 10 10	41-19878
7 1000 1000 1000 1000 1000 1000 1000 10	9810 9804
5.54 11.15 12.81 36-33 37.72 .000. 4297 .0548 .0119 .0119 101989 .9587	9587 9576 9167
6.64 10.54 9.67 24.92 24.03 0007 4368 0883 0184 0182 101740 9102 o	. 9102 . 9080 . 8590
10.37 7.26 17.78 14.67 .0011 39.68 .0785 .0155 .0153 1.1627 8952	8952 8928
8,45 10,23 6,10 13,00 8,84 ,0006 ,3622 ,0854 ,0158 ,0157 1,1504 ,8592	•
6.96 9.95 7.26 0003 04025 1682 0290 0289 101421 721	.7211 .7153 .6634 .2243 .3096
. 4976, 4118 100, 8318 0318 1,138 4 , 474,	.6794 .6730 .6236
.4158 .2123 .0329 .0328 1.1346 .6471	
70/10 P0/P0 EFF-P	
INLET INLET INLET	
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ROTOR BLADE ELEMENT AND OVERALL PERFORMANCE AND DESIGN DATA

FINE CIT AIRFOIL AERODYNAHIC SUMHARY PRINT RUN
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TO/TO PO/PO EFF-A EFF-P INLET
152

ROTOR ANGLES NASA ENGLISH CSPAN IN 1N FT/SEC FT/S 10 18,467 20,408 421,3 779 10 18,467 20,408 421,3 779 10 18,467 21,047 428,2 72 10 22,314 22,864 443,1 65 10 25,791 25,520 449,8 579 10 25,791 25,520 449,8 579 10 25,791 25,520 449,8 579 10 25,791 25,520 449,8 579 10 25,791 25,520 449,8 579 10 25,791 25,520 449,8 579 10 25,791 25,520 449,8 579 10 25,791 25,520 449,8 579 10 25,791 25,520 442,7 10 25,791 25,520 442,7 10 25,791 25,520 443,1 65 10 27,79 21 35 10 3,22 5,61 4,42 10 10 3,22 5,60 5,40 12,23 10 4,22 5,60 5,40 5,10 10 4,52 5,56 8,75 2
A ENGLISH A ENGLISH DIA-1 (SPECIAL) IN FT/SEC FT/SEC FT/SEC 17,467 19,769 4121.2 797.4 413. 18,467 20,408 4121.2 727.5 428. 19,467 21,047 428.2 727.5 428. 22,314 22,964 443.1 650.6 443. 25,791 25,520 449.8 597.8 449. 28,991 22,944 447. 28,991 20,040 443.1 650.6 443. 28,991 22,991 42.7 549.8 447. 28,991 21,291 42.5 436.3 425. 28,999 31,271 425.2 436.3 425. 28,499 31,

10/10 PO/PO EFF-AD EFF-P INLET INLET INLET INLET 1.0842 1.2722 84.60 85.11

ROTOR BLADE ELEMENT AND OVERALL PERFORMANCE AND DESIGN DATA

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7 1 1 2 1 1 2 1 1 2 1 2 1 2 1 2 1 2 1 2	• •
20LY Z-197 # 4-PAGE 34-0 # 7.5EC F 1/5EC 623-0 623-	1.0349
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7.52;33 7.52;33 7.52;4 7.52;4 7.53;6	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
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11.5P	
31 7/SEC F 7301-0 7301-0 7301-0 1055-0 11055-0 11143-4 11162-3 11143-4 11162-3 11143-4 11162-3 11055-0	6913 6453
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55 59 57 59 59 59 59 59 59 59 59 59 59 59 59 59	
AIRFOLL AERODYNAMIC SUHHARY PRINT RUN # 31,5PEED CODE 70;POINT # 4,PAGE 36.00 E FT/SEC FT/SEC DEGREE DEGREE DEGREE FT/SEC FT/S	0327
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0 -9 × 8 × 9 × 7 × 7 × 7 × 7 × 7 × 7 × 7 × 7 × 7	EFF-P
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KSPAN DIA-1 DIA-2 V-11 VH-2 VD-1 VD-2 DB-1 BB-2 VB-1 DIA-1 DIA-2 V-1 VD-2 VD-1 VD-2 DB-1 BB-2 VB-1 DIA-2 V-1 DIA-2 V-1 VD-2 VD-1 DIA-2 V-1 DIA-2 VD-1 DIA-2 V-1 DIA-2 VD-1 DIA-2 VD-1 DIA-2 V-1 DIA-2 VD-1 DIA-2 DIA-2 DD-1	
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RETOR ANGLES NASA ENGLISH NASA ENGLISH 10 18,467 19,10 18,1467 19,10 18,467 19,10 28,14 22,10 28,10	3 8 8

ROTOR BLADE ELEMENT AND OVERALL PERFORMANCE AND DESIGN DATA

ROTOR BLADE ELEMENT AND OVERALL PERFORMANCE AND DESIGN DATA

ROT	ROTOR ANGLES	23	•				ATR	OTC AER	PODYNAMI	AIRFOIL AERODYNAMIC SUMMARY	RY PRIN				8:32:18		4700	146716
NASA.	NASA ENGLISH (SPECIAL)	48)	EC1AL)									* X O X	31.	SPEED C	31.SPEED CODE 70.POINT	POINT *	6 , PAGE	36.01
	DIA-1 DIA-2 Val Val	I A = Z	1=1	V=2	VH-1	VH-2	1-01	V0=2	8-1	2-8	8	8.=2	1=0	Z=1A	1=404	Z=+0A	1-0	2.0
MSPAN IN	<u>z</u>	ī	VSEC. F	T/SEC F	1/SEC	FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC DEGREE	TISEC F	1/SEC 0		EGREE D	EGREE D	EGREE F	DEGREE DEGREE DEGREE FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC	T/SEC F	T/SEC F	1/5EC F	T/SEC F	r/SEC
-	17.467 705.71	4.769	333.6		333.6	479.5	þ	564.4	00.	49.65	80.55	12.21	678.6	0.06	\$0.65- B.06	P. P.	-	
91	18,467.20,408	904.0	340.1	710.9	340.1	477.0	•	527.0	00.	47.84	61.43	18.90	711.3	504.7	-624.7	-163.3	624.7	4.069
	19.467 2	21.047	345.6	677.4	345.6	458.0	0.	499.2	000	47,46	62,30	24.92	743:7	2.905	6.88.9.	-212.8	658.5	712.0
8	•	22.969	355.5	608.8	355.5	415,1	•	441.2	00.	46.74	64.77	38,90	834.4		-754.B	-335.6	754.8	776.8
2 98	_	25,520"	357.5		357,5	381.3	0.	396.7	00	. b1 . 9 h	-67.72	50.72	942.9	- 602.7-	-812.5-	-466:6-	-872.5-	-863:3-
82	28.954 26	28.076	351.0	540.8	351,0	374.2	•	390.5	00	46.22	70.27	56.20	1040.5	673.1	-979.5 -55V.	-554.3	979.5	949,8
	31,295 29,99	9.993	.345:5-	-830.8	342:2	336.8	6.	10.3	60.	50:05	-40.21	-90.09	1112:6	-6-169-	409-1-0301-4-00#	-60400	105857	10.1.0
8		30,630	339.9	522.0	339,9	323,7	•	409.5	00	51,68	72.51	62,67	1130.8	705.5-	705.5-1078.5 -626.	-626.7		1036.2
. 88 .	32,499 3	31.271	.337.9	510.9	337.9	309.8	0.	406.2	00	-25.67	72.92	95.49	1150.1	-721.6-	721.6-1099.4	-651.6	1099:4	1057.8
SCHOOL SECTION OF STREET			1	2011	۵		0- 046		- 0 - 0 - 0	. 0.00	/200-	4.00		-0.439	3	7-4		* 1-2-
THE TAXABLE PROPERTY TO THE TAXABLE TA	1 P P P P P P P P P P P P P P P P P P P	TOFF OF	CREE DI	TORER D		2 X C I V		-	TOTAL PROFILE	111100	P 107	Pol Total Total	0.141	STATIC	•			
	5.33		19.16	Karac Kar 71 . 61	α	2 2 2	-84.68	1964	1000	1500		9867	-	XHX	47.00	16578	.4779	14384
; ه			94	2 4 . 6 7	4		1		3 0 0			•	47.00	77.0	200	. A 2 5 A	65.72	777
:							-			200		3 2 3				0 3 7 1		
5		1001	17.1	Y 0 0 7 2	0 / • / •	• 000	0/0/	01.0		. 001	* O * * * *	9,000		1357		0 1	000	
8		10.00	4.07	25,87	24.02	.0131	. 5041	.1051	.0220	.0192		906	* * 0 6 *	.8642	, 3224	.5272	089/	000
2	8.19	10.77	8.43	17.00	99.41	-0164	- 4885	-1377	.9920		1.3641	•			-1526	1074	- 8604 	5234
2		09.01	5,39	14,08	8.86	•0120	.4785	.1717	.0324			.7948	,7855	.7421	.3172	.4678	• 6436	.5822
88	8.75	00.01	00.9	11.22	7.26	.0137	.5097	.2378	2240°	.0398	$\overline{}$	- 1114	6985	-1059-	-3048-	8854	12001	0,40
8	8.70	9.79	6.70	9,83	6.77	.0142	. 508	. 2511	.0429	.0405	1,3632	,6932	.6796	.6342	3002	.4473	1.0199	9.09.
; 88	8,71	9.63	7.64	8,35	6,38	1910	- 5040	. 2604	- 6260	. 9650	98561	-6774	. 6633	. 9179	3050	4371	1:0370	4610
				70770 TOTAN			0											
			INLET			IN ET IN	INET											
				. 96			54											
			•	50.501 601101	i	03.57	21.0											

8	OTOR ANGLE	GLES					AIRF	OIL AER	ODYNAMI	AIRFOIL AERODYNAMIC SUMMARY PRINT	RY PRIN	-		١.	23:22:48			JULY 12:1971
NAS	NASA ENGLISH) HSI	SPECIAL								-	RUN #		31 SPEED C	CODE 90, POINT #	POINT #		1, PAGE 36,01
1	DIA-1	2-2	T=7	۷ <u>-</u> 2	VM-1	VM-12	V0-1	V0-2	8-1	8-2	81	B2	. 1-1	×1-2	107	V01-2	-	0 - -2
3	Z	z	FT/SEC :	Π.	/SEC	FT/SEC F	T/SEC F	T/SEC D	EGREE D	I/SEC FI/SEC FI/SEC DEGREE DEGREE DEGREE	EGREE D	EGREE !	FT/SEC	DEGREE FT/SEC FT/SEC FT/	T/SEC FT	T/SEC F	VSEC FT/SEC FT/SEC	T/SEC
۴	17.467	19,769	545.0	958.1	545.0	683.2	0	671.8	000	44.52	54.43	15.61	937.0	709.5	-762.2	-190.8	762.2	862.6
2		20.408			556.5	660.2	•	617.4	00•	43.08	55,37	22,48	979.3	715.0	-805.8	-273.1	802.8	890.5
2	. ~1	21.047	566.9	•	566.9	635.7	•	576.6	00•	42.19	56.28	28.19	1021,2	722.6	-849.4	-341.7	849.4	918.4
8	22,314		590.4	795.4	590.4	631.9	•	483.0	00.	37,40	58.76	39,39	1138,7	817.7	-973.7	-519.0	973.7	1002.0
	25,791	25,520		733.0	603.5	599.5	•	421.7	00.	35,12	61.19	49.08	1277.0	915.5-	1125,4	-691.8	1125.4	1113.6
2	28.954	28.076	596.7	685.3	596.7	579.7	0.	365,5	00.	32,22	64.70	55,97	1397,3	1037.1-	1263.4	-859.6	1263,4	1225.1
8	31.295	29,993	į	658.5	580.4	556.5	0	351.8	00.	32.31	66.97	59,82	1483.8	1107.1-	1365.5	-956.9	1365.5	1308.7
8	31,883	30.63	575.7		575.7	509.8	0	358.3	00.	35.14	67.52	62,48	1505,6	1103.4-	1391.2	-978.2	1391.2	1336.5
	32,499			:	572.1	446.6	0.	358.0	8	38.77	68.03	66.07	1529,1	1101.5-	1418.1-	1006.5	1418.1	1364.5
1.	INCS	SINCH	DEV	TURN	AMBER O	MEGA-B	D-FAC 0	OMEGA-B D-FAC OMEGA-B LOSS-P LOSS-P	LOSS-P	LOSS-P	P02/	EFF-P	FFF-AD	ISS-P PO2/ EFF-P EFF-P M-1 M-2 M-1	M-1	M-2	M-1	M2
S S	*SPANDEGREE	EGREE	EGREE	DEGREE D	DEGREE S	SHOCK		-	OTAL P	TOTAL PROFILE P	P01	OTAL .	TOTAL :	STATIC				
م	.91	S.	15.44	38,62	48,82	.0050	. 4114	.0704	.0150	.0139	1.7720	.9582	.9547	.9158	.5027	.8419	.8691	.6234
2	:	5.79	~	32,89	43.39	.0070	.4230	.0888	.0190	.0175	1.7064	.9395	.9347	.8953	.5147	.7918	.9129	.6263
2	- 20	5.57	15.51	28.09	37.85	1600	.4338	.1087	.0231	.0212	1.6543	.9166	•		•	9644.	,9524	.6311
8	.89			19,36	24.01	.0172	.3979	.0621	.0129	.0093	1.6054	.9362	•		•	.6939	1.0604	.7134
8	2.24	4.83	ĺ	12,71	14.62	.0365	.3833	.0866	.0173	.0100	1.5498	4168.	.8645	ĺ	٠	.6363	1.1842	7947
2	3.22		5.19	9.74	8.88	0550	.3451	.0838	.0159	.0054	1.5079	.8742	•		•	.5939	1,2903	.8987
8	3.61	4.86		7,15	7.26	.0709	3385	.1153	.0211	.0083	1.4826	.8159	•		•	.5680		6456
8	3.71	4.78		5.04	6.75	.0760	3539	.1650	.0284	.0154	1.4479	.7392	•		•	5345		.9461
82	3.81	4.73	9.14	1.96	6.38	.0840	.3667	.2092	•0322	.0194	.0194 1.4041 .6655	•6655	.6493	.6814	.5265	.4882		.9391
			Ĭ	- 1		F-AD EF	<u>ا</u> 1											
			=	- 1	INLET IN	NET INE	LET											
			-	1.1556 1.5618		% % 87.29 AB.06	X											
			4,	1	-	3	2											

(SPECIAL) A-2 VM-1 VM-2 VO-1 VO-2 B-1 B-2 B ¹ FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC DEGREE DEGREE DEGREE 769 533.4 944.3 533.4 653.6 .0 681.5 .00 46.80 554.9 .00 44.42 56 .00 554.9 849.9 554.9 606.8 .0 632.9 .00 44.42 56 .00 577.4 782.8 577.4 592.2 .0 631.9 .00 44.42 56 .00 590.6 577.4 782.8 577.4 592.2 .0 611.9 .00 44.42 56 .00 590.6 577.4 782.8 577.4 592.2 .0 411.2 .00 39.03 62 .00 590.6 577.8 590.6 590.0 .0 4414.2 .00 38.04 67 .00 590.6 570.8 531.3 .0 415.7 .00 38.04 67 .00 550.4 648.8 566.4 490.1 .0 425.9 .00 38.04 67 .00 565.4 648.8 566.4 490.1 .0 425.9 .00 40.84 67 .00 550.4 67 .00 550.4 67 .00 550.4 67 .00 550.4 67 .00 550.4 67 .00 550.4 67 .00 550.4 67 .00 550.4 67 .00 550.4 67 .00 550.4 67 .00 550.4 67 .00 550.4 67 .00 550.4 67 .00 550.4 67 .00 550.4 67 .00 6	ROT	ROTOR ANGLES					AIRFOIL		AERODYNAMIC	C SUMMARY	RY PRINT	·		ત	5:24:26		1 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2,1971
IN TIN FYSEC	NASA	ENGLISH	(SPECIAL)									# NOW	31,	SPEED CC	10E 30'F	NIOC	2 PAG	36.01
17.467 19.769 533.4 944.3 53.1 18.467 20.408 544.9 944.3 54.1 19.467 20.408 544.9 944.3 54.1 19.467 20.408 544.9 944.9 55.2 22.314 22.964 577.4 782.8 57.2 22.314 22.964 577.4 782.8 57.3 21.295 29.993 570.8 674.6 57.3 21.893 31.271 562.7 618.6 56.3 21.499 31.271 562.7 618.6 56.4 6.33 15.25 28.89 37.2 1.41 5.39 9.69 13.43 14.2 5.70 5.31 6.49 13.43 14.2 5.70 5.31 6.49 13.43 14.1 5.39 4.35 6.08 7.3 6.41 5.10 5.10 5.70 5.31 6.49 13.43 14.1 5.39 5.19 4.35 6.08 7.3 6.41 5.10 5.70 5.31 6.49 13.43 14.10 5.10 5.10 5.31 6.49 13.43 14.10 5.10 5.10 5.70 5.31 6.49 13.43 14.10 5.10 5.10 5.70 5.31 6.49 13.43 14.10 5.10 5.10 5.70 5.31 6.49 13.43 14.10 5.10 5.10 5.70 5.31 6.49 13.43 14.10 5.10 5.10 5.70 5.31 6.49 13.43 14.10 5.10 5.10 5.70 5.31 6.49 13.43 14.10 5.10 5.10 5.31 6.40 5.40 5.40 5.40 5.40 5.40 5.40 5.40 5	ONVE	` <	:		3	VM-2	1-07	V0-2	8-1	8-10-10-10-10-10-10-10-10-10-10-10-10-10-	1100	8 - 18 18 18 18 18 18 18 18 18 18 18 18 18 1	. 4-17	7.2-17	/01	70,-2	U-1	U-2
17.467 19.769 533.4 944.3 53 19.467 20.408 544.7 994.4 54 19.467 20.408 544.7 994.9 54 22.314 22.964 577.4 782.8 57 22.314 22.964 577.4 782.8 57 23.29.993 570.6 674.6 57 31.883 30.630 566.4 648.8 56 32.499 31.271 562.7 618.6 56 1MCS INCM DEV TURN CAMB DEGREE DEGREE DEGREE DEGR36 6.07 15.25 39.57 48 2.70 6.33 15.89 33.80 43 2.71 5.39 9.69 19.74 24 2.70 5.31 6.49 13.43 14 2.10 5.10 5.76 6.11 5.26 8.36 8 3.61 5.44 6.31 6.49 13.43 14	Z		- 1/36/-		0	7 7 7	וואני ו	ואר חב	טאבר טי	בפאבה ט	EUNEE U	ביטאנים ד	17566	1357	/256	1 200	730	7000
18,467 20,408 544,7 894,4 54 19,467 21,047 554,9 849,9 55 22,314 22,964 577,4 782,8 57 22,314 22,964 577,4 582,8 583,2 688,9 58 31,295 29,993 570,8 674,6 57 31,893 30,630 566,4 648,8 56 32,499 31,271 562,7 618,6 56 INCS INCM DEV TURN CAMB DEGREE DEGREE DEGREE DEGREE DEGR -36 6.07 15,29 33,57 48 2.70 6.33 15,49 33,80 43 2.70 5.31 6.49 13,43 14 2.70 5.31 6.49 13,43 14 2.70 5.31 6.49 13,43 14 2.70 5.31 6.49 13,43 14 2.70 5.31 6.49 13,43 14 2.70 5.31 6.49 6.11 574 24 2.70 5.31 6.49 13,43 14 2.70 5.31 6.49 13,44 24 2.70 5.31 6.49 13,44 24 2.70 5.31 6.49 13,44 14 2.70 5.31 6.49 13,44 6.41	1 	7.467 19.76	59 533.4	944.3	533.4	653.6	•	581.5	00.	46.20	54.98	15.42	929.7	678.1	- 761.4 -	-180.2	761.4	861.8
19.467 21.047 554.9 649.9 55 22.314 22.964 577.4 782.8 57 25.314 22.964 577.4 782.8 57 25.314 22.964 577.4 782.8 57 25.35 56.9 59.95 57.8 674.6 57 31.803 30.630 566.4 648.8 56 32.499 31.271 562.7 618.6 55 32.499 31.271 562.7 618.6 56 32.499 31.271 562.7 618.6 56 32 15.25 39.57 48 2.70 6.33 15.89 33.80 43 2.70 5.31 6.49 13.43 14.2 5.70 5.31 6.49 13.43 14.2 5.70 5.31 6.49 13.43 14.2 5.39 5.19 4.35 6.08 7.35 6.08 7.35 6.08 7.35 6.08 7.35 6.08 7.48 7.35 6.49 13.43 14.2 5.39 5.19 4.35 6.08 7.35 6	2	~	18 544.7	994.4	544.7	632.0	0.	532.9	00.	40.84	55.91	22.11	972.0	682.7	-805.0	-256.7	805.0	889.6
22.314 22.964 577.4 782.8 57 25.791 25.520 590.6 732.4 59 53 25.520 590.6 732.4 59 53 21.295 29.993 570.8 674.6 57 31.883 30.630 566.4 648.8 56 32.499 31.271 562.7 618.6 56 32.499 31.271 562.7 70RN CAMB DEGREE DE	16	~	i	6.648	554.9	606.8	0	594.9	00.	44.42	56.82	27.93	1013.9	688.2	848.6	322.6	848.6	917.5
25.791 25.520 590.6 732.4 59 28.954 28.076 585.2 688.9 58 31.295 29.993 570.8 674.6 57 32.499 31.271 562.7 618.6 56 INCS INCM DEV TURN CAMB DEGREE DEGREE DEGREE DEGREE DEGREE 34 6.11 15.25 28.89 37 1.41 5.39 9.69 19.74 24 2.70 5.31 6.49 13.43 14 2.70 5.31 6.49 13.43 14 2.70 5.31 6.49 13.43 14 2.70 5.31 6.49 13.43 14 2.70 5.31 6.49 13.43 14 2.70 5.31 6.49 13.43 14 2.70 5.31 6.49 13.43 14 2.70 5.31 6.49 13.43 14 2.70 5.31 6.49 13.43 14 2.70 5.31 6.49 13.43 14 2.70 5.31 6.49 13.44 6.41 2.70 5.31 6.49 13.44 6.41 2.70 5.31 6.49 13.44 6.41 2.70 5.19 4.55 8.08	8			782.8	577,4	592.2	0	511.9	00.	40.84	59.29	39,55	1131.2	768.1 -	- 7.2.7	-489.2	7.276	1001.0
28.954 28.076 585.2 688.9 58 31.295 29.993 570.8 674.6 57 31.883 30.630 566.4 648.8 55 32.499 31.271 562.7 618.6 56 INCS INCM DEV TURN CAMB DEGREE DE	8	5.791 25.52		732.4	590.6	569.0	.00	461.2	• 00	39.03	62.28	48.86	1270.0	864.8-1	124.3	651.3	1124.3	1112.5
31.295 29.993 570.8 674.6 57 31.803 30.630 566.4 648.8 56 32.499 31.271 562.7 618.6 55 INCS INCH DEV TURN CAMB DEGREE DEGREE DEGREE DEGR36 6.07 15.25 28.89 57 1.41 5.39 9.69 19.74 24 2.70 5.31 6.49 13.43 14	2	8,954 28.07	o	6889	585.2	550.4	0	114.2	00	36.96	65,11	55,75	1391.3	979.4-1	262.2	-809.7	1262.2	1223.9
31.883 30.630 566.4 648.8 56 32.499 31.271 562.7 618.6 56 INCS INCM DEV TURN CAMB DEGREE DEGREE DEGREE DEGR 36 6.07 15.25 39.57 48 02 6.33 15.89 33.80 43 02 6.33 15.89 37.80 43 04 6.11 15.25 28.89 37 1.41 5.39 9.69 19.74 24 2.70 5.31 6.49 13.43 14 2.70 5.31 6.49 13.43 14 3.61 5.19 4.35 8.08 7 3.93 5.19 4.35 8.08 7	3	1,295 29,99	3 570.8	674.6	570.8	531.3	•	415.7	0	38.04	67.29	59.21	1478.8	1038.1-1	364.2	891.8	1364.2	307.8
1 Jucs Inch DEV TURN CAMB DEGREE DEGREE DEG	8	1,883 30,63	10 566.4	648.8	566.4	490.1	•	124.7	000	50.0	67.82	61.71	1500.9	1034.4-1	389.8 -	910.6	1389.8	1335.2
INCS INCH DEV TURN CAMB DEGREE DEGREE DEGREE DEGRE -36 6.07 15.25 39.57 48 -36 6.11 15.25 28.89 47 34 6.11 15.25 28.89 47 2.70 5.31 6.49 13.43 14 2.70 5.31 6.49 13.43 14 2.50 5.19 4.92 9.36 8 3.93 5.19 4.35 8.08 7 4.01 5.10 5.74 6.11 7	8	2,499 31.27	1 562.7	618.6	562.7	448.5	•	125.9	000	43.54	68.34	64.42	1524.4	1039,3-1	416.7	937.3	1416.7	363.2
INCS INCH DEV TURN CAMBER OMEGA-B D-FAC OMEGA-B LOSS-P PO2/ EFF-P EFF-AD EFF-P M-1 M-2 M ⁻¹ P DEGREE DEGREE DEGREE DEGREE SHOCK -36 6.07 15.25 39.57 48.82 .0058 .4430 .0355 .0076 .0063 1.8079 .9796 .9599 .4915 .8270 .8615 .9053 .905 .9599 .9589 .9589 .9058 .905	1		ı		,			ı	•	,								
DEGREE DEGREE DEGREE SHOCK -36 6.07 15.25 39.57 48.82 .0058 .4430 .0355 .0076 .0063 1.8079 .9796 .9599 .4915 .8270 .8615 .9596 .9778 .9594 .4915 .8270 .8615 .9589 .9596 .9599 .9596 .9599 .9599 .9595 .9595 .9595 .9595 .9595 .9596 .9599 .9596 .9599 .9596 .9495 .9599 .9599 .9599 .9595 .9595 .9595 .9595 .9595 .9596 .9445 .9445 .9445 .9405 .9599 .9558 .9104 .5125 .7596 .9445 .9445 .9415 .9596 .9405 .9597 .9551 .9256 .9445 .9595 .9597 .9551 .9256 .9445 .9595 .9597 .9551 .9256 .9597 .9551 .9256 .9597 .9551 .9256 .9597 .9551 .9256 .9597 .9551 .9256 .9597 .9551 .9256 .9445 .9597 .9551 .9256 .9445 .9597 .9551 .9256 .9445 .9459 .9405 .9397 .9351 .9256 .9445 .9459 .9405 .9397 .9351 .9256 .9445 .9459 .9405 .9397 .9351 .9256 .9445 .9459 .9405 .9397 .9351 .9256 .9445 .9510 .9251 .9256 .9445 .9405 .9397 .9351 .9256 .9445 .9405 .9397 .9351 .9256 .9445 .9405 .9397 .9351 .9256 .9445 .9405 .9397 .9351 .9256 .9445 .9405 .9405 .9405 .9405 .9405 .9406 .9405 .940	1	:	-		œ	MEGA-B	J-FAC OM	EGA-B L	055-P	_0SS-P	P027	EFF-P E	FF-AD	FFF-P	M-1	M-2	H-1	M 2
-36 6.07 15.25 39.57 48.82 .0058 .4430 .0355 .0076 .0063 1.8079 .9796 .9778 .9594 .4915 .8270 .8615 .902 6.33 15.89 33.80 43.39 .0078 .4458 .0121 .0104 1.7505 .9630 .9599 .9368 .5032 .7809 .9053 .34 6.11 15.89 33.80 43.39 .0078 .4452 .0151 .0104 1.7505 .9930 .9358 .9104 .5125 .7309 .9053 .945	M.SPAN DE	REE DEGREE	DEGREE D		ш	HOCK		T.	TAL	ROFILE	PO1	DIAL I	STAL S	TATIC		1		
02 6.33 15.89 33.80 43.39 .0078 .4558 .0565 .0121 .0104 1.7505 .9630 .9599 .9368 .5032 .7809 .9053 .34 6.11 15.25 28.89 37.85 .0100 .4682 .0808 .0172 .0151 1.7009 .9405 .9356 .9104 .5125 .7396 .9445 .141 5.39 9.69 19.74 24.02 .0181 .4447 .0625 .0130 .0092 1.6502 .9397 .9351 .9236 .5332 .6790 1.0510 .2.70 5.31 6.49 13.43 14.60 .0372 .4293 .0865 .0173 .0098 1.6173 .9008 .8938 .8863 .5444 .6316 1.1740 .3.91 5.19 4.35 80.8 7.0533 .2955 .0936 .0177 .0073 1.5866 .8749 .8938 .5949 .5320 1.5811 .3949 .35 5.19 4.35 80.8 8.20 1.5311 .7586 .8111 .7584 .5502 1.5514 .5505 1.3770 .4222 .2153 .0352 .0217 1.5262 .7769 .6888 .7049 .5176 .5225 1.5982	م ا	36 6.0	17 15.25	-	48.82	• 0058		,0355	• 0076	.0063	1.8079	.9796	.9778	,9594		.8270	.8615	.5939.
.34 6.11 15.25 28.89 37.85 .0100 .4682 .0808 .0172 .0151 1.7009 .9405 .9358 .9104 .5125 .7396 .9445 .920 1.6502 .9357 .9351 .9236 .5332 .6790 1.0510 .0092 1.6502 .9397 .9351 .9236 .5332 .6790 1.0510 .0092 1.6502 .9397 .9351 .9236 .5332 .6790 1.0510 .0092 1.6502 .9397 .9351 .9236 .5332 .6790 1.0510 .0092 1.6512 .9306 .8938 .8863 .5444 .6315 1.1740 .0092 1.6512 .9006 .8938 .8865 .5444 .6311 .0553 .3955 .0936 .0179 .0073 1.5866 .8749 .7978 .5320 1.5811 .0092 1.5914 .7994 .7978 .5260 1.5710 .0092 1.5914 .5506 1.5770 .0120 1.5532 .7353 .7747 .5214 .5506 1.5770 .0120 1.5532 .7353 .7747 .5214 .5506 1.5770 .0120 1.5532 .7363 .7447 .5506 1.5770 .0120 1.5525 .7069 .6888 .7049 .5176 .5525 1.5982 .0100 1.5500 .0100 1.5525 .7069 .6888 .7049 .5176 .5525 1.5982 .0100 1.5500 .0100 1.5500 .0100 1.5500 .0100 1.5500 .0100 1.5500 .0100 1.5500 .0100 1.5500 .0100 1.5500 .0100 1.5500 .0100 1.5500 .0100 .0100 1.5500 .0100 .0100 1.5500 .01	2	E.02 6.3	13 15.89	33,80	43,39	.0078	-	,0565	.0121	,010.	1.7505	.9630	6656	9368	_	.7809	.9083	.5960
1.41 5.39 9.69 19.74 24.02 .0181 .4447 .0625 .0130 .0092 1.6502 .9397 .9351 .9236 .5332 .6790 1.0510 . 2.70 5.31 6.49 13.43 14.60 .0372 .4293 .0863 .0173 .0098 1.6173 .9008 .8938 .8863 .5444 .6316 1.1740 . 2.70 5.31 6.49 13.43 14.60 .0372 .4293 .0863 .0179 .0073 1.5866 .8749 .8665 .8648 .5390 .5920 1.2711 . 3.61 5.44 4.99 9.36 8.91 6.72 .071 .4139 .1829 .0322 .0190 1.5532 .7523 .7523 .7427 .5224 .5508 1.3770 . 4.12 5.04 7.50 3.91 6.38 .0840 .4222 .2153 .0353 .0217 1.5262 .7069 .6888 .7049 .5176 .5225 1.3982 .	2		1 15	28.89	37.85	• 0100	Ĭ	,0808	•0172	•0151	1.7009	.9405	.9358	.9104	_	.7396	9445	.5989
2.70 5.31 6.49 13.43 14.60 .0372 .4293 .0863 .0173 .0098 1.6173 .9008 .8938 .8863 .5444 .6316 1.1740 . 3.61 5.44 4.99 9.36 8.91 .0553 .3955 .0036 .0179 .0073 1.5866 .8149 .8665 .8648 .5390 .5920 1.2811 . 3.93 5.19 4.35 8.08 7.26 .0711 .3984 .1375 .0257 .0126 1.5784 .7978 .5262 .5758 1.3546 . 4.12 5.04 7.50 3.91 6.38 .0840 .4222 .2153 .0217 1.5262 .7069 .6888 .7049 .5176 .5225 1.3982	2		<u>ნ</u>	19.74	24.02	.0181		,0625	.0130	• 0092	1,6502	.9397	.9351	.9236		.6790	1.0510	.6663
3.61 5.44 4.99 9.36 8.91 0553 3955 0936 0179 0073 1.5866 8749 8665 8648 5390 5920 1.2811 3.93 5.19 4.35 8.08 7.26 0711 3984 1375 0257 0126 1.5786 8111 7984 7978 5262 5758 1.3546 4.01 5.10 5.74 6.11 6.77 0761 4139 1829 0352 0190 1.5532 7523 7463 7427 5214 5506 1.3770 4.12 5.04 7.50 3.91 6.38 0840 4422 2153 0353 0217 1.5262 77069 6888 77049 5176 5225 1.3982	2	2,70 5,3	11 6.49	13.43	14.60	.0372		,0863	.0173	8600	1.6173	9006.	.8938	.8863		.6316	1.1740	.7458
5.19 4.35 8.08 7.26 .0711 .3984 .1375 .0257 .0126 1.5786 .8111 .7984 .7978 .5262 .5758 1.3546 .5.10 5.74 6.11 6.77 .0761 .4139 .1829 .0322 .0190 1.5532 .7523 .7363 .7427 .5214 .5506 1.3770 5.04 7.50 3.91 6.38 .0840 .4222 .2153 .0353 .0217 1.5262 .7069 .6888 .7049 .5176 .5225 1.3982 .	8	19.61 5.4	66.4	9,36	8.91	0553	1	.0936	.0179		1.5866	6478		8648	Τ.	5920	1.2811	, 8416
5.10 5.74 6.11 6.77 0761 4139 1829 0132 0190 1.5532 7523 7363 7427 5214 5506 1.3770 504 7.50 3.91 6.38 0840 4222 2153 0353 0217 1.5262 7069 6888 7049 5176 5225 1.3982	8		9 4.35	8.08	7.26	.0711	_	1375	.0257	.0126	1.5786	.8111	.7984	.7978		.5758	1.3546	.8860
7.50 3.91 6.38 .0840 .4222 .2153 .0353 .0217 1.5262 .7069 .6888 .7049 .5176 .5225 1.3982 .	8	1	0 5.74	6.11	6.77	.0761	i	1829	.0322	0610	1.5532	.7523	.7363	.7427	- 7	. 5556	1.3770	.8778
	2	4.12 5.0	14 7.50	3.91	6.38	.0840	Ī	.2153	.0353	.0217	1.5262	.7069	•6889	.7049		. 5225	1.3982	.8778

TO/TO PO/PO EFF-AD EFF-P INLET INLET INLET 1,1706 1,6298 87,73 88,56

ROTOR BLADE ELEMENT AND OVERALL PERFORMANCE AND DESIGN DATA

7 / SEC FT/SEC DEGREE DEGREE OF STATES OF STAT	PUNEZ VO-1 VO-2 B-1 B-2 BF-1 BF-2 VO-1 VO-2 VO-1 VO-2 POPOINT B V-2 VO-1 VO-2 VO-1 VO-2 BF-1 BF-2 VO-1 VO-2 VO-2 VO-1 VO-2 VO-1 VO-2 VO-1 VO-2 VO-1 VO-2 VO-1 VO-2 VO-1 VO-2 VO-2 VO-1 VO-2 VO-1 VO-2 VO-1 VO-2 VO-1 VO-2 VO-2 VO-2 VO-2 VO-2 VO-2 VO-2 VO-2	1	ROTOR ANGLES	IGLES					ATRF	IT AERL	DYNAMIL	AIRFOIL AERODYNAMIC SUMMARY	RY PRIN				22:55:9		300	311971
F75EC F75EC F75EC DEGREE DEGREE OF A 10.2 I	VH-Z VO-1 VO-2 B-1 B-2 BV-1 BV-2 VV-1 VV-2 VO-1 VV-2 C FT/SEC FT/	z	ASA ENGL	. ISH	SPECIALI	_								RUN	31,	SPEED C	00E 90+	POINT #	4 PAG	5 36.01
F7/SEC F1/SEC F1/SEC DEGREE DEGREE OF 60 60 60 60 60 60 60 60 60 60 60 60 60	F77SEC F77SEC F77SEC DEGREE DEGREE F75EC F77SEC F77	•	-V19	DIA-2	V=1		1	VH-Z	1-01	7-04	8-1	2-8	Brel	B * - Z	1.0	7-17	104	V0*=2	1	7-0
5 5 5 6 5 6 5 6 5 6 6 6 6 6 6 6 6 6 6 6	0.639.0	S SPA	z. 3		FT/SEC F		•	TISEC F	T/SEC F	T/SEC DI	EGHEE DI	EGREE D	EGREE D	EGREEF	T/SEC F	T/SEC F	I/SEC F	T/SEC F	T/SEC F	1/250
\$ 527.1 .0 641.7 .00 45.22 \$ 599.7 .0 50 445.22 .00 41.39	4 627.1 .0 641.7 .00 45.66 56.38 21.60 966.9 675.0 =805.2 = 2446.1 5 599.7 .0 604.6 .0 00 45.22 57.27 27.52 1009.0 677.6 =848.8 = 313.0	ſ	17.46.	19.76	524.0	8-016	524.0	639.0	þ	840.4	8	12.74	25.4	15.02	5.2	9010	270100	51/1	1010	
5 599.7 .0 604.6 .00 45.22 5 548.5 .0 442.0 .00 41.39 5 517.8 .0 445.7 .00 40.72 1 480.9 .0 455.4 .00 40.72 1 480.9 .0 455.7 .00 40.72 1 480.9 .0 455.4 .00 40.72 2 00.0 40.72 2 00.0 40.72 2 00.0 40.72 2 00.0 40.0 40.0 40.0 40.0 40.0 40.0 40.	5 599.7 0 604.6 00 45.22 57.27 27.52 1007.0 677.6 - 848.8 - 313.0 7 568.5 . 0 626.2 00 42.79 59.77 39.88 1126.0 740.9 - 972.9 - 475.1 5 51.5 . 0 442.0 . 00 412.79 59.77 39.88 1126.0 740.9 - 972.9 - 475.1 5 51.5 . 0 442.0 . 00 40.77 65.55 55.76 1366.8 945.9-1262.4 - 762.1 1 480.9 . 0 445.7 00 40.72 67.67 59.01 1475.1 1005.7-1364.5 - 626.1 1 480.9 . 0 455.4 00 40.72 67.67 59.01 1475.1 1005.7-1364.5 - 867.1 1 480.9 . 0 455.4 00 40.72 67.67 67.0 64.11 1520.7 1006.8-1417.0 - 905.6 1 1 490.9 . 0 457.9 . 00 46.19 68.19 61.35 1497.3 1003.2-1390.1 - 880.1 1 1 1520.7 1006.8-1417.0 - 905.6 1 1 1 1520.7 1006.8-1417.0 - 905.6 1 1 1 1 1520.7 1006.8-1417.0 - 905.6 1 1 1 1 1520.7 1006.8-1417.0 - 905.6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	=	18.46	7 20,401	1 535.4	897.2	535,4	627.1	•	641.7	00.		56,38	21,60	966.9	675.0	-805.2	-248.1	805.2	887.8
5 549.0	5 549.0 5 549.0 6 483.9 6 0 482.0 7 55.5 7 53.88 1126.0 7 748.87 126.6 8 834.8-1124.5 7 531.5 9 0 0 442.0 9 0 0 49.7 9 62.77 748.87 126.6 8 834.8-1126.4 9 62.6 7 43.9 7 631.5 9 0 442.0 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	<u>۔</u> ا	195.61. 5	7. 21.047	545.5	851.6	545.5	599.7	0.	9.409	00	_45.22	57.27	27:52	T009:0	677.6	8.848.	-313.0	-8 48.8.	-414-
5 549.0	5 549.0	ಗ	0 22,31	1 22.96	1 566.7	774.6	566.7	568.5	٥	526.2	00.	42.79	59,77	39,88	1126.0	740.9	-972.9	-475.1	972.9 1001.	1001.3
7 531.5 .0 442.0 .00 39.74 4 517.8 .0 445.7 .00 40.72 4 430.5 .0 45.7.9 .00 40.72 4 430.5 .0 45.7.9 .00 40.19 5 HOCK 5 HOCK 5 HOCK 6 H598 .0166 .0025 7 .010 .4598 .0166 .0029 7 .010 .4598 .0549 .0117 .0094 1 .0191 .4698 .0693 .0117 .0094 2 .0563 .4244 .1070 .0204 .0097 5 HOCK 6 HCCK 7 HCC	7 531.5	عة ا	0 25.79	25,520	578.5	731.8	578,5	549.0	0.	483.9	00.	-41,39	62,77	48.87	1264.6	834.8-	1124.5	-628.8-	\Box	124.5-11112.7
1 460.9	1 480.9	~	0 28.95	¥ 28.074	1 573.7	691.3	573.7	531.5	•	442.0	00.	39.74	65,55	55,76	1386,8	445.9-	1262.4	-782.1	1262.4	1524.1
490.9 495.5 4 500 43.47 439.5 6 457.9 60 46.19 0 456.8 5 5 6 45.8 60 60 60 60 60 60 60 60 60 60 60 60 60	1 480.9 6 6 455.4 20 43.47 68.19 61.35 1497.3 1003.21390.1 -880.1 1 4 439.5 6 457.9 00 46.19 68.70 64.11 1520.7 1006.8-1417.0 -905.6-1 OMEGA-B D=FAC OHEGA-B LOSS-P LOSS-P POZZ EFF-AD EFF-AD EFF-P H-1 Z +00.6		5 31,291	29.99	1 560.4	683.2	F.042	517.8	0.	4.45.7	000	40.72	67.67	10.45	1475.T	1005.7-	1364.5	1.298-	1364.5	1.000
4199.5 .0 457.9 .00 46.19 OMEGA-B D=FAC OMEGA-B LOSS-P LOSS-P SHOK 2.000.6 .4631 .0225 .0034 .0021 2.010 .4785 .0549 .0117 .0094 2.010 .4785 .0549 .0117 .0094 2.010 .4785 .0549 .0193 .0103 2.010 .4785 .0493 .0193 .0193 2.0563 .4244 .1070 .0204 .0097 2.0563 .4244 .1070 .0204 .0097 2.0563 .4244 .1070 .0204 .0097 2.0563 .4244 .1070 .0204 .0097 2.0563 .4244 .1070 .0204 .0097 2.0563 .4261 .1472 .0276 .0144	4 439.5	•	0 31,88	3 30,636	1 556.1	662.6	556.1	480.9		455,4	00.	43.47	68,19	61,35	1497.3	1003.2-	1390.1	-880.1	1390.1	1335,5
SHOCK TOTAL PROFILE SHOCK TOTAL PROFILE TOTAL	ONEGA-B D-FAC OHEGA-B L055-P L055-P POZZZ EFF-P EFF-AD EFF-P H-1 H-2 SHOCK Z 00066 48598 01166 00036 00021 1.8334 9908 9900 9807 9826 82226 9 00087 44631 00225 00048 00029 1.7868 9857 9844 9741 4944 77627 Z 00110 4785 0549 0117 00094 1.7346 9667 9544 9794 9796 5035 7403 1 00191 4469 0649 0117 00094 1.7346 9667 9574 9796 5035 7403 2 00110 4785 0549 0117 00094 1.7346 9667 9574 9797 5325 6688 1 00191 4469 10553 0191 0191 16487 9544 9717 9719 5226 6688 1 00191 9719 9719 9719 9719 9719 9719 9		16 32,49	9 31.27	552.4	634.8	552.4	439.5	0	457.9	80.	_ 61°9b_	68,70	64.11	1520.9	-8 ° 900L	1417.0	-905.6-	1417.0-	1363.4
2 - 00.06 - 45.96 - 01.66 - 00.36 - 00.21 10.14 10	SHOCK - 4598 - 0166 - 0036 - 0021 1014 1	ĺ	1 1 1 1			201				F. 4. 4. 7.		8-000	7.6.04				1.40	7-7-	1000	
SHOCK Z	SHOCK SHOCK TOTAL PROFILE POI TOTAL TOTAL STATIC 2 00087 44531 00225 00036 00229 1.78648 9957 9968 99701 2 00110 4785 00549 00117 00094 1.7346 9605 9574 99791 1 00191 4696 00693 00143 00103 1.6689 9364 9715 9190 2 0553 424 1070 00274 0017 1.6481 8954 8879 8879 2 05543 4244 1070 00274 0097 1.6268 8107 7770 77943 5 0771 4408 11893 0037 00276 1.6070 7599 7431 7745 8 0850 4500 22220 00368 0022 1.6070 7599 77174 6885 7089			E	٠ د د	: 20		0 L V D J E C			1000	1000		1	04111				•	
6.55 4.86 40.44 48.82 .0066 .4598 .0166 .0031 .8334 .9906 .9900	6.55 4.86 40.44 48.82 .00.66 .4598 .01.66 .00.26 .00.21 .6334 .9908 .9900 .9807 .9644 .9974 .656 .4631 .02.25 .0048 .00.29 .7868 .9657 .9844 .9974 .6564 .4611 .29.75 .97.40 .9741 .9765 .0011 .7346 .9657 .9944 .9974 .9965 .9975 .	S SPA	NOEGREE	DEGREE	DEGREE	JEGREE .		SHOCK		Ĕ	DTAL P.	ROF1LE	Po1	OTAL	OTAL	TATIC				
6.79 15.38 34.78 43.39 .0087 .4631 .0225 .0048 .0029 1.7868 .9857 .9844 6.56 14.81 29.75 37.82 .0110 .4785 .0549 .0117 .0094 1.7346 .9606 .9574 5.87 10.01 19.88 24.01 .0191 .4648 .0643 .0117 .0094 1.7346 .9606 .9574 85.80 10.01 19.89 11.8481 .8954 .8875 5.88 5.01 9.79 8.92 .0563 .4244 .1070 .0204 .0097 1.6247 .8660 .8564 5.56 4.14 8.67 7.26 .0720 .4261 .1472 .0276 .0144 1.6258 .8107 .7970 5.38 6.84 6.77 .0721 .4408 .1693 .0337 .0206 .6270 .7570 .	6.56 14.81 29.75 37.82 .0110 99.85 .0549 .0117 .0094 1.7346 .9657 .9844 .9741 .6.56 14.81 29.75 37.82 .0110 99.85 .0549 .0117 .0094 1.7346 .9606 .9574 .9396 .5.87 10.01 19.88 24.01 .0191 .9469 .0693 .0193 .01689 .9549 .9364 .9315 .9190 .5.88 5.01 9.77 8.92 .0583 .9544 .1070 .0204 .0097 1.6247 .8660 .8564 .8536 .5.88 5.01 9.77 8.92 .0553 .9244 .1070 .0204 .0097 1.6247 .8660 .8564 .8536 .5.88 5.01 9.77 0.726 .1972 .0276 .0144 1.6268 .8107 .7970 .7993 .5.47 5.38 6.84 6.77 .0771 .9408 .1893 .0337 .0202 1.6070 .7599 .7431 .7455 .5.40 7.18 4.60 6.38 .0850 .9500 .2220 .0368 .0229 1.5820 .7174 .6985 .7089		1.	5 9 2	98.41	40.44	48.82	9900.	86Sh.	99100	.0036	•	1.8334	8066		.9807	.4826	.8226	:	3787
5.56 14.81 29.75 37.82 .0110 .9785 .0549 .0117 .0094 1.7346 .9606 .9579 . 5.87 10.01 19.88 24.01 .0191 .9469 .0693 .0113 .6689 .9364 .9315 . 5.88 5.01 9.77 8.92 .0543 .9424 .1070 .0204 .0097 1.6247 .8860 .8564 . 5.58 4.14 8.67 7.26 .0720 .94261 .1972 .0276 .0194 1.6258 .8107 .7770 . 5.38 6.84 6.77 .0771 .9408 .1893 .0137 .0206 .6270 .7770 .	6.56 14.81 29.75 37.82 .0110 .4785 .0549 .0117 .0094 1.7346 .9606 .9574 .9396 . 5.87 10.01 19.88 24.01 .0191 .4968 .0693 .0143 .0103 1.6689 .9364 .9315 .9190 . 5.88 6.51 13.90 14.61 .0382 .4560 .0953 .0191 .6469 .9364 .8679 . 5.88 5.01 13.90 14.61 .0563 .4244 .1070 .0204 .0097 1.6247 .8660 .8564 .8536 . 5.58 4.14 8.67 7.26 .0720 .4261 .1472 .0276 .0144 1.6268 .8107 .7970 .7943 . 5.47 5.38 6.84 6.77 .0771 .4408 .1893 .0337 .0202 1.6070 .7599 .7431 .7455 . 5.40 7.18 4.60 6.38 .0850 .4500 .2220 .0368 .0229 1.5820 .7174 .6985 .7089	_		5 6.7	15,38	34.78	43,39	.0087	.4631	.0225	.0048		1.7868	.9857		.9741	444	.7827		5888
5.87 10.01 19.88 24.01 .0191 .4696 .0693 .0143 .0103 1.6689 .9364 .9315 5.80 6.51 13.90 14.61 .0382 .4560 .0953 .0191 .0114 1.6481 .8854 .8875 5.88 5.01 9.79 8.72 .0563 .4244 .1070 .0204 .0097 1.6247 .8660 .8564 5.58 4.14 8.67 7.26 .0720 .4261 .1472 .0276 .0144 1.6268 .8107 .770 5.38 6.84 6.77 .0077 .4068 .1893 .0137 .0202 1.6070 .7543 .7543 .754	5.87 10.01 19.88 24.01 .0191 .4696 .0693 .0143 .0103 1.6689 .9364 .9315 .9190 .5580 6.51 13.90 14.61 .0382 .4960 .0653 .0191 .0114 11.6481 .8954 .88799 .5970 .979 8.22 .0563 .4244 .1070 .0204 .0077 1.6264 .8660 .8564 .8660 .8564 .8660 .8664 .8660 .8664 .8660 .8664 .8660 .8664 .8660 .8664 .8660 .8664 .8660 .8664		9	1 6.5	14.81	29.75	37.82	.0110	4785	.0549	0117	\$600°	1.7346	: •	-9574	. 9396	5035	7403	. 64366.	28860
5,80 6,51 13,90 14,61 .0382 4566 .0953 .0191 .0114 1.648f .8875 8875 5.88 5.01 9,79 8,72 0.563 .4244 .1070 .0204 .0097 1.6247 .8660 .8564 5.58 4.14 8.67 7.26 .0720 .4261 .1472 .0276 .0144 1.6268 .8107 .7970 5.47 5.38 6.84 6.77 .0771 .4408 .1893 .0337 .0202 1.6070 .7570 .7570	5,80 6,51 13,90 14,61 .0382 .4560 .0953 .0191 .0114 1.648 .8954 .8875 .8779 .5.88 5.01 9,79 8.72 .0543 .4244 .1070 .0204 .0097 1.6247 .8660 .6564 .8536 .5.58 4.14 8.67 7.26 .0720 .4261 .1472 .0276 .0144 1.6268 .8107 .7970 .7943 .5.47 5.38 6.84 6.77 .0771 .4408 .1893 .0337 .0202 1.6070 .7599 .7431 .7455 .5.40 7.18 4.60 6.38 .0850 .4500 .2220 .0368 .0229 1.5820 .7174 .6985 .7089	"	9 1 0	5.8	10.01	19,88	24.01	.0191	9694	.0693	.0143	.0103	1.6689	•	9315	.9190	.5226	8699.	8++0*1	.6407
5.88 5.01 9.79 8.92 .0543 .4244 .1070 .0204 .0097 1.6247 .8660 .8564 .5.58 4.14 8.67 7.26 .0720 .4261 .1472 .0276 .0144 1.6268 .8107 .7970 .5.58 4.14 8.67 7.0771 .4408 .1895 .0337 .0202 1.6070 .7597 .7431 .5.58 .407 .7704	5.88 5.01 9.79 8.92 .0543 .4244 .1070 .0204 .0097 1.6247 .8660 .8564 .8536 .558 4.14 8.67 7.26 .0720 .4261 .1472 .0276 .0144 1.6268 .8107 .7970 .7943 .547 5.38 6.84 6.77 .0771 .4408 .1893 .0337 .0202 1.6070 .7599 .7431 .7455 .540 7.18 4.60 6.38 .0850 .4500 .2220 .0368 .0229 1.5820 .7174 .6985 .7089		3.1	5	15.9	13,90	14.61	.0382		.0953		. b110.	1:648	9954	8878	8799	5355-	6288	1:1660	-1173
4261 1472 0276 0144 1.6288 8107 7970 4408 1893 0137 0202 1.6070 7559 7431	44261 1472 0276 0144 1.6268 8107 7770 77943 4408 1893 01337 0202 1.6070 7599 7431 77455 4408 01320 0229 1.5820 7174 6985 7089		0.4	•	3 5.01	9.79	8.92	.0543	4244	1070	.0204	.0097	1.6247	.8660	8564	.8536	.5280	.5913	1.2737	9090
.4408 .1893 .0337 .0202 1.6070 .7599 .7431	.4408 .1893 .0337 .0202 1.6070 .7599 .7431 .7455 .		4.3	5.5	41.4	8.67	7.26	.0720	.4261	.1472	.0276	1410	1.6268	.8107	.7970	.7943	2915	5803	1:3487	2458
1000 1000 1000 1000 1000 1000 1000 100	.4500 .2220 .0368 .0229 1.5820 .7174 .6985 .7089	_	10° 4° 3°	3 5.4	5.38	9 9 4	6.77	.0771	4408	.1893	.0337	.0202	1.6070		_	Τ,	•	.5597	1,3718	•
C. C. 111 OTACIT 1770 CACO 0777 OCC.		_	7 7 8	3 5.46	7.18	09.4	6.38	.0850	4500	.2220	.0368	.0229	1.5820			į	٠,	. 5337	1,3935	1000

10/10 PO/PO EFF-AD EFF-P INLET INLET INLET 1.1787 1.6644 87.61 88.49

ROTOR ANGLES						AIR	OIL AER	DOYNAMI	AIRFOIL AERODYNAMIC SUMMARY	RY PRIN				7:95:01		300	12914	ļ.,
NASA ENGLISH		(SPECIAL)	_								₩ N O W	<u> </u>	SPEED	31; SPEED CODE 90, POINT	POINT	# 5,PAGE	GE 36.01	2
NSPAN IN	0.1A-2	V-1 V-2	V-2	T-HA	VH-2 VO-1 VO-2 B-1 B-2 B++1 B+-2 V+-1 V+-2 VO+-1 VO+-2 O-1 U-2 C-1/5EC F1/5EC F1/5E	V0-1	VO-2	B-1 EGREE	B-Z	Braj EGREE D	B - 2	1.756	V1-Z	VI-Z VOV-1 VOV-Z	V0*-Z	0-1 F1/SEC	U-2 F1/5EC	١
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10 18 467	- ,,	506.7	_	506.7	607.4	•	659.8	0	47.37	57.79	20.69	950.8	649	904.0	649.8 -804.6 -229.3	904.6		
1	7 21.047	515.8 851	851.6	515.8	576.0		627.2	00		58.69	26.70	- 1	646.2	-848.	-289.7		917.	Ь
30 22,314		533.0	755.8	533.0	512.0	•	556.1	8	47.36	61.26	40.95	40.95 1108.7	678.1	678.1 -972.2 -444	オ・オオオー	972.2	1000.5	s
50"25,791		542.2	727.7		506.2	0.	522.8	00.	_45.65_	64.24	49.30	49.30 TZ47.6	776.8	76.8-1123.6 -589.	1.685-	1123.6	23.6-1111.8	6
70 28,954		537.9	697.4	537.9	4.064	•	495.9	0	45,32	66.89	55,97	55,97 1371.4	877,5	877.5-1261.4 -	-727,3	1261.4	1223	N
٠.	1	i	700.3	525.7	478.5	0.	511.2	00.	46.89	16.89	16.85	1461.3	28.3	928 3-1363 4-	195:5	1363.4	1306.7	1
80 31,883			684.3	521.7	444.1	•	522,8	00.	49.67	69.41	61,32	61,32 1483,8	925,5	925.5-1389.U -811	-811.7	_	389.0 1334.5	'n
	31,271	518.1	666.6	518,1	409.7	0.	525.8	000	52:08	06.69	63.90 1507.7	1507.7	931.7	-1415;9	31.7-1415.9 836.6	1415.9	1362-4	+
INCS	TNCS INCH DEV TURM CANB	DEV	TURM C.	AMBER 0	.ER' OMEGA-8"D=FAC"OMEGA-8"LOSS-P"LOSS-P" PO2/"EFF-P"EFF-AD"EFF-P	-FAC DI	HEGA-B	_d_SS07	_d-SS07	- P02/	EFF-p-E	FF-AD	_£.F.+p_		H=1H=ZH=1H=Z		H 8-2	
MSPAN DEGREE	0 2 6	EGREE D	EGREE DI	EGREE S	HOCK	-	Ĩ	TOTAL PROFILE	ROFILE	Pol	POI TOTAL TOTAL STATIC	OTAL S	STATIC					
15.1	8.00	14:15	4.15 42.59	48.81	P 600	488b.	. 1020.	0043	-4889 0 Z01 0043 0063	1.8784	_	1:011	7.0110 1.0119 1.0187		į	1048.		þ.
10 1,88	8.22	14.48	37.10	43,38	.0118	4852	.485202350051	. 1500	0077	1.8445	1,0140	-	.0153 1.0224	4668	7804	*****	. 5655	ũ
16 2,25	ŀ	13.96	31.99	37.78	++10.	5073	.0236		•100	.0019 1.7918	i		. 9739	4746	İ	. 9227	28600	6
30 3,37		11.11	20.30	24.03	.0227	.5256	.0890	.0181	+0134	1,7016	.9243	9182	.9038	•		1.0241	.5826	•
19.4	7.27	94.9	14:93	14.63	5140.	!	1062	-0211	. 0129 7	1.7073	.8935	8820	.8746	-E 1643		Г	.6630	0
70 5,37	7.24	5.22	10,93	8.93	.0593	4810	.1303	.0247	.0136	1.7029	.8551	.8436	.8364	4935	•	1.2531	.7438	œ
88 5,55		4.10	96.6	7.26	.0747	9684	1770	.6333	.0195 1.723	1.7239	8002	7844	.7748	4830	ľ	_	ľ	Į.
90 5 60	0 . 6.70	5.35	8.10	6.77	.0797	.5047	.2154	.0385	.0244	1,7118	.7598	7410	7342	.4784	.5738	1.3544	.7738	8
89 5 98	1	96.9	9.00	6.38	.0878	\$118	. 2424	50400	•0260	1:6957	.7290	7081	.7062	4747	. 8549	1:3769	1156	٠.
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		2 =	IN FT TA	IN ET IN	CFFTAD CFF FF	<u>.</u> -												
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		•	1.1948 1.731	7314 8	A 87-12 A8-09	60												
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	A ENGL	ISH	NASA ENGLISH (SPECIAL)	_								₩ 20 20 20 20 20 20 20 20 20 20 20 20 20	1	31, SPEED CODE 90, POINT	.00E 90	POINT	4 6 PA	6, PAGE 36.01
	DIA-1	DIA-2	DIA-1 DIA-2 V-1 V-2 VH	V=2		VH-2	V0-1 -07-1 -07	Z-0A_	8-1	8=2	Bvel	82		V*=2V0*+1V0*-2U-1U-2	V0*-1	- 40 4 - 2	- Red	U=2
SEPAN IN	z	z	FT/SEC	FT/SEC FT/SEC FT/SI	141	C FT/SEC FT/SEC FT/SEC DEGREE DEGREE DEGREE FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC	T/SEC F	T/SEC DE	EGREE D	EGREE D	EGREE D	EGREE	1/SEC	71/SEC 1	T/SEC	FT/SEC	FT/SEC	FT/SEC
2	_	19.76	7.467 19.769 469.8 932.Z	7.2C6	8.69.6	593.8	0.	718.6	00.	50:43	12.85	13:40	843.9	- 910.5 - 760.00 - 141.5 -	0.09/=	5.1	0:00/	000
2	18.467	8.467.20,408	9 480.0	896.2	480.0	593.1	•	671.9	00.	48.56	59.14	20.01	935.9		631.8 -803.5 -216.0	-216.0	803.5	887
. 9	19.467	9,467 21,047	7 488.4	852.9	488	563.3		b * 0 h 9	. 00.	89.84	48.68 60.03 26.07 977.7	26.07	477.7	1.829	-847.0	-275.3	647.0	915
용	22,314	22,96	4 502.9	752.5	502.9	486.3		574.3	00.	44.14	62.60	41.12	41.12 1093.4	645.4	645.9 -970.8 -424.9	-424.9	970.8	666
2	25,791	5,791. 25,520	508.1	733.4	508.1	483.7	0.	6.9155	00	48,73	. 65.64	Z1: 6h	8.127.7231.9H	739.4.	39.4-1122.1 -559.1	-559.1	1-1122.1	122.1-1110.3
20	18.954	8.954 28.07	500.3		500.3	457.4	•	551.8	00.	50,35	68,33	55.64	55,64 1355,5		811.3-1259.7 -669.7	-669.7	1259,7 1221,5	1221.
: 88	31,295	29.99	3-487.5	713.3	487.5	434.1	0.	-1.995	00.	-52:52	70:30	-59:57	2.9661	657.0	857,0=1361,6 -738,	-738.7	1361.6	13051
8	31,883	30,63	1 483.9		483.9	405.9	0	573.1	00.	54,71.	70.17	61,88	61,88 1469,2	861.4.	861.4-1387.2 -759.5 1387.2 1332.7	-759.5	1387.2	1332.
8	32,499	31,27		687.5	4006	379.4	0	573,3	00	56,52		92.49	1493.5	64,26-1493,5-874,0-1414,0787,2-1414,0-1360,6-	141400	-787.2	1414.0	1360
				;				i							,	•	•	
	202	INCH	TAMBE INCH. DEV TORY CAMBE	TORK		R. 01EGA-0 D-F7C 01EGA-0 LOSS-P-LOSS-P-DO2/ FFF-D EFF-AD FFF-P T-FF-P T-FF-P T-FF-P T-FF-P T-FF-P T-FF-P T-FF-P	D-FAC 0	HEGA-B	-0550	. d=SS07	P02/	1.4-443	LFF-AD.	EFF-P		H.Z		7
SPAN D	EGREE	DEGREE	SSPAN DEGREE DEGREE DEGREE DEGREE DEGRE	DEGREE L	w	SHOCK		TOTAL PROFILE POI TOTAL TOTAL STATIC	DTAL P.	ROF1LE	P01	OTAL	TOTAL :	STATIC				1
9	7.94	6.6	7 13.23	44.87	핕	.0125	505	0368	007	0106	1.0001	1:0190	1.0208	3460.1	į	١	\$298	165
2	3,26	•	6 13. ⁸ 0	13.80 39,13	43,38	.0152	4007	. 5140	0,000-	0124	1.8733	1,0237	1.0259	1.0404	4.18	_	.8719	5487
15	3.64	9.2	13:27	33.96	37.71	.0182	.5211	.0071		.00150025 1.8231	1.8231	566°	0566	6066	4488	.7381	1116	- 0++5:-
8	4.80	8.7	1 11.26	21,49	24.01	.0269	.5528	. 8660.	.0203	.0147	1.7227	.9193	.9127	.8951	4609	.6447	1.0131	. 5533
8	40.9	!	8.68 6.78	15,61	14.62	.0451	5356	.1282	.9520.	•	1:737	.8796	8697		1	į		6286
2	6.83		4.87	12,69	8.90	.0629	.5376	.1864	.0357	.0237	1.7460	1818	. 7976	.7796	.4572		1:2393	.6825
2	56.9	8.2	1 4:70	10.73	7.26	.0782	1245	. 2321	62h0°	.0287	1.7614	7602	7404	77211	4460	2946	1.3149	-27.49
8	96.9		5 5.91	8.89	6.17	.0832	.5559	.2598	.0455	.0311	0311 1.7549	.7327	.7108		-			. 7 1 48
8	7,00	7.92	7.39	96.9	6.38	.0913	. 5577	.2783	. 0458	.0310	.0310' 1.7451""	.7119	. 9889	6755	. 4391	. 5695	1.3601	. 722

1.2071 1.7664 85.17 86.30

ROTOR BLADE ELEMENT AND OVERALL PERFORMANCE AND DESIGN DATA

AIRFOIL AERODYNAHIC SUHHARY PRINT RUN # 31.SPEED CODE 10.POINT # 1.PAGE 36.01 VH=Z VG=1 VG=2 B=1 B=Z B+=1 VG=2 VG-1 VG-2 UG-1 UG-2 UG-1 VG-2 UG-1 VG-2 VG-1 VG-2 VG-1 VG-2 VG-2 VG-2 VG-2 VG-2 VG-2 VG-2 VG-2	54.41 10-53 1037 3 -740-2 = 645.4	39.81 1266.4 870.0-1079.9 -557.1	64,70 58,23 1549,9 1117,6=1401,3 =750,4 1248,2-1235;1==64,70 58,23 1549,9 1117,6=1401,3 =750,1 1401,3 1358,8		416,3	OTAL PROFILE POI TOTAL STATIC	I	9314	8360 8243 8362	7701 7549 7714 5920 5669 7		
NASA ENGLISH (SPECIAL) NASA ENGLISH (SPECIAL) NASA ENGLISH NASA ENGLI	7,467,19,769,604,60,100,47,604,8 8,467,20,408,618,7,969,0,618,7	22,944 661.4 869.0 661.4 668.0 .0	716.0 662.0 588.0 .0	30,630 633,4 664,8 633,4 524,3 .0	98 32,477 31,271 030,2 503,5 030,2 416,3		40 . 0139 . 4440 . 0895	4,60 9,95 18,70 24,02 0410 4327 0857	3670	3603	7 4.87 12.39 =1,15 6.37 1504	

INLET INLET

ROTOR BLADE ELEMENT AND OVERALL PERFORMANCE AND DESIGN DATA

		* ! Z !	31.SPEED CODE 10.POINT	•	C,PAGE JOOUL
V0-2 8-1 8-1	1-18 2	B*=2 V*=1	V = 2 VO = 1	1.00	7-0
FT/SEC FT/SEC DEGREE DEGREE	EE DEGREE DE	GREE FT/SEC	FT/SEC FT/SEC	FT/SEC FT/SE	C FT/SEC
/* DO.	- Co. 45 . 81.	77.27 1036.0		9-213-6-646	858-6
8 .00	.80 55.72	23,46 1083,6		4 -293.7 895	4 989.5
8	13 56.57	28.94-1130.9	Ī	9362-7-943	-9-1020-6-
Ī	93 58 94	4	820 7-1081	9 -532,3 1081	9 1113.4
,	- 6 . 6 . 7		9.6	5 697 - 4 25n	G-1237-1
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λε 00° 0°	C	5/ 5/ 1547 0	1063,0-1403,	CD-1 Z //o- o	7
0	76-67-26	2.240 10 10	1114 4-1517	11612:0/1-6	12. tet 1
0	75 67 80	63,92 1669,6	1113,8-1545,	8-1000.1 1545	8 1485
74 00	שר מא יש		1120 7-1575	7_1030:071575	7-1516-7
	0				
-a_T055-p 105		FF-P EFF-AD		ļ	1 H 2
TOTAL PROF		TAI TOTAL	STATIC		
0510	2.00	9685 9563		. 98T6	-429-95
7510.			9264	8402	62 ,6390
	-	1		. 8008	-24 24
20202		• '	6468	7317	•
0223	_	-	16797	7053	1
.0228		•	• '	6228	6104, 2013
0332	100 1.7044		7558	1-0009	12 - 9350
180	-		7113	5748	47 9286
200	٠		6790	2446	70 - 9295
2		•			•
C FTYSEC FTYSEC FTYSEC DEGREE DEGREE 1		N	DEGREE DEGREE 55.72 23.44 55.57 23.44 55.57 23.44 55.57 23.44 55.57 23.44 55.57 23.44 55.57 23.57 55.5	DEGREE DEGREE 55.72 23.446 55.72 23.446 54.45 54.45 54.45 54.45 54.45 54.45 54.45 54.45 54.45 54.45 54.45 54.45 54.45 54.45 54.45 54.45 54.45 54.45 56.81 54.45 56.81 54.45 56.81 54.45 56.81 54.45 56.81 56.45 56.45 56.81 56.45 56.81 56.45 56.81 56.45 56.81 56.45 56.81 56.45 56	SEREE DEGREE PT/SEC FT/SEC FT/

ROTOR BLADE ELEMENT AND OVERALL PERFORMANCE AND DESIGN DATA

10/10 p0/p0 EFF AD EFF P INLET INLET INLET INLET INLET INLET INLET

ROTOR BLADE ELEMENT AND OVERALL PERFORMANCE AND DESIGN DATA

80	ROTOR ANGLES	•					AIRFOIL		AERODYNAMIC		SUMMARY PRINT	_		~	20128123		JULY 23	23,1971
NASA	NASA ENGLISH		(I SPECIAL)								-	NON	35,	SPEED C	C00E 101	BUNIO	PAGE	PAGE 38.01
3	1 V - 1	DIA-2		۷-2	- 17	VH-2	V0-1	V0-2	B-1	8-2	- B	82		42	101	V02		0 - 2
S SPAN IN	-		FT/SEC P	1.738/L	FVSEC	1 JEC F	۲	17SEC DI	EGREE DE	GREE DI	EGREE DI	EGREE	TYSEC +	T/SEC F	1355	7stc 1	12EC 11	357
r	7.467 1	9.769	5a9.4	1008.9	5a9.4	650.2	•	763.7	00.	49.20	55,17	16.49	1032,1	687.7			847.3	95 ₈ • 9
5	8,967 2	90, 0	603.5	967.1	603.5	4 · 05 q	0	715.7	00.	47,74	56.03	22,87	10801	706.5	845.8		1	4.684
5	9.467 2	1.047	0.919	6 6 6 6	616.0	618.0	٥	681.3	00.	47,78	56.88	28,75	1127.5	706.3	.944.3		_	0.20.9
8	* 1	12.964	642.8	849,3	642.8	587.4	0	613.5	00	46.24	59,28	40.42	1258.7	771.8-	082.4			113.9-
2 28	791	5,520	658,7	829,7	658,7	585.9	0	587,5	0	45,08	62,23	47.98	1413.9	875.4-	251.0	+059-	1251,0 1	1237.9
70 2	954 2	8.076	651,5	765.8	651.5	-552.8	0	530.1	00.	43,80	65,10	56.34	1548.3	-999.2-	404.5	i '	F	361:4-
8	11,295 2	666.6	632.9	745.0	632.9	513,6		539,6	00	11,94	67,37	60,70	1 644 7	1049,5-	518.0		_	484 9
8	11,883 3	0.630	627.5	723.0	627.5	466.3		552,1	00.	49,85	16.79	63,46	1669.0	1043.9-	546.5	-933.6	_	485.8-
	32,499 3	11.271	623.4	702.1	623,4	430.7		554,5	00	52.17	68,42	68,59	1695.2	1054.5-	1576.4		_	516.9
	•	•	1	,	•	;		•	•	•	•	•	•		:			
	1 MC S	INCH	DEV	TURN	CAMBER	DHEGA-B	D-FAC OH	EGA-B	055-p	055-p	P 0 2 /	i deddi	F - A D	EFF.	-	H-2	-	7 H
KSPANDE	MSPANDEGHEE DEGREE DEGREE DEGREE DEGRE	GREE D	EGREE C	JEGREE 1	DEGREE !	SHOCK		F	ءَ	OF ILE	-	DTAL T	TALTS	TATIC	-	-		
h	- 1 -	42.9	16.32	38,68	48,82	12100	5077	.0317		0400		9832	9814	9696		.8727	9196	65646
9	90.	6.43	99.91	33,16	43,39	9510.	5069	•160.		.0033		9813	9792	.9693		. 8345	61.10*	-9609
₽	62.	6.17	16.05	28.13	37,83	.0205	5249	.0687		.0101		9538	2445	.9351		. 1067.	. 1950	9909.
8	1.39	5,38	10.60	18,86	24,00	.0430	5202	9690		5600.		9249	9119	1016		,7242	1.1757	6581
8	2,62	5,25	5.,2	14.25	14,62	.0794	5070	* 1 1 4		.0071		8688	8791	.8772		.7015	0,16.1	.7401
2	3,59	5,43	5,58	9.76	8.91	.1102	0696	.1271		.0032		8658	846	.8529		64337	-4348	1919
2	00.	5,26	5,33	4.67	7,26	. 1344	4790	.1866		9600		7892	,7702	.7815		0619.	.5168	.8720
8	01.	5.18	7.49	4.45	6.76	91410	4951	,2309	,0384	0110	1,8360	. 7426	7198	.7382	.0185	9965	8118	- 6614-
8	4.21	5,12	9,76	2,54	6,38	.1524	4997	, 2566		.0164		7133	4889	.7130		.5766	.5653	0998.
				•				:	;									

10/10 PO/PO EFF-AD EFF-P INCET INCET INCET 1,2348 1,9079 86,25 87,44

ROTOR BLADE ELEMENT AND OVERALL PERFORMANCE AND DESIGN DATA

	ROTOR ANGLES	NGCES						Y	IRFUIC	ALKODY		マピンへ	AIRFOIL AERODYNARIC SUNMARY PRIN			:		F		- -	-1461975
×	NASA ENGLISH	A ENGLISH (SPECIAL)	(SPE	CIVID										¥ ⊃ ∝	n	31, SPEED CODE 10, POINT	2002 a	10,00	=	3, PAG	3, PAGE 36.01
	D A =	PIA	7	-	7-7		AXA	1-0A_z	1 10-2	1-8-Z		3=2	1-16	B 2	A Fe	• •	. VO.	2	2-1	1-0	Z-0 1-0 2-10A 1-10A Z-1A
% SPAN	=	Ξ	k 1	SEC F	FT/SEC FT/SEC FT/SE		PT/SE	PT/SEC FT/SEC FT/SEC DEGREE DEGREE DEGREE FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC	C F7/5	C 0568	EE 0E(GREE D	EGREE 	SEGREE	F1/5EC	17/5	C F1/5	11/ 23	SEC F1	/SEC F	1/SEC
-	17.45	1 1 . 7 6 7		284	2005.3	284	1 652	9	0 764.5		60	1050	55.14	16:45	145 1030	Ĭ.	8 .	. 0 8 D . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 .	12.8	9-2-6	2.45
2	18.467	7 20,408		603.2	966.6	603	2 648.2	2.	.0	117.0	00	47.88	55.99	22,71	1078.7		.3 -89	703.3 -894.2 -271.	71.2	894.2	768,2
.	19.467	7 21.047	1	615.8	_420.2	615	8 - 617	00	.0 . 682.8	8.	. 00*	68. 4	. 96.95	28.57	1126.	ŧ	8.	2.6 =3	36.4	942.6	1019.1
8	22.314	_		6.1.9	846.2	641	9 576	٠.	619 0.	7.	00	17.03	59.27	40.50	1256.8		158,7-1080,	0.5 -492.8	92.8	690.5	1112,0
.	25.79	1. 25,520	į	657.2	827.5	657	. 376	-	.0 593.7		00	45,86	62.24	48°04	1411.	<u>.</u>	862.7-1248	8.9642.	42.1	248.4	1235,7
8	28.954	4 28,076		650.3	769.0	.650	3 549	9.	.0 537.9	٠.	00.	14,38	65.10	56,17	1545.6		9-1-6.	988.9-1402.0 -821.6 1	21.6 1	1402.0	1359,5
2	37:2957	5 27 993		431 54	751:0	631.	2 210	2:	.155 0.		100	17:21	-67:36	80.08	<u>6.1.101.104.05</u>	Γ	:6-151	5:4-1	101:5-1518-1	218-4	1452,3
8	31.883	3 30.630		626.5	732,8	626.	294 5	-	.0 564.3	ŗ.	00.	50.41	67.91	63.06	1666.		1031,1-1543	3.9 -9	-918.9 1	1543.9	1483.2
8	32.479 3	9 31:27	1	22.3	711.4	622	3 429	7.	0 567 3	-	00	52.90	68,42	19.59	65.61 1692.3	_	039.9-1573.	_	0	.0.1573.7	1514.2
	2	Z -		- X	INCH DEV TURN CAMBE	CAMBER	ONEGA	ONEGA"8 D*FAC OMEGA"8 LOSS*P LOSS*P POZ/ EFF*P EFF*AD EFF*P	OMEGI	-B 103	2-6	125-P	1704	25.4	EFF - AD				7		Za. H. Jaki
NATA)EGREE	DEGRE	930 3	REE D	MSPANDEGREE DEGREE DEGREE DEGREE	DEGREE	SHOCK			TOTAL	1 480)F 1 L E	POI TOTAL	OTAL	TOTAL	STATIC					
-	. 22	2 6.	6.21	16:28	38,69	48.8	22.10. 2	15. 22	ē. 7	•	034	Z. 2000	0000	B166 0000.3	6066	ĺ	•		1	\$ 600	5887
2	50.		6.40	6.50	33,28	43.3	110. 6	55 .5095		0. 60	023 -	.00230010 2.0395	3.0395	96 66	.9931	1 , 9803		. 5005	8340 1	90100	.6068
9	.36	İ	6 . 13	5,87		37.8	2 0201		:	į	0103	0900•	. 4787	4674	1 5 9 6 1	:		5725	1.5064	- 2550*	- 6048 -
8	1.38		_	0.67	16,77	24.0	5 .0425	. 53	11 .0875		. 6210	1600	1.9122	9274	.9206	4 .9136	•	. 4965	7207	1.1737	.6462
2	2,63	3 5.27		5.74	14,15	9.41	2 .0786	115: 96	11.128	į	0230	0000	.9359	. 8925	.8819	Ĭ		6100	1.9869	.0116	. 7285
8	3.59	_		5.41	6.9	8.9	1 .1093	•	_			.002	1.8945	8661	. 8535		•	Ī	6454	.4317	.8298
8	-	5	5:55	5,62	88.2	7.2	6 13	32 . 4890	0.0.1862		.0334	1. 4600	.887 H	7936	. 7745	5 .7850		5862	16237	-8215	2458
8	-	0 5.1	8	7.08	4.85	6.7	4041. 9	9405. PO	16 ,2289	Ĭ	.0386	1510	9698	7 499	.727.	2 .7437	•	5800	1 0409	.5388	.8 497
2	4,2	1 2 1	12	69.8	2,81	6:3	151	15.	32 . 25	25600	1040	.0167	1.8467	7198	649	12:2	755		5634	. 2863	. 10527
				10.	T6710 - 60790	į	EFF-AD. FFF-P	4.64.0													
				X	INCET		INLET	INLET													
				-	9264 6275	.9269	86.79	87.94													
				-				•													

166

2	ROTOR ANGLE	GLES		-			AIR	FOIL AE	AIRFOIL AERODYNAMIC SUMMARY	C SUMH	ARY PRIN	2	1		23:13:3	-	JULT	7,1471
NAS	NASA ENGLISH		(SPECIAL)				•					₹	- n	SPEED	C00E 10	POINT	A S,PAG	S, PAGE 36+01
S.SPAN I	SPANIN	101A-2		7/55	C FT/SEC F	FT/SEC	VH-2 VG-1 VG-2 VG-2 B-1 B-2 B-1 B-2 VB-1 VF-1 VF-2 VG-1 VG-2 U-1 VG-2 FT/SEC	V0-2	DEGREE C	B-2	EGREE	DEGREE	FT/SEC	FT/5EC	V0 - 1	V0 2	FT/SEC F	17/SEC
	17.467	1	2885	-865.4 1014.	4 565.	4-642.5	0.	785.0	.00	50:70	62.95	15:11	1019:	-665	-847:5	1.42.1-	-647-5-	858-2
2	18.467	7	8 578		3 578,9	643.0	•	738.6		48.94	57,13	21,37	1066.	0910	-696.0	-251.6	896.0	490.2
£	19.467	21,047	7 590.1	1. 934.	9 590,1	1 610,5	0	708.0	:	49.24	58,00	27,17	1113.7	687,5	9 + + 6	.00 49.24 58.00 27.17 1113,7 m 687,5 4944,5 - 313.2	944.5	1021.2 -
8	22,314	22.964	4 611.	6 837.6	, 611.	6 528.0	0	649		50.89	60,53	41,34	1243.5	703	7-1082.6 -464	7.494-	1082.6	1114,2
3	25, 791	25,520	0 624.		7 624	_	•	625.0	00.	49.93	63.47	6.0	1398	, 8 ₀ 7	-1251-	1-613.2	1251,3	1238,2
2	26,954	28	129	2 788,7	۰	2 520,7	, P.	592,4		48,69	66,13	55,88	1536,1	929	29,6-1404,8	2,69,8	9 40 4	1362.2
£	31.295	~	1	1.564-1	1 606	!	0	619.	00.	-69.05	68, 23	PD 65	1635	980.2	=1518.4	. G 40 2	-1518 4-	-2:5541
8	31,883	•••	0 601.2	783	8 601.2	2 468.1	•	628.2	00.	53,33	68,76	61,39	1659,7	977.6	-1546.9	-857.9	1546.9	1486.1
<u>\$</u>	32.499	31.271	:	762	5 576.	426.4	0	632.0	;	56.01	56.01 69.27		1685	.64,27'1685,9"-982,8-1576,8'-885	9.9721-	1885.Z	1576,8	1517.2-
	INCS INCH	HUN	DEV	DEVTURN	ZANBER	OMEGA-B	04864-8"5-74-7"	OMEGA-A	T-055-P	L 055-P	P02/-	d- 113.	EFF AD.	- EFF		H-2	_	H 1-2.
0 2 402	GREE	DEGREE	DEGREE DEGREE DEGREE	DEGREE	DEGREE		•	,	TOTAL	PROFILE	0 0	TOTAL	TOTAL	TOTAL TOTAL STATIC				
	. 93	7.3	6 41 9	41.1	3 48 81	_	5277	,0034	000	7 0026 2, 1313	2,1313	9987	_98661866	. 6463			į	5747
,	1.19	7.5	15.1	6 35.7	6 43 3	9010. 8	5204	. 0063	.001	0054	2.0979		1,0044		5368	8437	1 6 6 5	.5953
*	1.53	7.3	7 14.4	7 30.8	3 37.8	1 .0230		.0380	.00	.0032	2.0395	•		•	!	;	1.0402	•
2 19	2.60	6.63	3 11.60	19.11	7 24.1	4 .0456	.5768	.1219	.024	.0153	1,9361	•	•	8824	٠	•	161539	٠
9	3.81	6.50	7.0	3 1401	14.6	4 .0817	5580	1	.028	.0121	1.9695		;	1958	:		.1:2890.	•
2	4.59	9 4 8	8 5.1	4 10+25	5 8,92	2 .1121	,5237	.1519			1.9829	. 8492	8339	. 8351	.5749		9214.1 4959.	.7736
' #8	4,85	9.1	2 4.1	1:0	9 7.26	1361	5347	.2024		İ	.0130.2.0219	. 797	1751	1776	15620		-4864-1	0000
8	4.93	9	74°S 6	7,3	7 6.7	6 .1433	5489	.2375		•	2.0132	7628	٠	. 7435	٠	6049	1.5258	7995
8	50.5	2.0	7 7,35	5.00	16,3	1545	9955	,2677			0191 1,9928	7342	7072	•	•		-	7993
			;	T0/10 - P0/P0		EFF AN EFF -P	. d- 44											
			(INLET	Ì	INET	INLET											
				1.2554 1.9981	19981	85.43.8	86.79											

ROTOR BLADE ELEMENT AND OVERALL PERFORMANCE AND DESIGN DATA

20:29:27 JULY 23:1971 CODE 10:PDINT # 6:PAGE 36:01 VO*-1 VO*-2 U-1 U-2	7587 7567 77587 77568 -845,1 -169,2 845,1 956,5 -893.5-247 4-893-5-987-4		9 -602.0 1247.9 1	2-1514,2 -822,1 1514,2 1451,2 2-1542,6-838,2-1542,6-1482,m	-1572,4 -865,1 1572,4 1513,0	H-1 H-2 N'-1 N'-2	5111 8705 9401	5269 8383 9905	.7964 1.0340	. 1060 1.1482	6876	1.4897	6385 T.5162	5355 6181 1,5408 ,7735	
NT RUN # 35.5PEED 8-2 V-1 V-2	E DEGREE FTJSEC FTJSEC F 69 14,99 1011,2 654,0 53 21,36 1059,1 68,7	40 27,23 1105,8' 676,5' 93 '41,40' [235,2' 692]3-	5 797	69 59 19 1625 3 957 2-	65,12 1676,4 953,7	/ EFF-p EFF-AD EFF-p	٥ -	1,0100 1,0111	9820	1006 1604	8779	0672 0540	7535 7279	•	
AIRFOL AERODYNAMIC SUHMARY PR	.00 .00	709 6 .00 49.78 58. 653.4 .00 51.53 60.	000		00	L055-p		• ••	.0062 .0011	.0238 .0144	1381 .0276 .0114 1.9889	. 0310 . 7910	2540 .0443 .0198 2.0230	,0450 ,020°	
4-1 VH-2 VO	55.3 631.6 58.4 631.0	79.4 600.3	11.2 522.1	90 5 490 2 35 4 444 7	31.2 401.0	CÁMBER OHEGA-B D-FAC OMEGA-B	6344	5 5279	5490	4.03 .0457 .5842	;	525/4	•	•	O EFF AD EFF P
SPECIAL)	r * 8	21.047 579.4 929.5	25 520 611 2 820 3	29.993 590.5 797.5	31,271 581,2 762,1	DEV TURN	JEGREE DEGREE DEGRE	7,95 15,14 36,	7,70 14,49 31.	7,04 11,55	4.27 6.93 6.70 14.85 1	6. 4. 5. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4.	5.40 6.49 6.09 7.16	6,41 8,20	10/10 PO/PO
ROTO NASA OT	SEANIN 10		2 2 2 2 2 3 2 3 3 3 3 3 3 3 3 3 3 3 3 3	88	98 32	-	K SPANDE G			8			8 8		

1,2583 2,0123 85,47 86,84

ROTOR ANGLES						AIRFL	OIL AER	AIRFOIL AERODYNAMIC SUMMARY PRIN	C SUMMA	RY PRIN	-		2	0:53:29		איזמר	7,1971
NASA ENGLISH		(SPECIAL)									NOR	31.	SPEEC	OCE 10.	POINT #	16.PAG	1 16.FAGE 36.01
- NIO	2-410	1-1	2-1	Ļ	Z-WA	1-01	Z-DA	1-8	B-2	1-18	8 -2	V*-1	٧٠-2	VO1	V02	U-1	U-2
% SPANIN	Y I	FT/SEC FT/SEC FT/S	1/5EC F	S	TISEC F	FT/SEC FT/SEC FT/SEC DEGREE	TISEC C	LEGREE D	EGREE D	IEGREE D	EGREE !	175EC 1	7/SEC F	TASEC F	T/SEC F	T/SEC F	1/SEC
\$ 17.45	7.467 19.769	# SDOI # 6 # S	100 S.4	549.4	630.6	0	784.3	00.	51.20	56.98	15,29	1008.3	653.9	-845.4	-172.5	40.00	955.8
10 18.46	18.467 20.438	3 562,5	612.9	562.5	634.8		737.3		49.27	57.82	21.53	1056.1	683.0	-893.8	-250.5	80.00	987.8
16 19,45	9.467 21.047	573.2	931.4	573.2	6.06.5	0.	706.9	ì	49.39	58.68	27.24	1102.9	683.5	-942.2	-311.8	942.2	1018.7
30 22.31	2.314 22.964	1 592.6	3.928	592.6	508.2	•	651.2		52.03	61.24	42.17	1232.0	6.65.8	1080.0	-460.3	1080.0	1111.5
80 25-79	50 Z5-79I Z5-5ZD	503.0	815.0	603.0	513.9		632.5		50.91	64.21	49.53	1386.4	792.1-	1248.3	-602.7	1248.3	1235.2
70 28.95	28.954 28.C76	5 597 8	7.87.5	557.8	502.1	Ω.	666.7		50 • 39	66.83	56.24	1521.7	-7.408	1401.4	-752.2	1401.4	1358.9
86 31.29	31,295 29,993	582.6	743.2	582.6	480.9	•	630.7	!	52.67	68.96	5.0	1622.9	951.5	1514.7	-821.D	1514.7	1451.7
80 31.88	90 31.883 3D.63D	577.6	783.2	577.5		•	844 .4		55.42	69.48	62.06	1647.8	948.9-	1543.2	-838-1	1543.2	482.5
32.45	86 32.499 31.27I	573.5	762.8	571.5	401.2	0	648.6		58.27	69.97	65.11	1674.3	563.7	1573.0	-865.0	1573.0	.CC 58.27 69.97 69.11 1674.3 583.7-1573.0 -865.0 1573.0 1513.6
			:								:						
INCS	INCS INCH DEV	DEV	TURN	AH BER 0	MECA-B	DEFAC 0	MEGA-B	L 055-P	LOS S-P	P02/	EFF-P 6	FF-10	EFF-P	K-1	H-2	H - 3 K	H 9-2
KSPANDEGREE DEGREE DEGREE DEGREE DEGR	DEGREE	DEGREE D	EGREE DI	EGREE S	HOCK		-	OTAL P!	ROFILE	PO1	OTAL T	OTAL S	TATIC				•
1.62	1	15.12	41.68	48.81	.0171	P 5344	0179	BE22-	0075	2.1440	1.0096	1.0107	1.0140	.507	.8679	. 9372	. 5639
10 1.90		15.31	36,29	43,38	.0204	.5229	0318	0068	0113	2.1140	1.0182	1.0202	1.0269	.5211	.8378	.9877	.5881
15 2.24	4 7:38	34.49	31:45	37.76	.0244	.5409	.0097	.0021	0033	2.0611	.9941	.9934	.9892	.5303	.7985	1.0311	
30 3,36	16 7.34	12, 30	15.07	24.01	* C 4 6 4	5879	.1183	.0236	.0142	1.9422	• 5079	.8587	. 8 8 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	547	.6984	1.1448	
80	8 7.24	7.18	14.58	14.63	2280	.5671	1400	-0277	.0115	1.9882	. 4778°	.8549	.8585	.556	5826	1.2782	
36 5.36		5,49	10.65	8.92	.1122	. 5393	.1616	.0305	₩ 533 •	2.0005	. 8439	. 6278	.8262	.551	.6537	1.4005	
86 5.5		4.7	5.32	7.26	.1360	.5524	.2151	. C 3 S 6	.0151	2.0379	.7896	.7673	.7661	.538	.6508	1.4861	
99 2 08	6 6.75	60.9	7.41	6.77	.1432	.5667	.2515	.0438	.0192	2.0313	.7569	.7316	.7332	532	63386	1.5127	
5.3	5 6.67	8.16	99.4	6.38	.1540	4.86 6.38 .1540 .5745 .2793 .0446 .0204 2.0123 .7293 .7616 .7083	.2793	. 6445	.0204	2.0123	.7293	.7616	.7063	.528	1 .6186 1.5374	1.5374	.7734

10/10 F0/PO EFF-AD EFF-P INLET INLET INLET INLET 1.2583 2.0146 85.65 87.00

Rotor Pressure Ratio = 1.1273

11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -	
FAGE 18-16-16-16-16-16-16-16-16-16-16-16-16-16-		
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	# # # # # # # # # # # # # # # # # # #	
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Rotor Pressure Ratio = 1.1433

BASELINE STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

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Rotor Pressure Ratio = 1.1676

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	DIA	DIA-1 . DIA-Z		خ	7.	VH-1	VH-2	1.00	7-0A		-	8-2-8		2-6	- T- A	7	10x	**** YOU YOU X	1.0	7.0
S SPAN! N	z	Z		1 FT/	SEC FI	/SEC F	T/SEC	FT/SEC	FT/SEC	DEGREI	E DEGR	EE DEG	REE DE	GREEFF	T/SEC F	T/SEC F	1/566	FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC DEGREE DEGREE DEGREE DEGREE FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC	T/SEC FT/SEC	T/SEC
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2	25.60		93 431	1.8	380.9	353.4	378,7	248.	2 41	3 35,(07 6	, 23	46,31	04.09.	-512.0-	766.9	-370.3		- 618.5	97529
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Rotor Pressure Ratio = 1.1540

Rotor Pressure Ratio = 1,1803

	DIA-Z V-1 V-2 VH-1 VH-2 VO-1 VO-2 B-1 B-2 B-1 B-2 V-1 V-2 VO-1 VU-2 UV-1 TO-2 U-1 VO	71.489 851.7 853.2 681.8 853.7 510.3	21,961 815,7 830,3 666,7 828,0 470,0 -61,7 35,17 -4,27 19,85 44,18 70,2 1154,7 -240,7 -804,7 710,7 742,9	12,9 ""435,5 ""-68,6 " 33,82" "4,89 " 24,38 " 45,87 "	6.9 351.8 -78.9 29.36 -6.11 34.93 50.29 762.9 1153.7 -436.9	12,5 284,7 84,7 25,05 7,08 7,66 54,60	0.6 233.8 -84.3 21,50 -7.61 49.99 58.48	-625.0 588,3 581,7 583,5 228,4 -75,7 721,45 -7,39 -52,80 -61,39 -	570.2 552./ 565.6 233.4 -71.8 22.71 -7.23 54.63 62.40	30.273 571.4 516.4 520.4 511.1 235.7 7.73.6 24.40 48.22 56.67 65.05 747.7 1211.7 771.9-1078.4 1027.8 1024.8	- 2	FERE DEGREE DEGREE SHOCK TOTAL PROFILE POJ TOTAL TOTAL STATIC	.0000 .1507 . [2060300030096130000000028.23487621	.0000 .1458 .0796 .0203 .0203 .9762 .0000 .0000 2.3699		9.10 35747 50.67 ,0000 ,1341 ,0323 ,0090 ,0090 ,9922 ,0000 ,0000 1.2317 ,6371 ,6637 ,6864 1		9,83 29,12 49,87 ,0000 ,1674 ,0535 ,0176 ,0176 ,8894 ,0000 ,0000 9,9007 ,5677 ,5682 ,8299	12.58 28.83 28.63 52.12 0000 2228 1191 0013 0413 0413 0413 0000 0000 0000 000	14,23 30,14 53,69 ,0000 ,2306 ,0758 ,0267 ,0267 ,9867 ,0000 ,0000 ,2907 ,5294 ,5046	7,88 [5,46 32,62 56,06 ,0000 ,2919 ,1436 ,0513 ,0513	#CORR 10/10 PO/PO EFF = AD CFF = P #C:7A!	INET INET INET I	8M/SEC 135.03 1.0842 1.2563
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Rotor Pressure Ratio = 1.2722

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| 31.5PEED CODE 70.PDINT 8 F VFZ VO'=1 VD'=2 F TOZE F 7/SEC F | |
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Rotor Pressure Ratio = 1.4314

ALREGIC AERODYNAHIC SUHHARY PRINT
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25.601 25.893 618.6 555.9 512.8 551.8 345.8 -67.8 33.98 -7.00 45.31 59.64 729.6 1
70 27,818 27,902 597,3 525
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Rotor Pressure Ratio = 1.3485

		T / V H V V V V V V V V V
등문 등문	77/5EC FT/5EC 6476-6476-6476-651-651-651-651-651-651-651-651-651-65	77.5EC PT/5EC 647.4 518.4 519.
445.9 358.4 474.5 501.6 501.6 501.6 501.6 501.6 474.6 501.6 501.6 474.6 501.6	77/5EC FT/5EC 6476-6476-6476-651-651-651-651-651-651-651-651-651-65	77.5EC PT/5EC 647.4 518.4 519.
	# VEX 6176 FTVB 6176 4 5476 4 5476 4 5476 6 445 6 446 6 616 6 6 6 6	18PECIAL) 19PECIAL) 1987 17755 1961 17775 1961 1961 197777 13.0 1963 1978 1978 1978 1988 1988 1988 1988 1988

Rotor Pressure Ratio = 1.3732

Rotor Pressure Ratio = 1.3705

RUN # 31, SPEED CODE 90, POINT # 1, PAGE 18"-2 V'-1 V'-2 V(0'-1) 16RE FT/SEC FT	STATO	STATOR ANGLES					AIRF	OIL AEF	AIRFOIL AERODYNAMIC SUMMARY PRINT	C SUMMA	RY PRI	F-7	•		23:22:48	_	7	JULY 12,1971
L VM-2 VO-1 VO-2 B-1 B-2 B-1 B-1 VO-2 VO-1 VO-2 VO-1 VO-2 VO-1 VO-2 VO-2 VO-1 VO-2 VO-1 VO-2 VO-2 VO-2 VO-2 VO-2 VO-2 VO-2 VO-2	NASA EN	SLISH										₩ NOS	31	SPEED	CODE 90.	POINT #		E 36.02
C FT/SEC FT/SEC FT/SEC PEGREE DEGREE FT/SEC	DIA-	1 DIA-2		V-2	- M-1	VM-2	V0-1	V0-2	8-1	B-2	B*-1	84-2	V=1.	V2	V01-1	V01-2	2	2-5
3 1002.2 650.8 -45.7 39.61 -2.61 16.96 44.46 622.1 1404.1 -239.8 -983.4 890.5 2.974.3 599.6 -86.6 58.15 -2.09 22.57 47.00 862.9 1403.6 -37.11-1044.9 916.7 3.0 888.1 475.8 -119.9 57.6 -5.53 57.10 48.88 833.6 1443.6 -36.1107.3 3.0 888.1 475.8 -119.9 52.88 -7.69 36.34 52.63 913.7 1463.2 -541.5-1162.8 1017.3 3.0 888.1 475.8 -119.9 52.88 -7.69 36.34 52.63 913.7 1463.2 -541.5-1162.8 1017.3 3.0 886.1 475.8 -119.9 52.89 -7.69 36.34 52.63 913.7 1463.2 -541.5-1162.8 1017.3 3.0 886.2 36.80 8-110.1 27.5 37.5 44.36 55.88 996.3 1503.4 -696.7-1244.6 1117.1 3.0 786.7 368.8 -116.1 27.5 3 -7.33 54.01 61.20 1160.6 1584.4 -696.7-1244.6 1117.1 3.0 786.7 368.8 -16.1 27.33 54.01 61.20 1160.6 1588.6 -958.9-1398.8 1305.2 3.0 736.1 -121.5 29.71 -10.19 56.01 64.77 1155.0 1595.9 -957.6-1443.3 1325.7 3.0 6 679.9 368.1 -121.5 29.71 -10.19 56.01 64.77 1155.0 1595.9 -957.6-1443.3 1325.7 3.0 6 679.9 368.1 -121.5 29.71 -10.19 56.01 64.77 1155.0 1595.9 -957.6-1443.3 1325.7 3.0 6 6700 1.000 0.0000 2.4047 8876 7.725 8800 2.0 6.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	S.SPANIN	Z		FT/SEC	FT/SEC	TISEC F	T/SEC F	T/SEC L	EGREE D	EGREE D	EGREE (JEGREE F	T/SEC F	T/SEC	FT/SEC F	T/SEC F	T/SEC F	T/SEC
2 974.3 599.6 -86.6 38.15 -5.09 22.57 47.00 826,9.1428.8 -317.1-1044.9 916.7 9 949.3 562.0 -108.6 57.16 -6.53 27.10 48.8 853.5 1443.6 -580.1-10874 942.0 988.1 475.8 -119.9 32.88 -7.65 913.7 1443.6 58.10 42.8 8 833.6 1443.6 58.10 17.3 11.2 8 843.0 420.4 -114.8 30.55 -7.75 44.36 55.88 996.3 1503.4 -696.7-1244.6 1117.1 11.2 8 843.0 420.4 -114.8 30.55 -7.75 44.36 55.88 996.3 1503.4 -696.7-1244.6 1117.1 11.2 8 78.5 7 7.7 8 7.7 8 7.8 8 7.8 8 165.8 8 75.4 6 -1333.6 1213.8 12.1 746.7 366.4 -961.1 21.2 27.7 7 7 52.5 161.28 165.6 1548.4 -845.0-1333.6 1213.8 12.1 746.7 366.4 -961.1 -121.5 29.71 -10.19 56.01 64.77 1155.0 1595.9 -957.6-1443.3 1325.7 13.4 8 70.001 1833 .211 0526 0523 9129 0000 0000 2.4047 997.6 -1443.3 1325.7 13.4 8 70.001 1833 .211 0526 0523 9129 0000 0000 2.4047 8876 7700 7923 8880 15.5 0000 1688 0598 0276 0275 9534 0000 0000 2.4047 8876 7700 7923 8880 15.5 0000 1688 0598 0000 0000 2.4047 1659 1.0 121 0526 0527 9534 0000 0000 2.4047 18191 18459 7.700 7923 8880 15.5 0000 0000 2.2049 11524 0555 0555 0554 0000 0000 2.1194 7.8 9000 0000 2.2049 11524 0555 0555 0555 0000 0000 0000 1.1045 05925 05927 0592 0000 0000 0.2049 11524 0555 0555 0555 0555 05000 0000 0.1045 0500 0.0000 0.1045 0.1045 0.1074 0.0000 0.1045 0.1045 0.1047 0.1045 0.1047 0.1045 0.1047 0.1045 0.1047 0.1045 0.1047 0.1045 0.1047 0.1045 0.1047 0.1045 0.1047 0.1045 0.1047 0.1045 0.1047 0.1045 0.1047 0.1045 0.1047 0.1045 0.1047 0.1045 0.1047 0.1047 0.1045 0.1047 0.104	\$ 20.4(39 21.48	-		786.3	1002.2	650.8	-45.7	39.61	-2.61	16.96	94.44	822.1	14041	-239.8	-983.4	890.5	
2 949.3 562.0 -108.6 37.16 -6.53 27.10 48.88 633.6 1443.6 -580.1-1087.4 942.0 688.1 475.8 -119.9 32.88 -7.69 36.34 52.63 913.7 1463.2 -541.5-1162.8 1017.3 10.0 688.1 475.8 -119.9 32.88 -7.69 36.34 52.63 913.7 1463.2 -541.5-1162.8 1017.3 10.0 786.7 368.8 -116.1 27.5 44.35 44.5 1102.6 1102.6 1503.4 -695.7 -1244.6 1117.3 10.0 786.7 366.8 -116.1 27.5 1 -6.39 6.34 51.02 51.00 10.6 150.3 -103.1 26.79 -7.74 52.51 61.28 1165.8 1579.6 -924.9-1383.6 1137.8 12.6 759.1 358.3 -103.1 26.79 -7.74 52.51 61.28 1165.8 1579.6 -924.9-1383.2 1283.2 12.6 759.9 368.1 -121.5 29.71 -10.19 56.01 64.77 1155.0 1595.9 -957.6-1443.3 1325.7 12.5 540.6 150.6 1	10 21.00			i	76.	974.3	599.6	-86.6	38.15	-5.09	22.57	47.00	826,9	1428.8	-317.1-	.1044.9	916.7	
*** *** *** *** *** *** *** *** *** **	. 16 21.5		2 930.2		741	949.3	562.0	-108.6	37.16	-6.53	27.10	48.88	833.6	1443.6	-380.1-	1087.4	942.0	
2 843.0 420.4 -114.8 30.55 -7.75 44.36 55.88 996.3 1503.4 -696.7-1244.6 1117.1 11.2 2 843.0 420.4 -114.8 30.55 -7.75 44.36 55.88 996.3 1503.4 -696.7-1244.6 1117.1 11.2 2 786.7 366.8 -116.1 27.51 -8.39 50.02 59.46 1102.6 1548.4 -845.0-1333.6 1213.8 2 8.1 795.1 26.79 -7.74 52.51 61.28 1166.6 1585.6 -924.9-1385.2 1283.2 2 746.7 366.4 -96.1 20.25 -7.3 54.01 61.91 1166.6 1585.6 -938.9-1385.2 2 8.2 7 368.1 -121.5 29.71 -10.19 56.01 64.77 1155.0 1595.9 -957.6-1443.3 1325.7 2 8.4 679.9 368.1 -121.5 29.71 -10.19 56.01 64.77 1155.0 1595.9 -957.6-1443.3 1325.7 2 8.4 670.0	30 23,3		2 876.4		736.0	888.1	475.8	-119.9	32.88	-7.69	36,34	52.63	913,7	1463.2	-541.5-	.1162.8	1017.3	1043.0
.0 786.7 368.8 -116.1 27.51 -8.39 50.02 59.46 1102.6 1548.4 -845.0-1333.6 1213.8 12 6 759.1 358.3 -103.1 26.79 -7.74 52.51 61.28 1165.8 1579.6 -924.9-1385.2 1283.2 13 6 759.1 358.3 -103.1 26.79 -7.74 52.51 61.28 1165.6 1585.6 -924.9-1385.2 1283.2 13 6 679.9 366.1 -121.5 29.71 -10.19 56.01 64.77 1155.0 1595.9 -957.6-1443.3 1325.7 13 8 OND CALL BOOK SET COMEGA-B LOSS-P POST FFF AD EFF-P M-1 M-2 M1 N 8 OND CALL BOOK SET CALL BROFILE POI TOTAL STATIC STATIC STATIC SET CALL STATIC SET CALL STATIC SET CALL STATIC SET CALL STATIC SET CALL STATIC SET CALL SET CALL STATIC SET CALL SET CALL SET CALL STATIC SET CALL	9.52 08 .	_	3 827.0	850	_	843.0	450.4	-114.8	30.55	-7.75	44.36	55,88	996,3	1503.4	-696.7-	1244.6	1117.1	1129.8
.6 759.1 358.3 -103.1 26.79 -7.74 52.51 61.28 1165.8 1579.6 -924.9-1385.2 1283.2 13.1 746.7 366.4 -96.1 28.25 -7.33 54.01 61.91 1160.6 1585.6 -938.9-1398.8 1305.3 13.6 679.9 368.1 -121.5 29.71 -10.19 56.01 64.77 1155.0 1595.9 -957.6-1443.3 1325.7 13.5 57.1	27.8		Ì		708.0	786.7	368.8	-116.1	27,51	-8.39	50.02	59,46	1102,6	1548.4	-845.0-	-1333.6	1213.8	1217.5
1 746.7 366.4 -96.1 20.25 -7.33 54.01 61.91 1160,6 1585,6 -938.9-1398.8 1305.3 13.6 679.9 368.1 -121.5 29.71 -10.19 56.01 64.77 1155.0 1595.9 -957.6-1443.3 1325.7 13.6 679.9 368.1 -121.5 29.71 -10.19 56.01 64.77 1155.0 1595.9 -957.6-1443.3 1325.7 13.7 13.6 13.6 13.6 13.6 13.6 13.6 13.6 13.6	. 86 29.4(794	•	709.6	759.1	358.3	-103.1	26.79	-7.74		61,28	1165.8	1579.6	-924.9-	-1385.2	1283.2	1282.1
6 679.9 368.1 -121.5 29.71 -10.19 56.01 64.77 1155.0 1595.9 -957.6-1443.3 1325.7 12 CMEGA-B D-FAC OMEGA-B LOSS-P LOSS-P PO2/ EFF-P EFF-AD EFF-P M-1 M-2 M·1 F F E SHOCK E SHOCK B7 0011 1833 .2111 0526 0523 .9129 .0000 .0000-3.7718 .9041 .8876 .7292 1 B87 0001 1699 .1537 .0391 .0390 .9412 .0000 .0000 2.4047 .8191 .8876 .7292 1 S6 0000 1688 .0908 .0276 .0377 .9618 .0000 .0000 2.4047 .8191 .8459 .7366 1 S6 0000 .2049 .1524 .0500 .0275 .9534 .0000 .0000 2.1194 .7700 .7700 .7923 .8089 1 S8 0000 .2049 .1524 .0500 .0500 .9574 .0000 .0000 2.11045 .6995 .6977 .9732 1 B8 0000 .2402 .1575 .0555 .0555 .9586 .0000 .0000-1.1045 .6932 .6682 1.0194 1 EFF-AD EFF-P WCI/A1 INLET INLET LBM/SEC .8 S S S S S S S S S S S S S S S S S S	80 29,91	29,85	-	•	682.1	746.7	366.4	-96-1	28.25	-7.33		61.91	1160.6	1585,6	-938.9-	1398.8	1305.3	1302.8
SHOCK SHOCK OMEGA-B LOSS-P LOSS-P PO2/ EFF-AD EFF-AD EFF-P M-1 M-2 M*-1 M E SHOCK TOTAL STATIC T	30,36	a			645.6	6.679	368.1	-121.5	29.71	-10.19		64.77	1155.0	1595.9	-957.6-	1443.3	1325.7	1321.8
SHOCK E SHOCK E SHOCK E SHOCK E SHOCK E SHOCK TOTAL PROFILE POI TOTAL TOTAL STATIC STAT		:				i					- i				. !	:		
E SHOCK E SHOCK TOTAL PROFILE POI TOTAL STATIC STAT	INC	S INCM	DEV	TCRN NEO	CAMBER (MEGA-B	D-FAC C	MEGA-B	LOSS-P			EFF-P E	FF-AD	EFF-P	X-1	× 12	: :- :-	M2
87 .0011 .1833 .2111 .0526 .0523 .9129 .0000 .0000-3.7718 .9041 .8876 .7292 1 .855 .0007 .1698 .1537 .0391 .0390 .9412 .0000 .0000 2.4047 .8191 .8854 .8663 .7311 1.9000 .0000 2.4047 .8191 .8859 .7311 1.9000 .0000 2.4047 .8191 .8859 .7351 1.9000 .0000 2.4047 .8191 .8859 .7351 1.9000 .0000 2.6000 .1688 .0908 .0276 .0375 .9731 .0000 .0000 2.1190 .7240 .7492 .8880 1.98 .0000 .2049 .1524 .0500 .0554 .9478 .0000 .0000 2.1190 .7240 .7492 .8880 1.98 .0000 .2393 .1888 .0654 .0654 .9478 .0000 .0000 2.1194 .6995 .6977 .9732 1.9000 .0000 .2393 .1888 .0654 .0654 .9478 .0000 .0000 .21045 .6995 .6977 .9732 1.9000 .0000 .2402 .1575 .0844 .0844 .9421 .0000 .0000-1.2798 .6724 .6539 1.0100 1.0001 .00000 .0000 .0000 .0	SSPAN DEGHEE	- DEGREE	DEGREE	DEGREE	DEGREE !	SHOCK			OTAL P			TOTAL 1	OTAL	TATIC				
-3.1825 10.35 43.23 53.85 .0007 .1698 .1537 .0391 .0390 .9412 .0000 .0000 7.5706 .8564 .8665 .7311 13.7 8.39 43.69 52.40 .0006 .1591 .1069 .0277 .9618 .0000 .0000 2.4047 .8191 .8459 .7366 15.59 -2.58 7.53 40.57 .0006 .0001 .0000 2.000 .7223 .8069 15.59 -2.59 8.23 40.57 .0000 .1669 .0275 .0275 .0000 .0000 2.1190 .7240 .7249 .8800 15.52 -5.09 8.05 38.34 49.88 .0000 .2569 .0576 .0577 .9518 .0000 .0000 2.1190 .7240 .7240 .7249 .8800 15.52 -5.17 12.21 34.53 52.08 .0000 .2909 .1524 .0550 .0550 .9574 .0000 .0000 2.1190 .7240 .7249 .8800 15.52 -5.17 12.21 34.53 52.08 .0000 .2393 .1888 .0654 .0654 .9478 .0000 .0000-1.1045 .6995 .6977 .9732 15.52 -5.60 13.48 39.90 56.06 .0000 .2402 .1575 .0555 .0555 .9586 .0000 .0000-1.1045 .6932 .6682 1.0194 14.16 -2.60 13.48 39.90 56.06 .0000 .2402 .1575 .0555 .9586 .0000 .0000-1.2798 .6724 .6539 1.0100 1. INLET	6 -2	75 .14	5 13.79	1 42.23	55.87	.0011	.1833		.0526	.0523	:	0000	0000	3.7718		.8876	.7292	1.2422
-3.3137 8.39 43.69 52.40 .0006 .1591 .1069 .0278 .0277 .9618 .0000 2.4047 .8191 .8459 .7366 1 -5.59 -2.58 7.53 40.57 50.66 .0001 .1669 .1121 .0312 .9634 .0000 .0000 2.820 .7700 .7923 .8089 1 -6.23 -3.09 8.28 38.31 49.57 .0000 .1668 .0908 .0276 .0275 .0000 .0000 .21190 .7700 .7700 .7722 .8869 1 -6.23 -3.04 9.06 35.91 49.88 .0000 .2402 .1584 .0554 .0057 .9574 .0000 .0000-11045 .6932 .6682 1.0194 1 -5.52 -5.17 12.21 34.53 52.08 .0000 .2402 .1575 .0555 .9586 .0000 .0000-1.1045 .6932 .6682 1.0194 1 -2.51 -2.60 13.48 39.90 56.06 .0000 .3083 .2376 .0844 .9421 .0000 .0000-1.2798 .6724 .6539 1.0100 1 INLET INLE	10.5	18 - 25	5. 10.35			2000	.1698		.0391	.0390	- 1	0000	.0000	7,5706		.8663	,7311	1,2652
-5.59 -2.58 7.53 40.57 50.66 .0001 .1669 .1121 .0312 .9634 .0000 .0000 2.820 .7700 .7923 .8089 15.23 -3.09 8.28 38.31 49.57 .0000 .1688 .0908 .0276 .0275 .9731 .0000 .2.1190 .7240 .7492 .8800 15.24 -3.09 8.28 38.31 49.57 .0000 .1688 .0908 .0276 .0275 .9731 .0000 .2.1190 .7240 .7492 .8800 15.52 -5.47 9.06 35.91 49.88 .0000 .2000 .0000 .0000 .0000 .0000 .1000 .0000 .1000 .0000 .0000 .0000 .0000 .0000 .1000 .00000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0				Ę	52	.0006	1591		.0278	.0277	,9618	Ī	• 0000	2.4047		. 8459	.7366	1,2781
-6.23 -3.09 8.28 38.31 49.57 .0000 .1688 .0908 .0276 .0275 .9731 .0000 2.1190 .7240 .7492 .8800 16.23 -3.09 8.28 38.31 49.57 .0000 .1688 .0908 .0276 .0500 .0500 .0000 .0000 .2190 .7492 .8800 14.28 -5.04 9.06 35.91 49.88 .0000 .2000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .1000 .1000 .0000 .0000 .0000 .0000 .0000 .0000 .1000 .0000 .0000 .0000 .1000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .5325 .6420 .5955 1.0004 1. INLET IN		•	-	0.0	500	1000	.1669	- 1	.0312	.0312	9634	Ĭ	.0000	2,8220		. 7923	.8089	1.2936
		•	æ		647	0000	.1688		.0276	.0275	.9731	Ĭ	.0000	2.1190		.7492	.8800	1.3239
-5.52 -5.17 12.21 34.53 52.08 .0000 .2393 .1888 .0654 .0654 .0978 .0000 .0000-1.1045 .6932 .6682 1.0194 15.51 -3.85 14.22 35.58 53.78 .0000 .2402 .1575 .0555 .0555 .9586 .0000 .0000-1.2798 .6724 .6539 1.0100 14.16 -2.60 13.48 39.90 56.06 .0000 .3083 .2376 .0844 .0844 .9421 .0000 .00005325 .6420 .5955 1.0004 1. NCORR WCORR TO/TO PO/PO EFF-AD EFF-P WCI/A1 INLET INLET INLET INLET INLET INLET INLET LAM/SEC . S. S. S. S. S. S. S. S. S. S. S. S. S	_	- 1	90.6	į	49.	.0000	-2049		.0500	0200	P256	0000	.0000	****	- 1	.6977	.9732	1,3585
1 -3.85 14.22 35.58 53.78 .0000 .2402 .1575 .0555 .0555 .9586 .0000 .0000-1.2798 .6724 .6539 1.0100 1.0000 .0000 .0000 .0000 .5325 .6420 .5955 1.0004 1.0000 .0000 .00005325 .6420 .5955 1.0004 1.0000 NCORR TO/TO PO/PO EFF-AD EFF-P WCL/A1 INNET	,		7 12.21		52.	0000	.2393		•0654	.0654	9418	.0000	-0000	1.1045		.6682	1.0194	1.3778
6 -2.60 13.48 39.90 56.06 .0000 .3083 .2376 .0844 .0844 .9421 .0000 .00005325 .6420 .5955 1.0004 1. NCORR WCORR TO/TO PO/PO EFF-P WCI/A1 INLET INLET INLET INLET LUB/SEC RP LBM/SEC 8 SOFT DATE 169.67 1.1556 1.4963 78.41 79.59 38.83	3°C= 1	-4	14.22	35	53	0000	2402		0555	0555	9286	0000	-0000	1.2798	- 7	6539	1.0100	1,3773
1 NCORR TO/TO PO/PO EFF-A LBM/SEC 11556 1.4961 78.4	7. t- 'es	9	=	39.90	•	0000	.3083	.2376	• 0844	.0844	.9421	0000	• 0000	-,5325	.6420	. 5955	1.0004	1.3754
LBM/SEC INLET INLE			T ORR T		1	E-AN FE	100	741										
LBM/SEC % 1556 1.4963 78.4		INLET	NET			ET	ET LBM	/SEC								•		
169.67 1.1556 1.4963 78.41 79.50		MOG	NAME				200	1										
			69.67	1556 1	. 404.	18.41 79		- d										

Rotor Pressure Ratio = 1.5618

	CTATOD	CTATOP ANGI FC	•			11	ATR	TOT! AFE	DONNAM	C SIMMA	DY DOTA	<u>.</u>			3:24:26		, IIII,	2.1971
Z	NASA ENGLISH)	(SPECIAL)	3			•					₩ Windows	31.	SPEED (ODE 30	POINT #	2,PAC	RUN # 31.5PEED CODE 90.POINT # 2.PAGE 36.02
i	IAL	7-2	7-7	2- 2	Š	VM-2	V0-1	V0-2	8-1	9-2	8'-1	81-2	V -1	V 2	V0'-1	V02	1- 0	0-2
S SPANIN		Z	FT/SEC	T/SEC	FT/SE	FT/SEC	FT/SEC !	T/SEC C	EGREE D	EGREE D	EGREE D	EGREE F	T/SEC F	1/550	T/SEC .F	T/SEC F	T/SEC F	7/SEC
ما	20.409	9 21,489	1	4 861.	7 74.	860.8	660.2	-38.5	41.44	-2.56	17.06	48.56	782.2	1300.8	-229,3	-975.2	889.7	936.7
2	21.008	3 21,96	1 950.9	9 826	8 725.6	824.3	614.6	-63.8	40.26	11 · 1-	22,55	51.09	786.1	1312,5	-301.2-	1021.1	915.8	957.3
₽	21.589	w	2 910.9		3 708	796.5	579.7	-78.1	39.52	-5.61	27.18	52,97	7.062	1322.9	-361.4-	1055.9	941,1	977.9
8	23,314	23.902	٠.	5 755,9	69	751.2	504.1	-84.3	36.25	-6.40	36,68	56,29	857.4	1353.0	-512.2-	1126.2	1016.3	1041.9
2	25.601	1 25.89	_	7 722.	2 671.4	717.9	459.7	-79.1	34.40	-6.29	44,35	59.27	938.9	1405.2	-656.3-	-1207.9	1116.0	1128.7
2	27,816	3 27,902		5 687.	4668.5	682.9	418.0	-78,7	32,01	-6.57	06.64	65,19	1038,7	1464.1	-794.7-	1295.0	1212,6	1216.3
	29,408	~	2 793.	_	9	657.3	424.0	-59.1	32.29	-5.13	51.97	63,87	1089.2	1492,5	-858.0-	1339.9	1282.0	1280.8
8	29.914	8		9.049 9	9	638.6	434.9	-50.4	33,92	-4.51	53.34	64.71	1083,6	1495,1	-369.2-	1351.8	1304.0	1301.5
8	30.382	2 30 29.	3 762.	7 590	3 624.3	586.7	438.1	-63.9	35.06	-6.25	54.84	67.03	1084.2	1503.9	-886.3-	1384.4	1324.4	1320.5
	INCS	INCM	DEV	TURN	CAMBER	OMEGA-B	D-FAC (MEGA-8	Loss-P	Loss-P	P027	EFF-P. E	FF-AD	EFF-P	M-1	M-2	M - 1	R OMEGA-B D-FAC OMEGA-B LOSS-P LOSS-P PO2/ EFF-P. EFF-AD EFF-P M-1 . N-2 M'-1 M'-2
* SPAN	DEGKEE	DEGREE	*SPANDEGKEE DEGREE DEGREE	DEGREE DEGRE		SHOCK			TOTAL P	ROFILE	POL	DIAL I	OTAL	TATIC				
9	89	2.03	3 13.84	00 - 11 11	0 55.87	.0024		.1408	.0351	.0345	9442	0000.	0000	.5771	.8782	.7463		.6903 1.1256
2	-1.04	1.90	⊣	0. 44.7	0. 53.85	0021		.1129	. 0288.	. 0282	. 9564	.0000	0000	.6527	.8317	. 47158		1,1363
	h6:	4 2.00	0	-	52.	.0022		.0777	• 0202	.0197	.9733	.0000	• 0000	.7425	•7965	#269*		1.1444
8	-2.21	9.	8.8	1. 42.05	20	0015		. 0431	.0120	.0116.	. 9867	.0000	.0000	. 8364	. 7436	.6538		1.1708
8	-2.34	18.	0 9.7	69.0h h	46	.0019		.0315	9600.	0600.	.9910	.0000	00000	.8860	•7065	.6222		1.2106
2	23.74	5.5	0_10.8	8 38.5	8.49.88	10007		1040	.0158	.0156	9870	.0000	0000	8342	1409.	. 5907		1.2579
8	•20	÷.	4 14.8	1 37.4	2 52.06	90000		.1126	•0392	.0390	9696	0000	•0000	•6699	.6835	.5622		.9402 1.2713
8	2.05	1.9	3 17.0	4 38 4	2 53.76	0008		.1107	.0392	.0389	.9712	0000	00000	.6890		. 5429		1.2671
8	1.12	2.7	6 17.4	is 41,3	1 56.05	94. 7000. 20		.1722	.0618	38 .1722 .0618 .0615 .9570 .0000 .0000 .6230 .	.9570	• 0000	• 0000	.6230	.6518	n26h.		1,2672
	; -2	NCORR	MCORR	10/10		FF-AD E	FF-P WC	L/A1										
			- 1		INLET	NET	NET LBY	4/SEC										
	•	RPM	LBM/SEC			THOS:	× .	77.										
	-	9991	12.19	167.24 1.1706 1.5956	1,5956	83.67 8	4.72	5.87										

Rotor Pressure Ratio = 1.6298

STATOR ANGLES	AIRFUL AERODYNAMIC SUMMARY PRINT	14:55:82
ISH (SPECIAL)		RUN # 31.5PEED CODE 90.POINT # 4.PAGE 36.01
DIA-1 DIA-2 V-1 V-2 VH-1 VH-2 VD-	-Z B-L B-Z B+=1 B	-Z1-1 - 1-1 - 1-1 - 1-1 - 1-1 - 1-1 - 1-1 - 1-2 - 1-1 - 1-2 -
PAN IN FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC	EC DEGREE DEGREE DEGREE DEG	EE FI/SEC FI/SEC FI/SEC FI/SEC FI/SEC FI/SEC
9 98,6 81 9,3 728,1 818,8 668	9.9 42.57 - Z.02 - 16.89 P.	.71 761.0 1286.Z =221.1 -965.8 - 889.4 - 936.1
21.008 21.961 947.5 783.6 713.6 781.1 623	1.1 41.13 -4.49 22.31 5	.51 771.7 1283.8 -292.7-1018.6 916.0 957.5
2 905.5 757.2 687.4 753.0 589	9.1 40.60 6.00 27.09 5.	.53 773.1 1298.1 -352.0-1057.1 941.3 978.1
2 837.2 715,3 657.5 710.5 518	2,5 38,24 -6,62 37,16 57	.72 825.0 1330.3 -498.3-1124.7 1016.5 1042.2
. 25,893 805,8. 690,1 645,4 685,9 402	5.3" 36.79 "-6.35 " 44.48 " 61	.36 704,5 1386,8 -633,7-1205,3 1116,2 1129,0
2 784.0 659.0 644.6 654.5 446	6,9 34,696,70 49,92 63	2 -76.9 34.69 -6.70 49.92 63.16 1001.8 1449.6 -766.7-1293.4 1212.9 1216.6
451.Z 637.7 454	8,7 34,93 -4,36 SI.80 6	-38-1053:0-1474:8-827,4-1329:8-1282.Z-1281:
6 784.1 620,7 630,2 619,5 466	8,2 36,51 -3,52 53,05 69	.19 1048.6 1476.2 -838.0-1339.9 1304.3 1301.8
768.9 574.9 607.8 572.3 470	470.9 -53.8 37.77 -5.41 54.55 6	67.39"1048,1 '1489.2""853,8-1374,6 1324,7 '1320.8"
TURK CAMB	1-8 LOSS-P LOSS-P POZ/ EFF	TR OHEGA-8 0-FAC OMEGA-8 LOSS-P LOSS-P POZ/ EFF-AG EFF-AG TEFF-AG MAI MAK
DEGREE DEGREE DEGRE	TOTAL PROFILE POI TOTA	L TOTAL STATIC
3.15 14.38 44.59 55.8700373430	046	9685 7051
2.77 10.95 45.62 53,84 .0031 .3543	744. 0360. 8960.	
.18 3,12 8,95 46,60 52,44 ,0036 ,3542	963	3 7906 6509-
8,59 44,87 50,66 ,0036 ,3453	.0119 .0109 .9872	.8689 .7282
.09 3,23 9,68 43,13 49,55 ,0057 ,3551		.0000 .9016 6971 .5904
2,22 10,77 41,39 49,89 ,0035 ,3803	.9867	\$195. 7979.
4164	9696	.7043 . 6814 5407
18,04 40,02 53,78 ,0043 ,4372	.0431 .0415 .9684	. 0000 7033 . 6689
5,48 18,27 43,18 56,45 ,0042 ,4988		6502 6536 4609
TANTAGE BESTER CANDOL OF COT OF BROOM BOOKS		
INLET INLET INLET		
	.1	
	1	

Rotor Pressure Ratio = 1,6644

STATOR ANGLES		AINTOIL AEROCTMANIC SUMMANT PAIN	DE DIMMHIC SO	HMARY PRIN		7:96191	2014 12114/1
NASA ENGLISH (SPECIAL)					RUN .	31.SPEED CODE 90.POINT # 5.PAGE 36.02	# 5,PAGE 36.02
DIA-1 - 614-Z V-1 V-1	VH-1 VH-Z	VO-1 VO-2 B-1	8-1-8-2	10.8	8 -2 A	Z-, DA 10, -1 AD, -2	
Ξ		TISEC FTISEC DI	GREE DEGRE	E DEGREE D	EGREE FT/SE	FT/SEC FT/SEC FT/SEC DEGREE DEGREE DEGREE DEGREE FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC	FT/SEC FT/SEC
9 20 400 Z1 488 865.4 730.8	189	893.4 - Z1.8	12.06 -1.71	71-16-79	16.79-52.67-712	772.4 1204.8 205.8 205.1	689.2 436.2
430.0		F.CC. 0.1F0			_	. 1427.1 =2/4.3=1014.	0.007
ŧ	ĺ	611.2 -75.1	43,51 -6,42			724.3"1246.9 -329.4-1052.	740.6- 977.3
30 23,314 23,902 603,4 630,1	587.6	547.8 .72.9	45.99 -6.65	65 38,52	60,68 751	.2 1278.0 -467.9-1114.	1 1015.7 1041.3
25,893 788,2.		521,9 -70,1	. 9 94	•	62,57-837	,3 1350.0 -593.5-1198.2	1115.4 1128.1-
2 776,5	.3 593,0 604,4	501.4 -68.7	40,22 -6,48		50,13 64,79 925	6 1419.4 -710.6-1284.3 1	1 1211.9 1215.6
29.382 796.1	8:009 2	522.3 -43.0		07-51:63	194-44-59-	4-1454:7-4758:9-1323:	1201:2-1280:1-
4 790.4	.3 581,1 580.5	535.6 -28.5	42.67 -2.	76 52,88	66.12 962	9 1453.8 -767.7-1329.3	1 1303.3 1300.7
30.293	563.0	540,7 -34,2	-34.2 43.84 -3.53	53-54;28-	-67.5996	54,2867,59-964,4 -1464,7782,9-1354,0-1	1-1323,7-1319,6-
	CAMBER OMEGA-B	D-FAC OMEGA-8 1	.055-P 1.055	-pp02/	r-ddi. d-ddi	OHEGA-8 D-FAC OMEGA-8 LOSS-P LOSS-P-PO2/- EFF-P-FF-ADEFF-P	
MSPANDEGREE DEGREE DEGREE DEGREE		<u>-</u>	TAL PROFI	LE POI T	OTAL TOTAL	TOTAL PROFILE POI TOTAL TOTAL STATIC	
2,69 5,61 14,69 46,77 55,87	77-55:87 50077	4507 -1955		-6926-89	0000	JO: 6360: 8445: 621	10545-120545-
10 2,20 5,13 10,87 48,13	13 53.84 .0070	4364 .1957	6640.	•	0000	-	
16 3.03 5.97 8.50 49.93	ţ	.4417 -1593	. 0415	į	0000	. 1747	ı
7.54 6.57	50.67	•	.0150	•	0000 0000	6942	•
45.6 46.6	49.54	4350 .0492	.0150 .0084	848	0000		.7193
_	40.91	.4596 .0743	.0245 .0173	•	0000 0000	.8341 ,6637	1 .7922 1.1932
8.93 15.82 45	0520 05200	ľ		ľ		10 .7257 .6762 .5050	. 8222
80 10.59 10.54 18.85 45.4	3 53,84	.5083 .1486	.0527 .0422	22 .9616	0000 0000	.7041 .6674	4 68131 1.2049
96 79.96 11.49 20.15 47.3	37 56.06 .0299	1481 9645	.0663	9855 5550	. 0000 . 0000	30	- 8122 1.2084 -
INLET		INET INET LONISEC					
LBM/SEC	ĺ	S 50FT					
#/ 00 P A 10 I A 20 A R 1	00.00 9/010 13/001						

Rotor Pressure Ratio = 1.7316

STATOR ANGLES	. E S				AIRFO	AIRFOIL AERODYNAMIC SUHHARY PRINT	DYNAMIC	SUMMAR	Y PRINT			25	20:31:43	7	JULY 23.1	1471
NASA ENGLISH	I SPECTALT			i i						RCN #	3213		ė	Ė	6, PAGE 36102	20190
- DIA-1 DIA-2		Z-A	× ₩-1	VH-2		X-0A	8-1	8-2	B 1 - 1				VO1 V			2-1
t	PY7SEC	235/44	1/SEC_77	T/SEC P	T/SECTFT	7SEC DE	GREE' DE	GREE DE	GREE DE	٠	/SEC_FT	FT/SEC-F1	INSEC FT/SECT	\21 \J	SECPT	350
5 20,409 21	489 961.	4 710.3	668.3	709.9	691.2	-24.7	45.97	66.1-	16.45	53,52	676.9 1	194.2 .	1194.2 -197.3 -960.2	,60.2 8	88.5	3.5.5
10 21,008 21,	1926 196	4.4.4 - 1	662.3	677.3	647,3	-51.2	かつ・サナ	-4.04	21,99	56.07	714.7 1	214.0 .	.267,3-10	07.2- 9		-1.956
- 18 21.589 22	432 881.7	4.059 7	629.2	646.2	417.6	-76.5	4.48	-6.78	27.14	58,45	708.1 1	1235.9 -	-322,2-1053	0	939.9	76.6
	902 7916	5 597.9	_	591.0	•	-90.7	.90.7 44.78 -8.73 39.13 62.42	-8.73	39.13	62,42	724.6 1		-457,4-13	1131.5-10	15.0 7	- 9.040
- 60 25,601 25	25,893 781.5	3 597.6		590.6	-	-91.0	43,62	-8.76	45.48	64.14	807.1 1	•	-575.4-1218.3	118.3 11	14.5	127.2
70 27,818 27	902 776:0	579.8.	ł	573.3	543,3	-86.4	****	-8.57	50.31	1	867.7-1		-667.7-1301;	101.112	1:0-1	-14:47
- 88 29,408 29	,382 785.5	5 571.7	543.2	568.2	567.5	-62,5	46,25	-6.28	52,69	67,05	896.2 1	1457.0	-712,8-1341,7	141.7 12	80.3 1.	279.1
80 29,914 29	29.056 780.2		_	557.2		48.8			54,08				-726,3-13	_	302,3 1	. 8 . 662
~	-	5	513.5	543.2	578.1	S		-4.79		68,29	904.5	1468,5	-744,5-1364,3	~	322.7	318.8
	!	i			•									!	:	!
INCS 12	INCH DEV	1088 C	CAMBER OF	FGA-B C	OHEGA-B D-FAC ONEGA-B LOSS-P LOSS-P	EGA-B L	055-P L		P02/ E	EFF-P EFF-AD	F-AD E	医牙牙中的	- - -	X-2		H. = 2
SPAN DEGREE DEGR	REE DEGREE	DEGREE DI	GREE SH	SHOCK	: •	10	TOTAL PR	:	PO1 T0	TOTAL TO	TAL ST	ATIC		İ	1	
5 3.60 6.52 14.41 47.96 55.86	1.52 14.41	94.74	55,86	.0099	.4423	1012.	.0524	6650	1226	• 0000	.0000 .6294	. 6294		Ī		1.0126
10 2.99	1.92 11.05	89.84	53,63	•0088	•	.2089		0150	.9269	0000	0000	,6306	640B*	1	6242 1	1.0294-
7 46.65 81	1,88 6.19	51,26	52.47	.0117	8494	.1733	1540.	.0420	1646		0000	.6853		. 7122.	.6162 1.	4940
30 6,32	9.31 6.50	. 15965 . (50,67	.0225		-0742		.0144	. 7602			. 9098	,	1	1. 6229	-5010.
01 98.9 08		52,38	49.58	.0340	. t 0 1 t	.0700		.0109	.9819	0000	0000	.8653	5699	. 5025	1 9689	, 1385
N 8.75	16.8 8.91	10:65	16.64	+0526	.5215		.0342	-0110.	. 9736	0000.		0Z09 •	:-	Ī	7	
. 86 13.62 14	4.08 13.61	52.153	52.03	0990	.5528	.1492		.0289	49621	0000	0000	.7297			.7539 1	.2017
80 15,42 15	.33 16.62	52,59		.0715		.1618	.0573	.0320	. 9256	.0000	. 0000	. 7139	6539	ľ	_	. 1985.
91 09 41 98 .	.00 18.88	53.18		9890.	1985	.1762	P 6 9 0 •	,0386	.9569	0000	0000	• 6958	.6462	* *9**	7558 1	.2026
	000	04.0		7 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		•						 				
13 18 1	IN ET	TNET THET T	ET	EY IN	NET INCET LOH/SEC	SEC										
X CE	BH/SEC	•		, 	808	,										
4177	9977. 149.95 1.2034 1.4859	.2034 1.4		79.05 80.54	54 31,32	32										

Rotor Pressure Ratio = 1.7483

STATOR ANGLES	NGLES					ATRE	TI AER	DOYNAHI	AIRFOIL AERODYNAHIR SUMMARY PRIN	RY PRI	- 2			16:57:3			13,197
MASA ENGLISH (SPECIAL)	SH (SPECIAL)	:14F3									₹ 2 2	- C	SPEED	SI, SPEED CODE 90, POINT #	POINT		6, PAGE 36.02
DIA-1	DIA-2 V	>	HA Z	7	VH-2	1-0/	VO-2-07	8-1	VO-1 VO-2 B-1 B-1 B-2 B-2 B1-1 B1-2	1.00	8 -2	1 - 1	7:17	_ ^ + z Z ^ O , = 1 ^ O , = Z C = 1 C = z C = 1	Z0A	-5-	7-0
K.SPANIN IN	N . FT/:	SEC F1/5	FT/SEC FT/SEC FT/SEC	EC FT/	SEC FT.	SEC FI	1SEC D	EGREE D	EGREE	EGREE	DEGREE	F1/5EC	FT/SEC	PT/SEC FT/SEC PT/SEC DEGREE DEGREE DEGREE PT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC	77/SEC 1	FT7SEC	F1/5EC
1:199 h:569 0:096 68b:12 60b:02 5	21.489	0.0	30 P.S	1:1	2.56	2.949	-15.5	10.18	-1:58	18:18	53:07	888	11177:10	188.4-1177.6-191.8950.4-898.0-935.0-	+-056 ···	999	935
10 21.008 21.96	21,961 9	925.0 66	665.6 65		663.8	652.9	-47.5	44,89	-4.12	21,73	56.49	705.9	1203.0	1203.0 -261.2-1003.0	-1003-0		. 955
15"21,589.22,432		883,5 7 63	;	1	634.8	1. 629	-72.3	44.95	.Z5 9 9	26:77	- 58,79	h::102	1225.8	17225.8 -315.2-1048.3	-1049.3	- 939.3	976.
30 23,314 23,902		793.2 58			584.9	1,995	-73.2	45,53	-7.13	38,88	62,28	714.0	1257.4	-448,3-1113	-1113.1	1014.4	1039
. 109 52 09	25.601 25.093 - 783.7	:	:	557,85	585.4	5.055	-71.6	44.62	. P. 98	45,28-	- 63,96	. 262.	1333,6	9 "1333.6" -563.4-1198	-1198:2	1113.9	1126.
70 27,818.27,902	27.902 78				_	557,7	-68.7	45.50	-6.82	44.96	65,89	852.3	1405.2	1405.2 -652.6-1282.	-1282.6	1210.3	1214.
85 27 408 29 382	Γ	192.8-57	Ì	543.4-5	P .0 .	377.3	-44 h	-46:73-	4:80	-52:27	66:73	180	1.443.8	7.9-1443.8-4702.2-1326.3-	1326:3	7279:5	-1278.
90 29 914		788.7 56			561.5	986.6	139.4	48.07	10.4-	53,60	67,24	888.2		1451.4 -714.9-1338.4	-1338.4	1301.5	1299.
- 86'30,382'30,293	30.293 781;	m	547.5" 51	512.6 5		589,6	-45°9	44,00	9.50	55,01	P1.89 -	893.	1466,3	55.01 - 68.14" 893.9" 1466.3 "-732.3-1360.9	-1360.9	1321.9	1318,0
										•	;	1	1				
INCS INCH	INCH	101	DEV TURM CAMBER		34-8 D	-FAC DH	EGA-B	_d_SS07	DHEGA-B D-FAC DHEGA-B LOSS-P LOSS-P	P02/	. EFF-P	EFF-AD.	. E F F 6 F	PO27 EFF-P. EFF-AO EFF-P	7 . H		7- 4
MSPANDEGREE DEGREE DEGREE DEGREE	EGREE DEGF	RE DEGR	LE DEGR	EE SHOCK	×		•	OTAL P	PROFILE	P 0 I	TOTAL TOTAL	TOTAL	STATIC				
4.11	7.03	3.12 47	.7655		13	4559	.2164	.0539	1150	9201	0000	0000	2469- 0000	ľ	į	01000	866
3,53	1 . 94.9	1.32 49	101 53		~	4703	.2141	.0546	.0520	.9254	.0000		.6357	.8087	.5633	69199	6159 1.018g
4.39	7 7,33 8,43 51,47 52,45	3.4351	.47 52			4800	.1824	0475	.0440.	9410	.0000	0000	1	7715	. 5403	6101	- 4900-1-10199
7.06	10.05	8.09 52	52.67 50		.0269	4811	.0778	.0217	.0142	.9791	.0000	•	.8615	.6831	. 4972	66123	1.0606
7,87	:	9.05 51	51.60 49	49.57	8140	. 9684	.0787	. 0239	.0112	.9796	.0000	1	8553	6703	8464	. 6764	111189
9.81	13.04 10	•			0635	5259	.1174	.0386	.0177	1074.	0000	0000	.7825	.6623	4803	i	101677
51.4.15	14:58	5.0851	51:53 52	1	.0721	5538	64910		.0323	. 9575	0000	0000	2507		4714	1946:	1 89
_	15,81	17.61 52	52.08 53		\$7.00	5687	.1759	.0624	.0347	9554	.0000	00000	.6920	.6604	4616	.7436	1.190
15.21	19.91		53,50 56	•0•	.0767	.2165	. 1919	0690.	.0414	.9523	0000	0000	.6724	6522	94416	. 7461	1.198
	W.C.D.R.	10/10	Wrose	E F 5 *	In EFF	- P - W.C 1/	-1 ×										
	INLET	INLET	INLET	INE		INLET INLET LBH/SEC	SEC										
	LBH/SE	LBM/SEC			1	SAFT											
	149.55	1.207	1.2071 1.6984		78.62 80.34		95										

Rotor Pressure Ratio = 1.7664

(SPECIAL)	1 DIA-Z V-I V-Z VO-I VH-Z VO-I VO-Z B-I B-Z B-I D-Z V-I V-Z VO-I VO-Z VO-I VO-Z VO-I VO-Z VO-I VO-Z VO-I VO-Z VO Z VO-I VO-Z VO Z VO-Z VO Z VO-Z VO Z VO Z VO Z	1038.0.1008.7 807	23,902 950.3 928.8 777. 25,893 904.0 880.9 763.	832.7 784.1 722	29,856 814,4 755,9 699, 30,293 763,5 661,3 636,	**************************************		48 9.25 43,66 52.	2.77 8.48 39.91 49.	-2.75 11.69 37.56 52. -1.38 13.91 38.35 53.	
NGLES	DIA-1 N 20-409	21,008 21,961	23.314 23.902	27.818 27.902 -29.408:29.382-	29,914 29,856 30,382 30,293	THCS THCH DEGREE DEGREE D	-2,43 .50	-2.4648	-4.40 -1.27	-3.29 -2.75	

Rotor Pressure Ratio = 1.7142

FUN # 31.5PEED CODE 10.POINT # 2,PAGE 36.02	EE SHOCK 87 20064 3192 1301 0324 0306 9437 0000 0000 7585 8937 7330 7344 1.2072 85 0064 3492 1301 0324 0306 9437 0000 0000 7585 8937 7330 7491 1.2150 86 0064 3492 1301 0324 0261 0246 9502 0000 0000 7995 8937 7730 7741 1.2153 87 0064 3468 0077 3665 0072 3540 0077 0106 0000 0000 8849 8609 7779 6476 8779 1.3017 87 0072 3540 0077 3665 00167 0166 8868 0000 0000 88609 7779 6476 8779 1.3017 87 0072 3645 00508 0167 0153 9652 0000 0000 88609 7779 6476 8779 1.3017 87 0071 4664 0868 0307 0262 9760 0000 0000 7790 6775 9778 1.3515 87 0071 4664 0868 0307 0262 9760 0000 0000 7790 6755 9788 1.3515 88 8154 8284 3568 888
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NGLES (SPECIAL) DIA=2 (SPECIAL) DIA=2 (Y-1AL) N 21-489 1070-4 21-761 1029-0 22-432 991-1 23-902 991-1 27-902 837-9 27-302 837-9 27-302 837-9 27-302 837-9 27-302 837-9	NCH DEV TURN CANB 2,92 12,35 46,42 55 2,65 10,55 46,72 53 2,83 9,02 46,25 52 2,72 8,46 44,25 52 2,72 9,98 42,35 49 1,45 9,03 42,42 49 1,45 9,03 42,42 49 1,45 9,03 42,42 49 1,45 9,03 42,42 49 1,45 9,03 42,42 49 1,45 9,03 42,42 49 1,45 11,40 52 6,23 17,94 44,24 56 1,10,67 10,70 p0/p0
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X 25 25 25 25 25 25 25 25 25 25 25 25 25	PAN 5 5 5 8 8 8
sel i i i i	* #4 {

Rotor Pressure Ratio = 1.8000

BASELINE STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

JULY 23,1971	7	988,1	,0-1155;9-1017;1-1063,3-	1182,2 1045,3 1086,1	255,2 1128,6 1157,3	352,4 1239,5 1253,7	152 2 1346 1350	528 9 1948 4 1445 5	242. 14/1.0 1400.	H-2 H'-1 H'-2		-	.7104 1.	.7124 1.	7608	. 8348	Ľ	5326 ,9415 1,3609	5087 9313 1.3527	1 .732/ 1.		
20:24:55 ED CODE 10:POI	2 VO = 1 VC	9 9 -254 8-11	8 -328	.9 -388.7-	165- 9	D.4 _666.4-1352	7 4 895 2-151	906	5,8 .725,2-1	-		~	881	. 8442	. 7923	,7778	8855 7273	•	7703 7031	•		
* 35.SPE	V 1 V	7 807,1 139	1 816,9 1 400	5 820,8 1408	-	972,2 1540	1076 9 159	2 1111.0 1647.6	7 1114,7 164	EFF-P EFF-AD EFF-P	TOTAL STATIC	0000	0000	. 0000	. 0000	. 0000	0000	• 0000	• 0000	• 0000		
RY PRINT RUN	8 - 1 8 - 2 cc. 2	6.62 [4.8]	23,69 55,6	28,26 57,0	37,19 59,6	43,27. 61.4	50,66 65,1	54.72 68.1	9°49 80°95	P02/	Pol	. 9354	9477	· 5596	6186	•	9842	0000 , 0000	.9477 .0000	•		
AIRFOIL AERODYNAMIC SUMMARY PRINT	8=1 8=2 286 887 8	43,76 -6,35	42.66 -6.68	42,27 -7,15	40,45 -7,59	39,00 -7,63	36 36 36 36 59	40.17 -2.73	41.27 -7.55	D-FAC OMEGA-B LOSS-P LOSS-P	TOTAL PROFILE	.0376 .0354	\$0.00, 6660,	0248 ,0220	1110. 8410.	0010, 19100	0173 0130	0351 ,0296	.0403 .0334	•		
IRFOIL AEROL	V0=2	· •	_	1.96. 9.	٠.	7-86-	7 -101.3	19	. 0.9/- 8.	C OMEGA-B L	101	41514	01810		.0533	.0529]	1014	5268 1143	1543	MC 1/A1	LBM/3EC SQFT
	VH-2 VO-1		791,1 689	~	735,1 597	737,3 573	671.1 514	614.0 541	573,0 545	OHEGA-B	SHOCK	.0092	040	0,0000	. 0135 . 4c	.0198	.0133	6510	. 5610.		EFF-AD EFF-P	
	V-2 VH-1	٠.					678,7 682,7 644,7 668.0	619.6 641.8		<u>~</u>	w			•		4	_'		5	~	PO/PO	
S (SPECTAL)	1-7	_	1016.8	976.1	920.5	4.00.7	855.1	839.8	827.6	0	DEGRE	5 10.	æ	4.81 7.78 4	,	5,44 8,40	æ			16.13	#CORR 10/10	
STATOR ANGLES	DIA-1 DIA-2	•		21,589	30 23,314 23,9	25.601	70 27, 818 27, 902 2 29, 408 29 182	29.914	30,382	INCS INCH	30			1.87	2.01		1.29	6.17	80 8 39 8	8 1e*/	NC ORR	

Rotor Pressure Ratio = 1.8662

BASELINE STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

STATO	STATOR ANGLES					AIRFO	IL AER	DYNAMIC	AIRFOIL AERODYNAHIC SUHMARY PRINT	Y PRINT		٠	7	20;28;23	,	JULY 23,197	1,1971
NASA EN	IL ISH	SPECIAL		:	1						NON .	35.5	PEED CI	C00E 10 1001H	OTHT #	PAGE	4.PXGE 36.02
DIA-	1 DIA-2	>	V-2	- 47		1-0^	V0-2	~	8-2	9-1	B - 2		× 2	V -1 - V	02	-1	U-2
	JW	1,335/14	T/SECT	T/SEC #	7	1st 1	125C 01	GREE DE	gree of	GREE DE	CREE	186		13E-1 -1		25.0	
20.4	79 21,489	1052.8	796.0	749.0	793.8	739,8	-59.1	59.55	-4.26	94.81	54,22	789,8	357,7	.250, [-1	101.5	790.0	042.4
10 21,00	78 21,961	1013.3	764.0	737.1	759.3	4.5.4	-63.6	43,33	-6.30	23,72	56,53	005.4"1	377.3	323,7-1	148.9	1-0:610	065.3
- 16 21.5	39 22, 432	969	738,7	706.0	731.7	1,499	-101.3	43,24	7.89	28,46	58,40	804.0	396.6	.383,1-1	189.4	047,2 1	088,1
30 23 3	249.86 61	907	7.08 5	676.6	7007	6114.2	7 101	41.76	- 9 Su	37 89	61.00	857.5-1	445.3	526.7-1	264.1-1	130.9	169.4
7			7.0	4 . 8 4		1 2 4 2	U	7 0 4	7 40	43.88	42 13	9 46	527 9	455.403	151	241.8	256.0
0 67 08					-										7	4 0 4 5	4
2,28	18 27, 702			E 0 / 0 -	962,0	0.556			11.0	16.06		1 1 5 5 0	C 7 1C				
. 2 90 ···	18 29 382	858	643.9	659	637.5	550,4	-,0.1	39,86	+0.e-	53,03	67,18 1	1 4.960	. 0 444	1-0.9/8.	515,3 1	426,5 1	455,2
80 29 P	14 29 856	6 47 9	619	632.3		564.7	-65.4	. 41.77	-6.04	54,50	67,87	0.86	634.0	886,3-1	513,6"	45 F; 0	2.844
96 30 38	82 30.293	837.4	582,5	611.5	579.7	6,695	-57.4	42.90	5.66	55,83	69.21	092.4	633.3	1092 4 1633 3 -903 8-1526 B	526.8 1	473,7 1	469
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* SPAN DEGRE	DEGREE	DEGRÉE L	SEGREE D	EGREE S	ž		1	JTAL PA	!	Pol To	TALTO	TAL ST	ATIC		-		
7	19 5.21	12.14	48.90	55,87	0112	4289	.1735	1640.	.0403	.9272	0000	0000	.6923	9150	6699.	1 0889.	1,1426
10 2.1	96.4	41.6	49.63	53,84	7010	4392	. 1641	0417	.0390	9349	. 0000	0000	7080	878	6249		1589
15 2.	34 5,78	7,02	51.13	52,38	0132	4418 .1246 .0323 .0289	1246	.0323	0289	9540	0000	0000	7681	6377	6210	4955	1,1741
	31 6.13	6.72	50.26	5n 66	7.0	4365	.0651	1810	0133	9784	0000	0000	. 8662	7785	5948	7378 1	- 2134
3 2	71.7	4 4 6	48,30	49.55	0273	4308	.0531	1910	00.00	9829	0000	0000	8788	7659	6012	. 8076	.2763
2	***	9.36	16.70	68.65	1020	4623	10634	0208		9811		0000	8659	7275	-9550	1468	324
	7.95	11.90	47.89	52.06	.0236	5111	1001	0378	0296	9680	0000	0000	1752	,7211	2675	. 9212 1	,3524
8	36 9,72	15,53	47,81	53,80	.02 RB	5341	1245	0440	0338	2496	0000	0000	7628	7078	50 60	1.5606	1354
88	98 ,0.55	18.02	48.55	56.07	•0285	.5749	1647	.059	6840	.9543	0000	0000	.7253	. 6967	44736	1016.	1.3279
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	NCORR W				EFF-AD EFF-P #C	*C1/	1 Y 1										
	INLET 1	INLET IN	THLET IN	IN[ET IN	IN ET IN	ET LBH7SEC	SEC.										
	RPH. LB	LBMZSEG .				165											
	1117. 1	79.80 1.	1.2346 1.8491		81.70 83.20 34.82	,20 37	2										

Rotor Pressure Ratio = 1.9079

BASELINE STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

10 00-10-4-4	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	6802 1.1159 6994 1.1443 6999 1.1620 7236 1.5266 8863 1.3165 9955 1.3143
00000000000000000000000000000000000000	NT 6 0 N M 0 0 M 0 0 0 0 N 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2 4 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3
10.POINT 10.VO=LZ- 77-1076:3 6=1185.6 8=1185.6 1=1245.9 1=1245.9 0=1474.9	
19:17:144 CODE 10:POINT CVO = 1:VO	H - H - H - H - H - H - H - H - H - H -
31.5PEED CODE 10.POINT # 3.PAGE 36-02 1 V*-Z VO'=1 VO'=Z U*-1 U=Z	
UN # 31.5PEED CODE 10.POINT -2 Vr=1 V*2 VO*=1 VPO*=2 -2 Vr=1 V*2 VO*=1 VPO*=2 -13 VPO*=2 VPO*=2 -13 VPO*=2 VPO*=2 -13 VPO*=2 VPO*=2 -13 VPO*=2 VPO*=2 -14 VPO*=2 VPO*=2 -15 VP	174 ST
777	**************************************
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7	924 EFF-P EFF-AD EFF-PP 9248 0000 0000 0000 095 9481 0000 0000 0000 095 9481 0000 0000 0000 095 965 965 965 965 965 965 965 965 965 9
EGREE 1-6-02 1-7-92 1-7-10 1-7	05126 00135 00135 00135 00135 00135
066866 066866 066866 07.02 07.02 07.02 07.02 07.02 07.02 07.02 07.02 07.02 07.02 07.03 07.	PROFILE PROFIL
THEOLIC AERODYNAMIC SUNMARY PRINT RUN # 31,5PEED CODE 10,POINT # 3,PAGE 36.02 VM-Z VOLI VOLLZ B=1 B=2 B*-1 B*-2 V*-1 V*-2 VO*-1 VO*-2 VO*-1 VO*-2 VO*-1 VO*-2 VO*-1 VO*-2 VO*-1 VO*-2 VO*-1 VO*-2 VO*-1 VO*-2 VO*-1 VO*-2 VO*-1 VO*-2 VO*-1 VO*-2 VO*-1 VO*-2 VO*-1 VO*-2 VO*-1 VO*-2 VO*-1 VO*-2 VO*-1 VO*-2 VO*-1 VO*-2 VO*-1 VO*-2 VO*-1 VO*-2 VO*-2 VO*-1 VO*-2 VO*-2 VO*-1 VO*-2 VO	CHEGA-B DFAC ONEGA-B LOSS-P LOSS-P POOL/ EFF-P H-1 H-2 H-1 H-2 H)-1-H-2 SHOCK SHOCK 10119 4366 1907 00450 00420 9248 00000 00000 6961 8765 6678 6802 111159 0113 4530 4176 00452 00423 9248 00000 00000 6961 8765 6678 6802 111159 0113 4530 4176 00452 00423 9279 0000 00000 6961 8765 6678 6809 11620 0126 4486 0727 0026 0030 9481 0000 0000 0000 7795 6368 6057 6809 11620 0127 0028 4486 0727 0027 0028 0000 0000 0000 8669 7274 6579 7942 12469 0128 4667 0643 00212 0135 9809 0000 0000 8669 7274 6551 8863 13105 0134 4667 0643 00212 0135 9809 0000 0000 8669 7274 6551 8863 13105 0134 5575 61261 00447 00326 9638 0000 0000 7783 7532 7526 7076 13197 0134 5575 61261 00447 00326 9638 0000 0000 7783 7532 7526 7076 13197 NLET INLET LBH/SEC 8 5 8 5 4 6 5 3 4 6 6
701L AER 7012 C 0 77 S 1 78 1 88 1 88 1 88 2 1 88 2 1 88 2 1	
AIRO 100 100 100 100 100 100 100 10	8 D-FAC ONEGA-8 9 -436 -1907 3 -4530 -1776 18 -4580 -1410 15 -4467 -0643 7 -5648 -1118 2 -5275 -1261 6 -5789 -1706 1 NLET LBM/SEC 1 5 - 5468 - 1706 8 - 5468 -
2	F F F F F F F F F F F F F F F F F F F
VM-2 7755 714.2 714.3 714.3 714.9 686.0 686.0 680.4 620.4	SHOCK -0119 -4366 -19 -0113 -4530 -17 -0138 -4580 -17 -0138 -4580 -17 -0205 -486 -07 -021 -496 -07 -0234 -667 -06 -0234 -568 -11 -024 -5789 -17 -0346 -5789 -17 -0346 -5789 -17 -0346 -5789 -17 -0346 -5789 -17 -0346 -5789 -17 -0346 -5789 -17 -0346 -5789 -17 -0346 -5789 -17 -0346 -5789 -17 -0346 -5789 -17 -0346 -5789 -17 -0346 -5789 -17
1 1/2 1/12 0/12 1/12 1/12	
747.4 732.4 747.4 732.4 747.4 732.4 747.4 732.4 747.4 732.4 721.8 702.2 661.0	0 C C C C C C C C C C C C C C C C C C C
	12 45 96 1 1 1 1 2 1 2 1 2 1 1 1 1 1 1 1 1 1 1
(SPECIAL) FT/SEC FT/SE	DEGREE DE
N G C C C C C C C C C C C C C C C C C C	NCS - INCH - C
37 ATOR ANGLES 38 ENGLISH 10 1 A 21 1 D 1 A 22 21 0 0 0 0 0 1 1 9 0 1 21 0 0 0 0 0 1 9 0 1 21 0 0 0 0 0 1 9 0 1 23 0 0 1 4 23 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	N M T M M M M M M M M M M M M M M M M M
STATOR ANGLES NASA ENGLISH (SPECIAL SERANIN 10 Z1.008 Z1.7487 1047.4 10 Z1.589 Z2.432 767.5 20 Z3.314 Z3.702 702.2 20 Z5.618 Z7.902 858.4 20 Z5.618 Z7.902 858.4 20 Z5.618 Z7.902 858.4 20 Z5.618 Z7.902 858.4 20 Z5.618 Z7.902 858.4 20 Z5.914 Z7.856 854.0	1NCS - INCH - DEV TURN CAHBER 5 6 2 6 2 5 5 5 8 4 13,75 47 64 55 8 8 10 6 5 1 9 9 42 49 58 53 8 10 6 10 6 1 40 6 8 6 7 9 10 8 8 10 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1
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Rotor Pressure Ratio = 1.9269

Rotor Pressure Ratio = 1,9981

11. 1	ATOR ANGLES ENGLISH SPECIAL IN A V V V V I IN A V V V I IN A V V V I IN A V V V I IN A V V V I IN A V V V I IN A V V V I IN A V V I IN A V V I IN A V I I IN A I I IN A I I IN A I I IN A I I IN A I I IN A I I I I I I I I
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Rotor Pressure Ratio = 2.0123

	STATCH ANGLES	ARGLES					AIR	CIL AER	CHANADO	CSUNNA	RY PRIN	1		,	0:53:29		7117	AIRFCIL AERODYNARIC SURMARY PRINT
×	NASA ENGLISH		(SPECIAL)									# NOW	31,	SPEED C	00E 10+	POINT #	16 . PAG	E 36.02
1	I-KIO	2-813	1-1	Z-A	T-HA	Z-NA	1-04	2-21	1-3	8-2	1-18	28	۸۰-1	72	VC - 1	VO *- 2	-1	U-2
& SPANIN	Z	Z	FI/SEC FT/SEC FT/SEC	FT/SEC	:1/5	FT/SEC 1	TISEC F	TASEC D	EGREE D	EGREE DI	EGREE D	EGREE F	T/SEC F	T/SEC F	T/SEC F'	TASEC FT	IVSEC F	T/SEC
	20 9 9 0 5	21.48	5. 20.409 21.489 1032.3 721.3	72153	8	719.6	759.8	- 50.2	47.40	-3.69	18.07	56.58	731.1	1306.4	-228.0-	1090.3	987.8	1040.1
2	21.008	21.961	21.008 21.961 1000.0 693.2	693 .2	697.9	690.1	716.2	-64.2	45.74	-5.33	23.30	58.52	760.2	1321.8	-300-6-	1127.2	1016.8	1062.9
, \$	21.589	21.589 22.432	1.096	£67.3	599	1 . 662.2	689.0	-61.4	58.55	-7.02	28.02	60.42	755.2	1342.2	-355.9-	1167.2	1044.9	1085.7
8	23,314	23.314 23.902			565.6	E15.4	642.7	-80.7	47.65	-7.47	39.66	63.56	761.0	1362.1	-485.8-	1237.6	1128.4	1155.9
8	Z2:20I	25.893	l	Γ	269.1	636.5	632.0	0.6/-	46.53	-7.08	45.38	64.46	853.0	1476.5	-607-1-	1332.3	1239.1	1253.3
2	27.818	27.818 27.902		€30.3	604•	625.3	613.7	-82.2	45.42	-7.49	50.45	E E . 42	950.1	1563.3	-732.8-	1432.7	1346.4	1350.5
#6 #	29-403	29.408 29.382	-	632.5	605	628.5	644.4	-70.9	46.79	44.9-	52,15	67.17	986.5	1619.9	-778.9-	1493.0	1423.4	1422.1
2	29.914	29.856		62	ŝ	624.6	6.59.9	-58.0	40.46	-5.10	53.43	67.43	581.2	1627.7	-788.0-	1503.0	1447.9	1445.1
\$6 !	30.382	30.293	871.3	608.7	9.	6.53.8	666.8	-58.6	46.64	-5.53	55.10	68,33	980.2	1640.8	-803.8-	1524-8	1470.5	1466.2
						1												
	INCS	E S C E	DEV	LORN	CAMBER	OMEGA-B	D-FAC (MEGA-B	L055-P	LOSS-P	P02/	EFF-P E	FF-AD	EFF-P	H-1	H-2	H1	H 2
SPAN	OEGREE	DEGREE	MERKEE DEGREE DEGREE DEGREE DEGREE	DEGREE	DEGREE	SHCCK		-	OTAL	ROFILE	P01 1	OTAL T	OTAL S	TATIC				•
	5.02	7.94	12,41	51,39	55,87	.0193	.4924	.2159	.0537	6840.	.9126	0000	0000	.6693	!	, 6CO8	.6369	1.0883
2	5 P • 3	7.3	2 10.11	51.07	53.84		.5026	.2181		6330.	.9158	0222	• נינונו	.6644		. 5775	.6571	1,1011
	2.26	8.20	7.88	52,87	52.40	.0229	.5123	.1919	6640	.0439	.9306	.0000	0000	.7015	!	.5552	.6543	1.1168
8	9.14	12.14	7.76	55,12	50.67	.0492	.5176	.0935	.0263	.0123	.9716	0000	0000*	.8460		.5141	•6450	1.1448
S	38.5	12.9	B 6.4	13.13	20.0	.CE 82	. 5124	.1068	. (325	.0117	. 5579	0000	0000	.6117		5285	7176	.7176 1.2155
₽;	9.77	13.01	10.00	55,92	49.92	6 223	.5353	.1437	.0472	.0240	.9580	0000	0000	.7416		.5157	.7953	1.2782
	14.26	9 +	13.45	2.5	52.03	0621	. 5676	.2053	.0713	• 0428	.9384	2022*	0000	.6485		. 5112	. 8175	1.3093
8 i	16.25	16.21	16,33	43.76	53.87	.0917	. 5782	.2111	£747	.0423	.9375	• 6630	0000*	.6414		. 5044	9628.	1,3086
8	16.15	17.53	ነ 16-15 17-53 18-14 55-47 56.07 .0967 .6021 .2256 .ቪታ10 .0463 .9349 .0000 .0000 .6249	55.47	56.07	.0967	,6021	.2256	3310	.0463	.9349	00000	0000	•6243	.7151			8042 3431
	z	NCORK WOORK	CORR	10/10	200/04	L CT - J J	70 0-3	7.57										
	H	INLET INLET	NLET	-	INLET	INLET INLET LBM/SEC	NLET LB	K/SEC										
	!	RPH	RPH LBM/SEC				S											
	=	11093. 1	170.23 1.2583 1.9134	2583 1		78.76 80.60	3,60 31	649										

Rotor Pressure Ratio = 2.0146

W.	AIRFOIL AERODYNAMIC SUMMARY PRINT				JULY 21,1971
(Special)	2 - 4	RUN #25	SPEED CODE JOSPOINT	, ==	4, PAGE 36.02
	7	L	FT/SECT	F	F
89 1046.9 787 1 744.5 787.0 736.0 -56.9	4.14 18.7		1350.8		1040.4
21,008 21,961 1009,4 754,7 733,6 749,0 693,3 -92,0	-7.02	57,05	1377.4	_	
21,589 22,432 968.6 729.0 706,5 721,1 662,5 -107.5	8.48	58,87 804	1395,0	- 10 - 10	7 1096.
23,902 907.0 698,9 677,1 693,7 603,5 -84,9	-6.78	60,63 857	1423.2	.7 112	
25,693 900,9 710,9 685,1 708,4 584,9 -59,8	.4.83	61.67	1492.8	124	٠.
70 -27,818 27,902 852,7 658,8 667,6 653,6 530,9	-7,23	02.20	1576.9	Γ,	2-1321-2
29,408 29,382 852,5 637,7 655,8 637,7 544,7 -51.1	15.5	000	000	PZ-1 6 - 1/-1-	۱
90 27, 714 27, 856 842, 8 612, 7 632, 6 612, 1 556, 7 -30, 4	2,63 5	9	157B.55	PT 0 0 7 1 4	7 011 0
96 30,382 30,293 829,1 566,5 610,2 564,8 561,3 42,6 42,61	61 -4.35 56.17	67.48 1076.1	1012.4 -710.4-1507	71 7.0<1-	1.01
SAMPLE OF THE CAMBER	-p LOSS-p p02/	EFF-P EFF-AD	EFF-P K-1	H-2 H-1	-1 H-2
TO TO THE TAIL OF THE PARTY OF		OTAL TOTAL			
2.31 5.23 12.26 48.80 55.87 .0109 .4309 .1612 .0°			2404. 3917.	0400	.6852 1.1366.
2,09 5,02 8,41 50,40 53,84 ,0106 ,4478 ,1600 ,04		0000. 0000.	.7214	. 6347	-
5.69 6.42 51.63 52.38 .0129 .4525 .1287	0000	0000	. 7677	9219.	_
3,27 6,27 8,24 48,69 50,66 ,0173 ,4406 ,0713	0510	٠	. •	. 1686.	, .
3,82 6,95 11,20 45,32 49,55 ,0262 ,4290 ,0602	2084 . CO10. P810.	0000 0000	•	. 5936	-
2,79 8,03 10,25 45,69 49,90 0191 4654 0496	0010.	· 0000 ·	848 ·····	2945	Ţ.
38 7,72 15,35 44,29 52,05 ,0223 ,4940 ,0745 .	.0182	• 0000•	. 8458	.5268	-
9,41 9,25 18,74 44,18 53,80 ,0259 ,5205 ,0962 ,	.0250	0000 0000	. 8177	• • • • • • • • • • • • • • • • • • • •	ī
8,71 10,28 19,33 46,96 56,07 ,0261	24 .0430 .9602	0000 0000	,7639 ,6902	¥09+	7137 1.311/
10/10					
"INLET "INLET" INLET INLET INLET					
RPM R94/5EC 8 45.56. 25.55. 55.45. 55					
Rotor Pressure Ratio = 1.9063					
	W.	W.	P_/P_	EFF-AD	d d
	GIFFO	BLOW	0		o
	WTOTAL	WTOTAL	Inlet Adj.	Adj.	<u>_</u>
	1	.00513	1.842	82.3	.9693

STATOR ANGLES				«	IRFOIL A	ERODYNAM	IC SUMMA	AIRFOIL AERODYNAMIC SUMMARY PRINT	;			12:08:57		1	1,197
. ?	(SPECIAL)	>	-1 VM-2	1-07					RUN #	_	75; SPEED (V0*-1 V0*-2	V02	7.5	14, PAGE 38. UZ
	1	FT/5	F175	E	FT/SEC		EGREE	DEGREE D	DEGREE FY	T/SECT	TYSEC !		1/SECT	Ι.	
21.489				736	۰.		+ 1 . + -	18.60	54,14	786.0	1353,7	-250.7-1097.2		987.5	1039
21,008 21,961			•	6.9	.3 -92.			23,71	56,85		1379,9	-322,3-		1016.5:1002;	2001
21,589 22,432		~	a	663	.3 -108		8.	28,32	58,68	803.7	1397,3			1044.6 1085.	1085
14 23,902		704.5 677.	1.2 699.3		.2 -85		0.9-	37,72		856,3	1425.5			1128,1	1156.0
25 893		_	_	585	^		4.	43,65			1495.2			1238.8	1252,9
18 27 902	÷	99 .		1	₹.			50,70			_		1434.2-	1346.0-	
29 408 29 382		_	'n		^		4.5	53,30			-		1472.1	1423.0	1421.7
29,914 29,856 6	8.14	_	0	557	-	*		54.68			_		1475.0	1447.5	1 4 4 4 6 7
30,382 30,293 8	28.1	2.9 608		561	.43		*4,35	56,19	92.69	1093.2	1613.6	-808.3-	.3-1508.9	1470.1	1465.8
	1				•										
INCS INCH D	DEV TURN			ø	C OMEGA-		1088-P	/20			EFF.	- I	Y .		¥ .
KSPAN DE GREE DEGREE DE GREE	REE DEGREE	EE DEGREE	E SHOCK	!		TOTAL	PHOFILE	Po1	TOTAL T	TOTALS	STATIC				
5 2.34 9.75	٠,	_	_	c				. 9324	0000	0000	.7096.	P016.	.6694	6649	1.1398
90.0	9.41 50	43 53.8		96 4433	33 . 1624	4 .0412	.0305	9359	0000	0000		8748	- 6396-	2969.	1.1612
2 77 6 73			7					9512	0				.6172	. 6957	1.1746
3.30 6.30	8.23 46	46.72 57.64	99.		52 .0748	8 .0209	0910	9752	0000	0000	9494		5914	7368	1 1966
			L L					0 7 0 5			0 1 4	74.01	9 5 5	. 80.8	1 2497
00.		7		•	:	•	7110	0.00	0000	0000				400	20 T V 1 - 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
2,82 6,09	07.0		2410.	•		00100		1000	מממים.			7 4 4			
70.7	? .	η,	•	•		•		7	0000	0000	000				
·	•	7	. 60 . 0263	1125. 69	0/=:-	\?\D.	.0324	000	0000	0000	20//*	2	э.		
6,63	V 32 4/		• .	•	÷	•	.045	4.274	0000	0000	6+47.	£ 684 3	600.	,	6616
KNOUN WHONK	18 TO/TO	00/00	EFF"AD EFF"P		*C1/A1										
	THEET	INLET	;		LBM/SEC										
RPH LBM/SEC	EC	9 1.8475	9 62.22	83,68	50F1										
_					•										
	,														
Kotor Pressure Katio ==	- 1.9063														
							W	,	W	2	P /P	ļ	EFF-AD	•	Q.
									בֿר מ	2	0	•			0
							WTOTAL		WTOTAL	٩٢	Adj.		Adj.		Local
							ł		.00262		1.843		82.14		.9682

BLOW OPTIMIZATION, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

ונצ.	AIRFOIL AERODYNAMIC SUMHARY PRINT					JULY 21,1971
MASA CNG LISH (SPECIAL)		RON W	25.5PEED C	CODE ICHPOINT		24;PAGE 36:02
30-226-61/266-61/266-61/266-61/266-61/266-61	EE-DEGREE DEGR	DECE	-11/35	175E- F17	SEC- F1756	17.5E
. 489 1045,8 786,2 742,7 784,2 736,2 -56,7	4.14 18	,72 54,44 784	.3 1348.4	-251,7-1096	٠.	9 1040.
1008.2 754.4 731.9 748.6 693.5 -92.1	23	57.05	1376.7		-	Ξ
967,4 729,3 704,7 721,3 662,8 -107,6 43	. 84.8. PS.	58,85	9 1394.6	-382.3-11	_	_
905.9" 699.8" 675.3 "694.6" 603.985.0" 4	37.	60° 16	_	-524.7-1242.0		
899,9 711,7 683,6 709,2 585,3 59,8 4(57 -4.82 43.	3 61,63 946	1492.4	-654,0-13	. 2	3 1253.
7-658,2-666,0-654;0-530,8-82,8-36	-7.22-50.	4 - 65,47-1053	.4-1575,7-	41-8.518	1433.5-1344	41350
851,5. 641,7 654,0 639,6 545,2	53,	3 66,54	1 1606.5	-878,3-1473	73.6 1423	6 1422.3
.841.7 614.9 630.8 614.1 557	5	67,41	. 1598,5	-890.9-1475	.8	7.5441
30,293 827,9 566,8 608,3 565,1 561,6 -42,6 42	72 -4.35 56.	.21 69.46 10 ⁹³ ,	9.1191.6.	-909-1-15	1507.0 1470.	1906
INCH DEV TURN CAMBER ONEGA-B D-FAC ONEGA-B LOSS-P	5-P LOSS-P PO2/	/ EFF-P EFF-AD	0 EFF-P	I.	H-2 H-1	H - 2
DEGREE DEGREE DEGREE SHOCK		TOTAL	TOTAL STATIC			i
55.87 .0111 .4330 .1735	• 0404	0000. 0000. 44	9569. 00		.6614 .6833	
" 8,41 50,48 53,84 ,0108 ,4476 ,1682	.0399	. 0000		:	İ	
6.41 51.73 52.37 .0131 .4518 .1364	.0319	0000	Ī	٠	: •	=
- 8,24 48,78 50,66 ,0176 439Z ,0779		0000		, •	•	-
11.20 45,39 49.55 .0266 .4277 .0666	.0122	•	•	•	-	-
""10.25""45,78 "49,90",0194"",4645"",0572""		32'' • 0000"'' • 0000	i		•	۲
2 15,34 44,40 52,05 ,0227 ,4913 ,0787	. 0195	.2 .0000 .0000	•	•	•	
5 18,74 44,28 53,80 .0264 .5178 .1008	. 4920. 1	0000. 0000. 91	•	٠	5033 . : 913:	3 1,3083
.0266 .5790 .1538	,0553 ,0458 ,958 ₀	0000 0000 08	00 .7496	. 5884.	4612 .91	- 10.1
4 to 4 to 5		•				
ET INLET INLET INLET INLET LBM/SEC						
11884. L946584 1.2330 1.8469" 82.15 83562 39879						
Rotor Pressure Ratio = 1.9063						
	WBLEED	WBLOW	4 °	•	EFF-AD	Po/Po
	WTOTAL	WTOTAL	Inlet Adj.		Adj.	Local
	1	.00263	1.842		82.11	9678
	ì		.00200		1.842	1.842

MASA ENGLISH (SPECIAL DIA-1 DIA-2 V-1 ESPANIN TN FT/SEC						TAILY AND THE ALTERNATION OF THE PARTY OF TH	¥ C C C C C								
FAN IN TN TN 5 20.409 21.489	ار) ۷-2	< H - 1	V H - 2	V0-1	V0~2	8-1	B-2	B • 1	RUN S	2	VISPEED C	CODE 10, POINT VO*-1 VO*-2	0 . POINT # YO * - 2	-34, P.K.GE38+UZ U-1 U-2	3538 + C
	791	7/5EC_FT	28	75EC FT.		DEGREE DE	5 A C. E.	FF .	DEGREETT	1/58C"F	T/SECT	75EC FT/SEC FT/SEC FT/SE	1/5EC #	1	FT75EC-
	-757	734.1	751.5		92.4	43,45	-7.02	23.49		8009	1376.3	-319,0-1152	1152,0		1000
	732	707.0	724.0	'n	107.9	43,22	8 48	28,10				.378.0-	_	ۍ	1083,2
		677.7	648.3		85,5	41.77	9	37, 52	60,61	954	٠.	-520 4-1239		1125.8	1154,2
25,601.25,873	-	\$ 8 Q			-60,2	40,57		43.4	-	2.44.	₹ '			1236.2	125043
70 27 8 8 27 9 2 8 3 8 3 8 5 5 3 8 5 5 5 8 5 3 8 5 5 5 5	3 637.6	655.6	637.0				. 4 . 57	50.52	65 33	1051 2	1574.6	873.9=1430.0	469.7	1343	1418.8
27.914 29.856 843.	B 1 9				30.4		2.83	54.50		1088.7		-886.2-	1472.1	1444.5	1441.7
30,382 30,293 829	9 569	_	1.895	0	-42.9	42.72	4.35	56.01	2	10,00		-1004-	15051	1967.1	1462,8
INCS INCH DEV	JUR X	CAMBER OF		-FAC ON	EGA-B	9-850	L055-p	P02/		FF-A0	EFF-p	-	H-2	H *- 1	H2
EGREE DEGREE DE	DEGREE D	EGREE SH	SHOCK	TOTAL PROFILE	, -	TAL PI	ROFILE	_	TOTAL T		STATIC	1			
5 2,38 5,30 12,26	88.84 91	55,87		4305	1660	.0413	.0385	.9307	0000	.0000	.7075	9116.	.6657	.6841	1,1357
2,15 5,09	1 50.47		0110		1640	•0416	.0388	.9352	0000	0000	.7130	.8763	. 6370	1695F	1,1578
2,82 5,76	2 51,70		.0133	2154.	1324	.0343	.0309	. 9510	0000	0000	.7596	8391	96152	9 6 9 4 5	-
3,33 6,33		•	. 2210.		.0722	0201	.0152	1976	.0000	0000	8569	7803	50.65	.,7351	•••
3,90 7,03		٠.	.0268		.0636	.0194	.0112	. 9794	0000		•	.7695	. 5967	8064	1.2456
6.10 10.		04.44	\$0100		1,50	.0178	4	0.840	• 0000		. 5000	7246	5513	9 4	1,3100
88 7 49 7 83 15 3	•	52,05	0228		* 1 % O *	0318	0239	7.7	0000	0000	9134	7/1/	4475	0,1,0	C D C C
					. 1005	0 7 0 0	4820°	0 6 8 3	0000	0000	75.0	000	82028	¥01.	2602 1
200,41 01.01 10.07	90.4 2	0.00	0500	1//6	/261.	, ,	£0.	7051	0000	• 0000	, 0¢/.				200
NCORR INCET	TO/TO PO	PO'PO EFFA	_ !		S. C.										
RPM LBH/SEC 110670 179.67	1.2330 1.	1.8483 82	82.28 83.74	N.U.											
Rotor Pressure Ratio = 1.9063	563					>	W I		3		9				
						>	WTOTAL		"BLOW WTOTAL		Inlet o		EFF.AD Adj.		Po/Po Local
							ı		.00283		1.843		20 21		2020
)		4.30	•	0000

BLOW OPTIMIZATION, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

Special Var	STATOR ANGLES			AIRFOIL !	ERODYNA	AIRFOIL AERODYNAMIC SUMMARY PRINT	RY PRIN	1		- 1	12:12:36		JULY 21,	1,1971
THOSE CTTYSECTTY SECTTY SECTTY SECTTY SECTT SECTT SECTTY S	LISH (SPECIAL)	- 47		0-1 v0-2	8-1	8-2	81	# ¥ C = 4	1-• 7	5PEED C	7 1 1 1 X	2-40		0-2-0
1 1006.8 757.0 772.6 625.4 625.4 147.1 -4.14 18.75 54.27 725.6 2224.7 17378 1224.1017.7 788.5 1007.5 1107.5	NI	St. C. PT / St. C. PT	F.	SECTT/SE	DEGREE	DEGREET	FGREE-DI	- C R E E - P -	/SEC-FI	ــب	1/SEC-F4		1.5E	1 2 2
1 1000-8 757,0 722,6 751,2 673,9 -22,3 73,75 -67,97 8015,5170-8 9.24,711115,710 2 706,2 713,7 705,4 675,0 677,2 603,4 -22,3 73,75 -69,98 26,97 8015,5170-8 9.24,11115,71115,71115,71115,71115,711,75 -67,97 711,1 705,2 713,7 603,9 713,7 705,4 615,8 96,0 12,5 173,7 603,9 713,7 711,1 565,0 -62,4 173,7 71	21.487	1.9 743.6	789,7 7	36.0 -57,	7.4.	+ - +	18,75	54.27			-252.4-1	047.0	760,5	9.0.01
2 96.9 711.3 70.5 5 723.3 662.6 -107.8 43.20 -8.48 28.80 803.5 1396.3 -3831-1194.3 1045.6 128 976.2 702.4 475.2 -525.6-12.2).11129.2 11129.2 1138.9 10.5 4 43.6 61.5 8 946.7 1325.2 -525.6-12.2).11129.2 1138.9 10.5 4 43.6 61.5 8 946.7 13.6 17.2 13.6 17.2 13.1 12.2 13.1 13.1 13.1 13.1 13.1 13	21.961	•	751.2 6	93.4 92.	J 43.4	2 7.02	23,87.	56.97	'n			1	-5.210	1063:7-
2 861.4 675.7 683.9 677.2 603.6 -85.9 41.7 6 -6.78 37.8 61.58 946.3 1425.2 -552.6-1243.11129.2 111 3 8979.7 713.7 683.9 711.1 895.0 -60.2 40.5 4.8 43.7 61.58 946.7 1949.3 -654.9 1314.7 1912.0 122 2 851.4 640.4 665.1 550.2 -83.2 7.25 50.78 65.45 1004.9 -872.1-1474.9 142.9 122.8 64.60.4 660.4 665.1 50.0 127.1 -1474.9 142.9 122.8 127.0 1004.1 1604.9 -872.1-1474.9 142.9 122.8 121.0 147.0 653.9 640.8 567.8 56.7 -30.4 41.4 5.2 53.7 6.7 1094.1 1604.9 -872.1-1474.9 142.9	. 15 21.589 22.432 967.9 73	'n	•	•	8 43,21	9 - 9 - 0	28.48	58,80	803.5	1396.3	.383.1-1	194.3	9.540	1086.5
3 899.9 713.7 683.8 711.1 585.0 -60.2 40.55 -4.84 43.76 61.58 946.9 1494.3 -654.9-1314.3 1240.0 122 2 851.4 660.4 666.1 655.1 530.3 -83.2 7.25 50.78 65.45 1054.9 -877.7-1473.9 1134.9 134.7 510.6 513.0 65.7 11473.9 1134.9 134.7 510.6 513.0 65.7 11473.9 1134.9 544.7 -50.8 31.2 6.7 65.7 1160.4 1160	23,902	•	i	 -	7.14 - 41.7	86.9 9	37,87.	60.71	856,37	~	-525.6-1	243.1	1129.2	1157,7-
2 851.4 660.4 666.7 655.6 530.3 -83.2 38.52 77.25 50.78 65.45 7054.5 1577.3 -817.1-1434.0 1347.5 77 4.45 51.45 66.70 1076.1 1604.9 87.7 -1475.8 1424.4 14.45 51.5 66.70 1076.1 1604.9 87.7 -1475.8 1424.4 14.45 51.4 14.5 61.5 14.6 10.6 12.8 14.8 14.2 14.1 14.5 14.1 14.1 14.1 14.1 14.1 14.1	25,893	æ	_	٥	2 40,5	7 4.84	43.76	61,58	946.91	۳.	.654.9-1	314.3	240.0	1254.1
2 851.1 637.0 653.9, 634.9 544.750.0 39.774.57 53.37 66.70 1096.1 1604.9879.7-1473.9 1424.9 1146.5 1446.9 1476.5 147	27.9.12		L	-	2 38.5	7.25	-80,78-	F65.4577	054.57	1577.3	-817.1-1	434:0-	1347:37	1351
Beyls 613.6 630.6 612.8 556.7 -30.4 41.45 -2.83 54.75 67.46 1092.6 1598.6 -892.1-1476.5 1448.9 14 BEYNES 569.5 608.0 567.8 561.3 -42.8 42.72 -4.35 56.26 6°.39 1094.7 1613.5 -910.2 1510.0 1471.5 14 DEV TURN CARBER OHEGA-B D-FAC OMEGA-B LOSS-P POZ/ EFF-P EFF-AD EFF-P N-1 M-2 M-1 M-2 M-1 M-2 M-1 M-2 M-1 M-2 M-1 M-2 M-1 M-2 M-2 M-2 M-2 M-2 M-2 M-2 M-2 M-2 M-2	2				8 39.7	4.57	53,37	66.70	096.1	6.4091	879.7-1	473.9	424.4	1423.1
DEV TURN CAMBER OHEGA-B D-FAC ONEGA-B LOSS-P POZ/ EFF-RD FFF-RD FFF-P N-1 H-2 H-1 H DEV TURN CAMBER OHEGA-B D-FAC ONEGA-B LOSS-P POZ/ EFF-RD FFF-RD FFF-P N-1 H-2 H-1 H DECREE DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE SHOCK DEGREE SHOCK DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE SHOCK DEGREE SHOCK DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE SHOCK DEGREE SHOCK DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE DEGREE SHOCK DEGREE	80 27 914 29 856 841.3 61	• •			15	5 -2.83	54,75	67,46 1	092.6"	•	٠.	476.5	448.9	1446.1-
DEV TURN CAMBER OHEGA-B D-FAC ONEGA-B LOSS-P PO2/ EFF-P EFF-AD EFF-P N-1 H-2 H-1 N DEGREE DEGREE SHOCK 12.26 48.85 55.87 0110 4279 1654 10411 0384 9312 0000 7055 9791 6666 6843 14 12.26 48.85 55.87 0110 4453 1655 10420 0393 9349 0000 7005 8735 87091 6666 6843 14 12.26 48.85 55.87 0110 4453 1655 10420 0393 0393 0000 0000 7554 8866 6873 14 12.26 48.85 55.87 0110 74453 1655 10420 0393 0393 0390 0393 0394 122 11.18 45.37 49.80 0175 4364 0273 0316 9503 0000 0000 7534 8866 6873 14 11.18 45.39 49.55 0265 4256 0064 0273 03122 9786 0000 0000 8835 7673 5960 88084 12 11.18 45.39 49.27 53.80 0326 4963 0093 0327 9826 0000 0000 8835 7673 5960 88084 12 11.18 45.39 49.27 53.80 0263 5189 10387 0274 9693 0000 0000 7733 7325 5244 9728 13379 13318 18.74 49.27 53.80 0000 7733 7325 5244 9728 5000 0000 7733 7325 5244 9728 5968 18.74 49.27 53.80 0000 7733 7325 5973 5973 18.74 49.27 53.80 0000 7733 7325 5973 5973 18.74 7255 5973 18.74 7255 5973 18.74 7255 5973 7450 0000 7743 6688 9635 9725 18.74 7255 725 725 725 725 725 725 725 725 72	30.20 B 20.20 B 70.50	40.80	_	•		,	54.24	6 6 7	-	,			47.5	467.2
DEV TURN CAMBER OHEGA-B D-FAC ONEGA-B LOSS-P LOSS-P POZ, EFF-P EFF-AD EFF-P N-1 M-2 M-1 DEGREE DEGREE SHOCK 12.24 48.85 55.87 0110 4279 1654 0411 0384 9312 0000 0000 7055 9091 6666 6843 19 8.41 50,744 53.84 0110 4279 1655 0420 0393 9349 0000 0000 7085 9873 6316 1695 110 18 45.39 49.55 0213 0450 0039 0000 0000 0000 0000 0000 1734 6316 6953 110 18 45.39 49.55 0256 4256 0213 0122 9786 0000 0000 08490 7779 5849 18 18 18 18 18 18 18 18 18 18 18 45.39 49.55 0226 4963 0039 00122 9786 0000 0000 0874 7779 5849 18 18 18 18 18 18 18 18 18 18 18 18 18	20 72 30.2.0 Zar. Or	0.00	į	2	:		07.0c		٦,		7.01			
DEGREE DEGREE SHOCK 12.26 48.85 55.87 0110 4279 1654 0411 0384 9312 0000 7055 9091 6666 6843 18 12.26 48.85 55.87 0110 4453 1655 0411 0384 9312 0000 7005 7085 9731 6458 18 12.26 48.85 55.87 0110 4453 1655 0411 0384 9312 0000 0000 7085 9731 6458 18 12.26 48.85 55.87 0110 4450 1350 0350 0312 9349 0000 0000 7534 8366 6145 6533 18 12.26 48.85 50.86 0175 4364 0256 0316 9503 0000 0000 0000 8490 7779 5895 18 11.18 45.39 49.55 0265 4266 0664 0273 0122 9786 0000 0000 8835 7673 5960 8984 12 110.23 45.77 49.90 0193 4628 0593 6175 00248 9626 0000 0000 8774 7725 5896 8965 77 110.23 45.77 49.90 0193 4628 0593 6175 00248 9693 0000 0000 8774 7725 5896 8965 77 110.23 44.27 53.80 0264 35189 1037 0224 9693 0000 7793 7703 5918 13 110.23 44.27 53.80 0264 5755 1548 0557 00401 9578 0000 7793 7703 5918 13 110.23 49.27 53.80 0264 5755 1548 0557 00401 9578 0000 7793 6688 9635 9725 18 110.23 41.86 56.07 0266 5755 1548 0557 00401 9578 0000 7793 6688 9635 9725 18 110.23 41.86 56.07 0266 5755 1548 0557 00401 8578 0000 0000 7793 6688 9635 18 110.24 45.77 670 670 670 670 670 670 670 670 670 6	DEV		EGA-B D-	FAC OMEGA.	1-5507 B.	4-SS01 4				FF - P		H-2		5-+H
7 12.26 48.85 55.87 .0110 .4279 .1654 .0411 .0384 .9312 .0000 .0000 .7055 .9091 .6666 .6843 1.0 8.41 50.74 53.84 .0107 .4453 .1655 .0420 .0393 .9349 .0000 .7085 .8973 .6368 .6958 1.0 8.43 51.67 52.38 .0107 .4453 .1550 .0350 .0310 .0300 .0000 .7534 .8366 .6953 1.0 8.44 48.74 50.66 .0175 .4364 .0756 .0211 .0162 .9754 .0000 .0000 .8470 .7779 .5845 .7754 1.0 8.24 48.74 50.66 .0175 .4364 .0756 .0211 .0162 .9756 .0000 .0000 .8470 .7779 .5845 .7754 1.0 8.24 48.74 50.66 .0175 .4256 .0213 .0122 .9786 .0000 .0000 .8774 .7779 .5845 .7754 1.0 8.24 48.74 50.66 .0175 .4256 .0241 .0162 .9786 .0000 .0000 .8774 .7725 .5849 .8984 1.2 8.24 48.74 50.60 .0193 .4256 .0241 .0122 .9786 .0000 .0000 .8774 .7725 .5849 .8984 1.2 8.24 48.74 50.76 50.07 .0266 .5755 .1548 .0557 .01461 .7578 .0000 .0000 .7457 .6888 .4635 .9728 .9718 1.2 8.24 48.77 6.668 .4256 .5755 .1548 .0557 .01461 .7578 .0000 .0000 .7457 .6888 .4635 .9712 .9712 .1888	DEGREE		DCK.		TOTAL	PROFILE"		•	:	TAT16				
2.13 5.07 8.41 50,44 53.04 .0107 .4453 .1655 .0420 .0393 .9349 .0000 .7085 .8737 .6388 .6953 1.8 2.72 5.73 6.43 51.67 52.38 .0130 .4500 .0350 .0316 .9503 .0000 .7534 .6366 .6145 .6953 1.8 2.72 6.32 8.24 46.74 6.746 .0132 .0162 .0000 .0000 .01000 .7779 .5441 1.3 2.85 6.07 10.23 45.77 99.70 .0193 .4024 .0203 .0132 .9786 .0000 .0000 .8535 .7779 .5494 1.3 2.85 6.07 10.23 45.77 99.70 .0193 .4628 .0264 .0203 .0132 .9826 .0000 .0000 .8774 .7725 .5496 .8945 1.2 2.85 6.07 10.23 45.77 99.70 .0193 .4628 .0254 .9728 .0000 .0000 .0000 .8774 .7725 .5496 .8945 1.2 2.85 6.07 10.23 49.27 53.80 .0263 .1091 .0387 .0294 .9728 .0000 .0000 .7933 .7152 .5496 .8945 1.2 8.50 9.35 18.74 99.70 .0266 .5755 .1549 .0557 .01461 .7578 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .0000 .0000 .7457 .6688 .4635 .9728 .0000 .0000 .7457 .0000 .7457 .0000 .0000 .7457 .0000 .7457 .0000 .0000 .7457 .0000 .0000 .7457 .0000 .0000 .7457 .0000 .0000 .7457 .0000 .0000 .7457 .0000 .0000 .7457 .0000 .0000 .7457 .0000 .0000 .7457 .0000 .0000 .7457 .0000 .0000 .7457 .0000 .0000 .7457 .0000 .7457 .0000 .0000 .7457 .0000 .7457 .0000 .7457 .0000 .0000 .7457 .0000 .7457 .0000 .0000 .7457 .0000 .7457 .0000 .7457 .0000 .0000 .7457 .0000 .7457 .0000 .0000 .7457 .0000 .7457 .0000 .0000 .7457 .0000 .0000 .7457 .0000 .0000 .7457 .0000 .0000 .7457 .0000 .00000 .7457 .0000 .0000 .7457 .0000 .00000 .7457 .0000 .00000 .7457 .000	7 12.2	_				1 .0384	. 9312	0000	.0000	. 7055	1,00.	9999.	.6843	1.1384
2,79 5,73 6,43 51,67 52,38 ,0130 ,4500 ,1350 ,0316 ,9503 ,0000 ,0000 ,8490 ,779 ,5495 ,734 11 3,32 6,32 8,24 48,74 50,66 ,0175 ,4364 ,0756 ,0211 ,0162 ,9751 ,0000 ,0000 ,8490 ,7779 ,5495 ,734 11 3,68 7,01 11.18 45,39 49,55 ,0265 ,428 ,0264 ,0203 ,0122 ,9726 ,0000 ,0000 ,873 ,5725 ,8084 11.2 2,85 6,07 10,23 445,77 49,70 ,0193 ,4628 ,0132 ,9264 ,0000 ,0000 ,8733 ,7725 ,5490 ,8725 2,46 7,01 15,36 44,36 52,05 ,0226 ,4763 ,0738 ,4177 ,0284 ,9728 ,0000 ,0000 ,7733 ,7225 ,5494 ,9721 8,50 9,35 18,74 44,27 53,80 ,0263 ,5189 ,0034 ,978 ,0000 ,0000 ,7733 ,7132 ,5122 ,9139 13 8,62 10,39 17,34 47,27 53,80 ,0264 ,5755 ,1548 ,0557 ,0461 ,9578 ,0000 ,0000 ,7733 ,7722 ,5122 ,9139 13 8,62 10,39 17,30 56,07 ,0266 ,5755 ,1548 ,0557 ,0461 ,9578 ,0000 ,0000 ,7733 ,7732 ,5122 ,9125 13 8,62 10,39 17,28 12,10 8,63 1,023 47,06 56,07 ,0266 ,5755 ,1548 ,0557 ,0461 ,9578 ,0000 ,0000 ,7733 ,7732 ,5122 ,9125 13 8,62 10,39 17,06 56,07 ,0266 ,5755 ,1548 ,0557 ,0461 ,9578 ,0000 ,0000 ,7733 ,7732 ,5122 ,9125 13 8,74 1,0878 10,10 8,74 1,0878	5.07 8.41	53,84	!	•	.042		4344	0000	0000	.7085	. 6737	- 8969.	. 6959	- 6651 .
3.32 6.32 8.24 46.74 50.66 .0175 .4364 .0756 .0211 .0162 .9751 .0000 .0000 .8490 .7779 .5495 .7364 11.1 3.88 7.01 11.18 45.39 49.55 .0265 .4256 .0664 .0203 .0122 .9786 .0000 .0000 .8535 .7673 .5960 .8084 1.2 2.85 6.07 10.23 45.77 49.70 .0193 .4628 .0263 .0132 .9826 .0000 .0000 .8774 .7225 .5496 .8965-1.2 2.85 6.07 10.23 45.77 49.70 .0193 .4628 .0263 .0248 .9728 .0000 .0000 .8774 .7225 .5496 .8965-1.2 2.85 6.07 10.30 18.34 44.27 53.80 .0263 .5189 .0294 .9693 .0000 .0000 .7933 .7032 .5242 .9728 1.3 2.50 7.35 18.74 44.27 53.80 .0264 .5755 .1548 .0557 .0461 .9578 .0000 .0000 .7933 .7032 .5422 .97139 1.3 2.60 8.35 18.74 44.27 53.80 .0264 .5755 .1548 .0557 .0461 .9578 .0000 .0000 .7933 .7032 .5022 .97139 1.3 2.60 8.35 18.74 44.27 53.80 .0264 .5755 .1548 .0557 .0461 .9578 .0000 .0000 .7459 .6688 .4635 .97125 1.3 2.60 8.35 18.74 44.27 53.80 .0264 .5755 .1548 .0557 .0461 .9578 .0000 .0000 .7459 .6688 .4635 .97125 1.3 2.60 8.35 18.74 44.27 53.80 .0000 .0000 .7459 .6688 .4635 .97125 1.3 2.60 8.35 18.74 87.04 87.04 87.06 .0000 .7459 .6688 .4635 .97125 1.3 2.60 8.35 18.74 87.04 87.05 87.04 87.0	•••		•		•		.9503	0000	0000	.7534	9366	.6145	.6953	1,1734
3,88 7.01 11.18 45,39 49.55 .0265 .4256 .0064 .0203 .0122 .9786 .0000 .0000 .8535 .7673 .5960 .8084 2,85 6.07 10.23 45,77 49,70 .0193 .4628 .0593 .0192 .9626 .0000 .0000 .8774 .7225 .5496 .8965 7,46 7,61 15.36 44,36 52.05 .0226 .4953 .0736 .0127 .0248 .9728 .0000 .0000 .8073 .7152 .5544 .9738 8,62 10.39 19.33 47.06 56.07 .0266 .5755 .1548 .0557 .01461 .9578 .0000 .0000 .7459 .6888 .4635 .9125 8,62 10.39 19.33 47.06 56.07 .0266 .5755 .1548 .0557 .01461 .9578 .0000 .0000 .7459 .6888 .4635 .9125 8,62 10.37 17.07 0.070 EFF-AD EFF-P HC1/A1 8,62 10.46 1.9578 .0000 .0000 .7459 .6888 .4635 .9125 8,62 10.46 1.9578 .0000 .0000 .7459 .6888 .4635 .9125 8,62 10.46 1.9578 .0000 .0000 .7459 .6888 .4635 .9125 8,62 10.46 1.9578 .0000 .0000 .7459 .6888 .4635 .9125 8,64 10.47	i		;	;	-		9751	. 0000	. 0000	0448	. 4777	.5895°	.7364	-1961-1
2,85 6,07 10,23 45,77 49,70 .0193 4628 .0593 .0132 .9826 .0000 .0000 .8774 .7225 .5496 .89655 .746 7,61 15,36 44,36 52.05 .0226 .4963 .0738 .0138 .9728 .0000 .0000 .8073 .7152 .5544 .9218 17,46 7,61 15,36 44,37 53.80 .0264 .9728 .0000 .0000 .0000 .7933 .7032 .5042 .9718 .8682 10,37 17,37 47,06 56,07 .0266 .5755 .1548 .0557 .0491 .7578 .0000 .0000 .7457 .6888 .4635 .9125 .1878 .0000 .0000 .7457 .6888 .4635 .9125 .1878 .1878 .1878 .1878 .1878 .1878 .0000 .0000 .7457 .6888 .4635 .9125 .1878 .8788 .8788 .8788 .8888	3,68 7		•		•	_	.9786	0000	0000	. 8535	7673	0965	. 8084 I	2480
7,46 7,61 15.36 44,36 52.05 .0226 .4963 .0738 .0127 .0248 .9728 .0000 .0000 .0073 .7152 .5244 .9218 1. 9,50 9,35 18,74 44,27 53,80 .0263 .5189 .1071 .0387 .0294 .9673 .0000 .7733 .7032 .5022 .9739 1. 8,62 10.39 17,33 47,06 56,07 .0266 .5755 .1548 .0557 .01461 .9578 .0000 .0000 .7459 .6688 .4635 .9725 1. NCORR WCORR TO/TO PO/PO EFF-AD EFF-P MCI/A1 INLET	Ĩ	;	į.	į	ì	,	. 9826	0000	0000	8774	7225	-2449	-8968	-3126-
9.50 9.35 18.74 44.27 53.80 .0263 .5189 .1091 .0387 .0294 .9693 .0000 .7933 .7032 .5022 .9139 13. 8.82 10.39 1°.33 47.06 56.07 .0266 .5755 .1548 .0557 .0461 .9578 .0000 .7459 .6688 .4635 .9125 13. NCORR MCORR TO/TO PO/PO EFF-AD EFF-P MCI/A1 INLET	^		•	•	-		.9728	0000	0000	. 6093	241,	.5244	.9218	,3213
D.39 19,33 47,06 56,07 ,0266 ,5755 ,1548 ,0557 ,0461 ,9578 ,0000 ,0000 ,7459 ,6888 ,4635 ,9125 1. R MCOKR TO/TO PO/PO EFF-AD EFF-P WC1/A1 T IN ET IN ET IN ET IN ET IN ET LBH/SEC LBH/SEC LBH/SEC S SOFT	9 9.50 9.35 18.74 44		•	-	•		.9693	0000	0000	.7933	,7032	- 5055	6616	. 3082
R SCORR TO/TO PO/PO EFF-AD EFF-P T INLET INLET INLET INLET LBM/SEC	2 10.39 19.33 4	20.03	•	-	•		9578	0000	0000	.7459	6888	4635	\$716	3129
T IN ET IN ET IN ET IN ET IN ET IN ET IN ET			1 4 4			i : : : i		!	1	!	:			
LON/SEC INC. INC. INC.	A CONTRACTOR	1	A 0 0 0											
TOS NO STATE STATE OF	I JAI I	INFE												
	LBK/SEC	40		204										

Rotor Pressure Ratio = 1.9063

Po/Po Local	6296.
EFF-AD Adj.	82.10
P _o /P _o Inlet Adj.	1.842
WBLOW WTOTAL	.00249
W _{BLEED} W _{TOTAL}	I

12:13:55	NO	13534 7253-511098-5 989-0 1041-4	1400.1 -384.0-1,195.7 1046.2 1087.1	1428 6 =526.5=1244.3 1129.8 1158.3	نہ د	1604.6 -881,3-1474,4 1425,1 1423,8	1598,9 ~893,6-1477,2 1449,6 1446,8	EFF-P H-1 H-2 H-1 H*-2		. 1299° +016	.675264076980	8379 .6172	,7793 :5937 7388	,7664 .6011 .8107 1	8839,7235,553 0,8992-1,3156 -7910 ,7159 ,5229 ,9240 1,3208	7040 \$015 0407	7317 ,6897 ,4617 ,9144 1,3128		
	B - 2 V - 1 GREE - FT / SEP-F	54.26 787.7	805.7	7.858 75.09	0.177 27.10	^.	67.50 1094.9	EFF+P EFF-AD	TAL TOTAL S	0000* 0000*	.0000* 0000*	, 9526 ,0000 ,0000 ,7626 ,	0000 0000	0000 0000	.0000 .0000		0000 0000		
AIRFOIL AERODYNAHIC SUMMARY PRINT	1-2 B'-1 SREE-DEGREE-DE	7.03 23.87	28,46	37,82	7.28 50.74	-4,55 53,34	-2,83 54,71 -4,38 56,21	355-p p02/ E	FILE POI TO	0390 ,9302	.0382 ,9365	.0300 ,9526	0146 9510	,0097 ,9812	0280 9703		1554 84+0		
AERODYNAHIC	1-2 B-1 B	157 - 2 44 - 6 1 4 1 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	43.09	59 1 62	**************************************	0.5 39,66	-30,4 41,32 -	OMEGA-B D-FAC OMEGA-B LOSS-P LOSS-P	TOTAL PRO	91,00	4040	.0333	.0193	.0177	i	.0413	1644 .0591	įų	:_
AIRFOIL	V0-1 V0	735.5	662.2	603	9,625		556.1	-B D-FAC OMEC		. 4278	. 4418	4455	4322	4204	4984	.5202	5786	FF-AD EFF-P WC1/A1	8 50FT 82.32 83.77 34.89
	VH-1 VH-2	745.6 790.4	707.7 728.	7,0	-668.2658	656.0 633.2	632.6 612.0	CAMBER OMEGA-	SEGREE SHOCK	55,87 ,0108	53,84 .010	52,37 ,012	20. 66 . 017		52.06 .0220		56.07 .0260	"	
	(SPECIAL) V-1 V-2 FT/SEC FT/SEC F	1047-4 792-5	969.2 736.4	907.7.707.1		852.1 635.2	842.3 612.8 828.7 567.4	TORN	DEGREE DEGREE D	12,26 48,75	8,41 50,34	6.42 51,57	8,24 48,63	11,17 45,30	-10.19 45.68 - 15.38 44.21	18.73 44.15	19,30 46,99	T0/10 INCET	. 180.131.2329'1.8486
	-1 DIA-2	5 20.409 21.489	1,589 22,432	3,314 23,902	7 818 27 902	9,408 29,382	9.914 29.856	INCS INCH	SSPAN DEGREE DEGREE DE	2,25 5,17	2.02 4.95	2.69 5.63	3,21 6,21	3.77 6.91	7.40 7.72	9.42 9.26	8,70 10,29	~ -	11106. 18C
ST	NASA E	200		N	2 2	1 88 2	8 8 1	1	SSPAN DE	 	2	91	; 8	\$	2 2	8	8		

Rotor Pressure Ratio = 1.9063

BLOW ONLY, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

STATOR	STATOR ANGLES					AIRF	DIL AER	DANADO	CSURBA	AIRFOIL AERODYNAMIC SUHHARY PRINT			7	ZZ;Z6;34 49:-corre	- N - C - C - C - C - C - C - C - C - C	JULY 2 	JULY 20,1971
DIAT DIAT STEELING	DIA-1 DIA-2			1 - E >	VH-2	V 0-1	V0-2	9-1	8-2		8 - 2	7-1-2	V 1-2	1-,01	V02	1-1	0-2
& SPAN IN	F	t		T7SECT	T/SEC F	175EC F	173EC D	DEGREET	DEGREE DEGRE	EGREE	EGREE	17SEC-1	1.35.	TYSEC-F	1/5EC	1456	17556
20,40	£ 20.409 21.489	852,7	862.2	682.8	861.4	510.7	-37.9	36.79	-2,52	14.70	41.58	706.0	706.0 1151.5	-179.1	-164.2	8 4 4 9	7.26.3
10, 21,00	21,008 21,961	816.5	828.3	-4.999	825.7	471.8	h . h 9 -	. 35.29	. Lh . h	19.68	44,33	-10804-	1154.5238.	7	-1006-7	710.1-	742.3
T 15 21,589	9 22,432	782,5	8008	1.649	796.9	436.9	-79.0	33.92	.5.68	24.25	46.41	713.0	1156,1	8	-83/.2	729.7	758,2
20-23,319	23,902	716.6	736.0 624.	-0.429-	730.4	352.1		- 29,43	- 90 . 2-	34.92	50,88			_	-698°3	-788.0-	- 601:4
_	1 25,893	670.8	681.0	607.4	674.2	284.6	7.5.7	25,10	80.8-	43.70	55,22	840.5	1182.2	-580.7	-470.9	865,3	875.2
70-27,81	7.818 27 902	636;7	627.5	292:0	620.0	234.2	5.96-	-21,58-	-8.85	-20:05-	59:19	-92126-	1210;5"	12103570631-1039	1039-6-	2.046	1000
- 85 29,408	8 29,382	624.1		580.7	579.5	228.6	68.	21,50	-8,72	52,82	61,82	9.096	1227,5	-765,4-1082,0	1082.0	0 + 6 6	993.1
90.29.914		. 848.	566.7	551.3	560.4	233,6	-84.3	22,98	-8.55	54,67	62,86		1228,7	-777.5-1093,	1093,4"	1011.1	10001
88 30,382	2 30,293	570.3	520,3	519.1	511.8	236,1	-93.7	24.47	-10.40	56.72	65,39			-790.8-1117.6	1117.6	1026.9	1023.9
INCS	I NCH	DEV	TURN		OHEGA-B D-FAC OHEGA-B LOSS-P LOSS-P	D-FAC OF	4EGA-B	L055-P	1.055-P	P02/	EFF-P EFF-AD EFF-P	. F-A0	1		H-2		2-,H
* SPANDE GREE	DEGREE	SEGREE DI	EGREE D		SHOCK	1.	F	OTAL "P	PROFILE	F 104	POI "TOTAL TOTAL" STATIC	JTAE S	ratic				
5 -5,51 -2,59 13,88 39,31 55,8	1 -2.59	13.88	39,31	55,87	0000	.1457	.0741	.0185	.0185	.9762	0000	0000	3.6295	,7626	.7744	.6328	1.0343.
	1 .3.1A	10.96	30.76	53,84		1506	9990	0,10	0110	. 9801	. 0000		2,1715	7244	. 7430	-, 6335	1.0357-
59.9.	5 -3.71	9.35	39,59	52,53	0000	1469		.0120	01120	.9872	.0000	0000	1.5234	9469	.7177	.6390	1.0360
30 9 . 22	1	8 . 16	36,49	- 50.67	0000	. 1450	.0338	. 4600*	# 600°	. 6166.			1.3000	6363-	. 6586	. 6846	1:0362
86 -11.73	3 -8.59	7.95	33,19	49.59	.0000	,1579	.0403	.0122	.0122	. 9913	0000	0000	0817.1	1965.	• 6086	.7545	1.0565
20 = 14,2	-14.23 -10.99	09.8	30,43	_49.87	0000	1863	.0583		_1610*	. 9885	0000	-0000	- 690°I	5671	S 6 D O	8273-	1:0802
. 10.8	8 -10.42	11,25	30,21	52,11	0000	,2383	.0967	.0334	.0334	. 9817	0000	0000	.2555	6155	.5204	. 8543	1,0873
P 9 8 - 08	4 -9.07	12.92	31,53	53,70	0000	. 2423	.0546	-0192	.0192	*066	. 0000	0000	. 5094	5283	- 4105	. 9446	1,0870-
		13,28	34,87	26.07	.0000	. 2964	5460.	.0335	.0335	. 9849	0000	0000	44199	,5022	4582	. 8359	1,0825
	COVER TOTAL GOODS	10,	04,	i i	Erran Erran	71							‡ 				
	TNET THET		THE ET THE ET	1	T L	ET TBR7SEE	SEC										
·	RPH LBM	LBH/SEC	1		, ,	506											
7.7	7746. 13	134.86 1.0842 1.2585	3842		80.68 81.27	,29 36,	9,										

Rotor Pressure Ratio = 1,2720

P_o/P_o Local

EFF-AD Adj.

P_o/P_o Intet Adj.

WBLOW WTOTAL

WBLEED WTOTAL .9846

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5		4-04-04												-	***・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・	•	
	S	PECIAL		<u> </u>							RUN	8	ĭ	005-101	k - (¥ 4.1 + 1.1	TO BOE COM
-	D14-2	-	2-7	ν. Η - Ι	VH-2	-0^	40-2	1	B-2		82	-	. 1	- O - I	7-107	-	2-0
N S S S S S S S S S S S S S S S S S S S	2	7.25.0.7	7/550 7	T/SEC F	1/SEC #	1/3EC F	1/550		DEGKEE D	EGREE U	7 7 7 7 7 2 2 4 7 9 4 7	1/250 4	1/250 -	1 7 2 5 7 1	7356 7	A 8 8 8 9 9	726.
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21,008	21,961			583.6	662.2	486.3	T 8 5	39,80	12.4-	ZD. 78	50.04	. 6.25	1031,7	-223.7		0.01	2.2.7
21,589	22,432	725.0	637.7	562.9	634.3	457.0	6.69-	39.06	-5.85	25,84	52.38	626.3	1034.3	-272.7	-623.0	129.6	758.1
	23.902	656.1	~	521.3	-586-	398.3	-4119-	-37,37	-6.01	.36,75	-10.45-	.0.159_	1048.7	-389.7	-869.5-	187.4	- 80%
	25.893	620.1	544	515,1	545.4	345.4	6.99-	33,84	66.95	45,25	59.92	731.9	1088.6	-519.9	-942.0	865.2	875.1
70 -27 RIB 37 9h2	17-9h9-	209:7	K18.7	C.O.B.	4 1 1 0	1,717	270.3	86-15	27.78	51.73	63.10	814:1	113671	-622-6-1013-2	1013-2	-940-2	10:00
86 29 408	78. 04	597.6	4.99.6	40.0	6 Y 6 T	9	12.7	33.61	5.97	53.11		829.1	1157.2	-663.1-1045.0	1045.0	993.9	993.0
29.95	20 BSA:			477.7	- Y 4 4		-	- 55 51				822.8	1157.3	-670.2-1050-1	1050.1	1011.0	- 0.6001
	30.293		462.8	459.2	460.1	344	6.8	36,87	90.9	56.07	66.78	822.7	1167.3	-602.5-1072.7	1072.7	1026.8	1023.8
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MSPANDEGREE DEGREE DEGREE DEGREE	GREE	ECREE. DI	EGREE	,	SHOCK		F	TOTAL	PROF ILE	P01	TOTAL" TOTAL ""STATI	OTALS	TATIC				
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10 01		. 11,22"	10.44	53,84	00000	3022	. 1148	.0293		8696	0000	0000		6688	5835	5547-	. 9063
16 -1.35		9.18	44.91	52.54	0000	3062	.0931	.0243	.0243	. 9774	.0000	0000	.6603	4939	5596	.5548	9121
;	- 85	9.21	43,39	50.67		2968	0244	. 0068	8900	.0566	0000	0000	906	. 5768	. 5163	.5772	9 1 8 8 ·
80 - 2.88	20	40.4	40.83	49.58		3167	.0292	6000	9900	9466	0000	0000	.8821	5451	4809	.6472	9526
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10.0	4.53	17,59	42,95	56.06	0000	- - -	.0612	.0220	.0220	+066°	0000	0000	.8363	9865.	.3770	•7154	1.0064
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17.	١,	3.71	1026 1.	123.71 1-1026 1-3351 83.9	3.91 84.56	ţ	32.06										
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									TOTAL		"TOTAL	7	Adi:		į		3

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BLOW ONLY, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

Special 1	MASA ENGLISH	411.5 418.6 418.6 418.6 441.5 441.5 441.5 441.5	10000	V CO C C C C C C C C C C C C C C C C C C	8-1 EGREE DEGREE 43.73	1-0		2 -	EDCODE 70,1 -2	- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	15 PAGE	20.00
7. 655.5 538.3 1.4 43.73 1.2 15.11 47.9 6 53.0 77.5 6 725.7 720.5 770.5	6B 1N 1N 1N 1N 1N 1N 1N 1N 1N 1N 1N 1N 1N	445 S S S S S S S S S S S S S S S S S S	10000	0 + 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EGREE DEGREE	1						
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0 502, 3 441, 0 42, 14 - 5,86 20,56 51,91 593,2 995,9 - 208,2 - 703,7 7,10,5 6 586,3 474,4 556,9 91,24 - 556,9 91,28 592,8 1004,7 - 255,7 7,0 1 7 9	10 21,008 21,961 748,6 23,314 23,902 645,4 25,601 25,893 602,6 26,408 29,382 597,5 10 29,914 29,856 597,5 10 29,914 29,856 597,5 10 29,914 29,856 597,5 10 29,914 29,856 597,5 10 29,914 29,856 597,5 10 29,914 29,856 597,5 10 29,914 29,856 597,5 10 29,914 29,856 597,5 10 29,914 29,856 597,5 10 29,914 29,856 597,5 10 29,914 29,856 597,5 10 29,914 29,856 597,5 10 29,914 29,856 597,5 10 20 20 20 20 20 20 20 20 20 20 20 20 20	108 CA	000	2=000-			47.90 5			-725.3	690.2	726,8
6 586.3 474.4 4 56.9 41.63 5.55 25.59 54.28 592.8 1004.7 255.7 2815.5 730.1 7 6 533.9 417.0 54.7 40.24 5.85 36.9 68.25 617.2 1014.9 5.71.5 -863.0 788.5 6 7 471.9 361.1 -37.4 39.66 4.5 53.15 65.41 766.6 1131.9 -613.5 -1031.1 994.6 7 7 471.9 381.1 -37.4 39.66 4.4.5 53.15 65.41 766.6 1133.9 -613.5 -1031.1 994.6 7 7 471.9 381.1 -37.4 39.66 4.4.5 53.15 65.41 766.6 1133.9 -613.5 -1031.1 994.6 7 7 471.9 381.1 -37.4 39.66 4.4.5 53.15 65.41 766.6 1133.9 -613.5 -1031.1 994.6 7 7 471.9 381.1 -37.4 39.66 4.4.5 53.15 65.41 766.6 1133.9 -613.5 -1031.1 994.6 7 7 471.9 381.1 -37.4 39.66 4.4.5 53.15 65.41 766.6 1133.9 -613.5 -1031.1 994.6 7 7 471.9 381.1 -37.4 37.66 4.4.5 53.15 65.4 647.2 -1069.7 1027.5 11027.	16 21,589 22,432 714,1 10 23,314 23,902 645,4 10 25,818 27,802 596,5 18 29,408 27,882 597,5 18 29,818 27,82 597,5 10 29,914 29,856 587,0 10 29,914 29,917 9,45 10 30 11,27 4,30 16,52 10 30 11,29 4,13 9,917	100 CA	9 - 77 - 9	7000 -	3.C L.ZF.	:	51,91.5	193.299	5.9208.2	-783.7-	710.5	742,7
6 533,9 417,0 -54,7 40,24 -5,85 36,99 56,25 617,2 1014,9 -371,5 -863,0 788,5 8 1 494,6 371,0 -62,8 37,99 -7,23 46,15 62,21 100,9 -494,8 -494,8 -938,5 865,8 8 471,9 34,7 10 -62,7 37,00 -7,45 50,68 64,52 752,0 1114,8 -581,6 -1006,4 940,6 9 471,9 381,1 -37,4 37,6 -4,5 53,5 53,15 64,17 7,17 19 381,1 -37,4 37,6 -4,5 53,5 53,15 64,17 7,17 19 381,1 -37,4 37,6 -4,5 53,17 114,3 -625,6 -1006,4 1011,7 101,4 461,2 384,9 -36,9 40,8 -4,5 8 54,7 4 -66,22 767,7 1141,8 -625,8 -10046,6 1011,7 101,4 10,6 10,2 385,3 -45,2 41,7 6 -5,89 56,10 67,7 1141,8 -625,8 -10046,6 1011,7 102,5 10,6 10,6 10,6 10,6 10,6 10,6 10,6 10,6	10 23,314 23,902 645,4 10 25,601 25,893 602,8 10 27,818 27,825,557,0 10 27,814 29,856 597,0 10 29,914 29,856 587,0 10 29,914 29,856 587,0 10 29,914 29,856 587,0 10 29,914 29,856 587,0 10 29,914 29,917 9,49	4000 5 400 5 400 5 400 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	9-17-0	000-	41.63 -5.5	'n		92.8 100		s.	730.1	758.7
1 494.6 371.0 -62.8 37.99 -7.23 46.15 62.21 686.1 1060.9 -494.8 -736.5 865.8 8 47.15 47.15 31.0 -62.7 37.500 -7.45 50.68 64.52 752.0 7114.8 -581.6 -1006.4 940.8 -745.5 14.15 17.1 17.1 17.1 17.1 17.1 17.1 17.1 1	10 25.601 25.893 602.8 10 27.818 27.902 596.5 10 29.919 29.856 597.0 10 30.382 30.293 576.6 10 30.382 30.293 578.6 10 10 10 10 10 10 10 10 10 10 10 10 10 1	1473.4 4473.4 441.5 1URN CAI		00-			. 58,25. 6	17,2-101	•	-863.0	3 88 2-	. 8 G B . 4.
1 479.4 359.0 -62.7 37.00 -7.45 50.68 64.52 752.0 1114.8 -581.6-1006.4 940.8 771.8 381.1 -37.4 39.66 -4.53 53.15 65.41 76.6 1133.9 -6.13.5-1003.1 994.6 9 7471.8 381.1 -37.4 39.66 -4.53 53.15 65.41 76.6 1133.9 -6.13.5-1004.5 1010.1 994.6 9 7471.8 115.2 384.9 -6.25.9 -6.25.7 71143.8 -6.25.9 -6.100.6 7.7 71143.8 -6.25.9 -6.100.6 7.7 71143.8 -6.25.9 -6	10 27,818 27,902 596,5 18 29,908 29,382 597,2 10 29,914 29,856 587,0 10 29,914 29,856 587,0 10 38,317 11,58 10 83 3,77 11,58 10 1,23 4,17 9,49 10 1,23 4,17 9,49	44730.44 44730.44 4411.55 4411.55 4411.55 4411.55 4411.55	476.3 479.4 459.7 471.9 443.1 461.2 431.6 439.2	0-	7	•	_	_		s,	865,8	875.7
7 471 9 381 1 -37 4 39 66 -4 53 53 15 65 41 766 6 1131 9 -613,51031 1 994,6 9 1 461,2 384,9 -36,9 40,98 -4,58 54,74 -66,22 767,7 1143,8 -626,8-1046,6 1011,7-104 6 439,2 385,3 -45,2 41,76 -5,89 56,10 67,68 773,8 1156,4 -642,2-1069,7 1027,5 10 6 439,2 385,3 -45,2 41,76 -5,89 56,10 67,68 773,8 1156,4 -642,2-1069,7 1027,5 10 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	10 29 408 29 382 597.2 10 29 919 29 856 587.0 10 30 382 30.293 578.6 10 10 29 40.17 9 49 10 10 10 10 10 10 10 10 10 10 10 10 10 1	441.05 441.05 1088 1088 1088 1088	459.7 471.9 443.1 461.2 431.6 439.2	·	37.00.72	.89.05.51	69:52		4.8581.8-	-6.900	-9.01.6-	43.7
1 461.2 384,9 -36.9 40.98 -4.58 54,74 - 66.22 767.7 1141,8 -626.8-1046,6 1011,7 -10. 6 419.2 385.3 -45.2 41.76 -5.89 56.10 67.68 773.8 1156.4 -642.2-1069.7 1027.5 10. ONEGA-B D-FAC OMEGA-B LOSS-P LOSS-P PO2/ EFF-AD EFF-AD EFF-P H-1 H-2 H-1 H SHOCK -0003 .3257 .0960 .0244 .9733 .0000 .0000 .7263 .6878 .5728 .5168 . 00002 .3597 .1254 .0320 .0319 .9680 .0000 .0000 .7263 .6876 .573 .5243 . 00002 .3597 .1254 .0320 .0319 .9680 .0000 .0000 .7263 .6875 .5373 .5243 . 00003 .3257 .0960 .0272 .0271 .9755 .0000 .0000 .7255 .6275 .5136 .5232 . 00003 .3257 .0969 .0082 .0077 .9953 .0000 .0000 .9195 .5280 .4330 .6621 . 00003 .3257 .0694 .0210 .0132 .9913 .0000 .0000 .8731 .5184 .4067 .6655 . 00000 .4825 .0420 .0149 .0120 .9932 .0000 .0000 .8731 .5184 .4067 .6655 . 00000 .4826 .0522 .0189 .0120 .9913 .0000 .0000 .8731 .5184 .4067 .6655 . 00000 .4826 .0650 .3778 .6655 . 00000 .0000 .8731 .5184 .4067 .	10 29,914 29,856 587,0 18 30,382 30,293 578,6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1441.5 1441.5 108N CAI	43,1-461,2		39.66 -4.5	13 53,15	65.41 7	66.6 113	3.9 -613.5-	-1031.1	9.466	443.7
6 439,2 385,3 -45,2 41,76 -5,89 56,10 67,68 773,8 1156,4 -642,2-1069,7 1027,5 10 OHEGA-B D-FAC OHEGA-B LOSS-P PO2/ EFF-P EFF-AD EFF-P H-1 H-2 H'-1 H SHOCK ODO3 3257 O980 OB14 O214 ODO3	18 30,382 30,293 578.6 18CS 18CF DECREE 10 10 10 10 10 10 10 10 10 10 10 10 10 1	TURN CAP	431.6 439.2	384 9 : -36 9 -	- 40° 98 4° 5	- 64,74-	66,22-7	411. 7.79	3.8 -626.8-	-1046,6	1011,7-1	.600
ONEGA-B D-FAC OHEGA-B LOSS-P LOSS-P PO2/ EFF-P EFF-AD EFF-P H-1 H-2 H-1 H SHOCK	INCS INCH DEV IN DEGREE DEGREE DEGREE 1.37 4.30 16.52 10 .83 3.77 11.58 15 1.23 4.17 9.49 20 1.79 4.78 9.39 50 1.30 4.43 8.80	TURN CAP DEGREE DEG		. ~	41,76 -5.8		67,68 7	73.8 115		-1069.7	1027.5	024.5
SHOCK	M DEGREE DEGREE DEGREE 10.52 10.552 1	DEGREE"DEC		-FAC OMEGA-B L	-SS07 d-SS0.	1004	del deldi	-AD EFF	i !	H-2	7	H *-2
7 .0003 .3257 .0960 .0244 .0733 .0000 .0000 .7203 .6878 .5728 .5168 . 5 .0002 .3597 .1254 .0520 .0219 .9680 .0000 .0000 .6827 .6575 .5373 .5543 . 5 .0003 .3669 .1042 .0272 .0271 .9755 .0000 .0000 .8255 .6275 .5373 .55243 . 7 .0009 .3718 .0562 .0141 .0139 .9901 .0000 .0000 .8597 .5659 .4670 .5439 . 7 .0008 .3725 .0269 .0082 .0079 .9932 .0000 .0000 .8731 .5184 .4067 .6655 . 7 .0060 .4625 .0162 .0165 .9913 .0000 .0000 .8731 .5184 .4067 .6655 . 7 .0060 .4675 .0694 .0249 .0231 .9891 .0000 .0000 .8477 .5000 .3778 .6690 . 7 .0060 .8771 .5000 .3778 .6690 .	10 10 10 10 10 10 10 10 10 10 10 10 10 1	43,60		1	DTAL" "PROFIL	Ī	51AL " TOT	AL STAT	10			
83 3,77 11,58 46,00 53,85 .0002 ,3597 ;1254 .0320 ;0319 ,9680 ;0000 .0000 ,6827 ,6575 ;5373 ;5272 ;1,79 49 47,18 52,55 .0003 ,3669 ,1042 .0272 ,0271 ,9755 .0000 ,0000 ,7255 ,6275 ,5136 ,5232 ;1,79 49,79 50,4009 ,3718 .0569 ,0019 ,0010 ,0000 ,0000 ,0000 ,0000 ,5497 .0569 ,4407 .0569 ,4407 .0569 ,4407 .0569 ,4407 .0569 ,4407 .0569 ,4407 .0569 ,4407 .0569 ,4407 .0569 ,4407 .0569 ,4407 .0569 ,4572 .0000 ,0000 ,0000 ,0000 ,0000 ,0000 ,4185 .0567 .0657 .0657 .0657 .0659 ,4672 .0660 ,4524 .0552 .0182 ,9913 .0000 ,0000 ,8731 ,5184 ,4067 .0655 .0657 .0694 ,0024 .0249 ,0231 ,9891 ,0000 .0000 ,8781 .5184 ,4067 .0655 .0699 .0249 .0249 .0231 ,9891 .0000 .0000 .8477 ,5000 .3778 .0699	2,24 4,17 9	•		.0980	.0244 .024	•		Ī	•	•	8915.	. 8543
23 4,17 9,49 47,18 52,55 .0003 .3669 .1042 .0272 .0271 .9755 .0000 .7255 .6275 .5136 .5532 . 1,79 4,78 9,37 46,09 50,67 .0009 .3718 .0505 .0141 .0137 .9901 .0000 .8597 .5659 .4670 .5437 . 1,30 4,43 8,80 45,22 49,59 .0008 .3925 .0269 .0082 .0077 .9953 .0000 .0000 .9195 .5280 .4930 .6021 . 1,34 4,54 10,02 44,46 49,90 .0012 .0421 .0132 .0128 .9932 .0000 .0000 .8731 .5210 .4936 .6551 . 2,34 4,54 10,02 44,46 49,90 .0012 .9425 .0128 .9932 .0000 .0000 .8731 .5144 .4067 .6655 . 2,34 4,54 17,02 45,56 53,82 .0060 .4627 .0694 .0249 .0210 .9932 .0000 .8931 .5144 .4067 .6655 . 2,34 4,54 17,02 45,56 53,82 .0060 .4627 .0694 .0249 .0231 .9891 .0000 .8977 .5000 .3778 .6690 . 2,34 17,18 17,78 17,65 56,06 .0050 .4627 .0694 .0249 .0231 .9891 .0000 .8977 .5000 .3778 .6690 . 2,43 17,18	1.23 4.17	46.00			!	;	;	,			··· 5243	-96695-
1,79	1.30		us.	•	•	•	•	Ī	_	•	.5232	9678
1,30 4,43 8,80 45,22 49,59 .0008 ,3925 .0269 .0008 .0009 .9953 .0000 .0000 .9195 ,5280 .4330 .6021 . 1,34 4,50 10.02 44,46 49,90 .0012 .4235 .0401 .0132 .0128 .9932 .0000 .0000 .8933 .5210 .4185 .6571 . 7,01 7,52 15,38 44,19 52,05 .0050 .4524 .0522 .0182 .0165 .9913 .0000 .0000 .8731 .5184 .4067 .6655 . 8,92 8,77 17,02 45,56 53,82 .0060 .4675 .0420 .0149 .0120 .9932 .0000 .0000 .8890 .5002 .3968 .6648 . 7,93 9,39 17,78 47,65 56,06 .0050 .5057 .0694 .0249 .0231 .9891 .0000 .0000 .8477 .5000 .3778 .6690 . NCORR MCORR TO/TO PO/PO EFF-P WC1/Al THLET INLET	1 . 30 4 . 43 B	:	:		•	•	1		` ;	•	\$ 5 4 3 9 ···	8832
1,34 4,55 10,02 44,46 49,90 .0012 ,4235 .0401 .0132 .0128 ,9932 .0000 .0000 .8933 .5210 .4185 .6571 . 7,01 7,52 15,38 44,19 52,05 .0050 .4524 .0522 .0182 .0165 .9913 .0000 .0000 .8731 .5184 .4067 .6655 . 8,92 8,77 17,02 45,56 53,82 .0060 .4475 .0420 .0149 .0120 .9932 .0000 .0000 .8890 .5082 .3968 .6648 . 7,93 9,39 17,78 47,65 56,06 .0050 .5057 .0694 .0249 .0231 .9891 .0000 .0000 .8477 .5000 .3778 .6690 . NCORR MCORR TO/TO PO/PO EFF-M EFF-P WC1/Al TNLET INLET INLET INLET INLET INLET INLET INLET INLET INLET INLET SEPTE		45,22		Ī	•	•	•		•	.4330	6021	.9214
7,01 7,52 15,38 44,19 52,05 .0050 .4524 .0522 .0182 .0165 .9913 .0000 .0000 .8731 .5184 .4067 .6655 .88,92 8,77 17,02 45,56 53,82 .0060 .4626 .0149 .0120 .9932 .0000 .0000 .8880 .5082 .3768 .6648 .77 7,73 47,65 56,06 .0050 .5057 .0694 .0249 .0231 .9891 .0000 .0000 .8477 .5000 .3778 .6690 .8891 .0000 .0000 .0000 .8477 .5000 .3778 .6690 .8871 .0000 .0000 .8477 .5000 .3778 .6690 .8871 .0000 .0000 .0000 .8477 .5000 .3778 .6690 .8871 .0000 .0000 .0000 .8477 .5000 .3778 .6690 .8871 .8771	1.34 4.50 10		ļ	1	32	•	•	1.	1		657	-8484
2 8.77 17.02 45.56 53.82 .0060 .4675 .0420 .0149 .0120 .9932 .0000 .0000 .8980 .5082 .3988 .6648 .3 3 9.39 17.78 47.65 56.06 .0050 .5057 .0694 .0249 .0231 .9891 .0000 .0000 .8477 .5000 .3778 .6670 . NCORR WCORR TO/TO PO/PO EFF-AD EFF-P WC1/A1 TNLET INLET INLET INLET INLET INLET INLET INLET SEFT	7.01 . 7.52 15.	_		•	•	•	•	•	_	•	• 6655	9748
3 9.39 17,78 47,65 56,06 .0050 ,5057 .0694 .0249 .0231 .9891 .0000 .0000 .8477 .5000 .3778 .6690 . N.CORR M.CORR TO/TO PO/PO EFF-AD EFF-P W.C1/A1 INLET INLET INLET INLET INLET INLET SEFF SEFT	90 8,92 8,77 17,02		~	į	•		•	٦,		. 3968 .	6649	-9.98 I.C.
TO/TO PO/PO EFF-AD EFF-P INLET INLET INLET S S	3 9.39 17.7	47.65	•	•	•	•	•	٠	•	,3778	0699	. 9895
	NCOR MCORR T	0/10 PO/P		-P #C1/A1						 		<u> </u>
	RPM LBM/SEC	מונבי זער										

Rotor Pressure Ratio = 1.3731

Po/Po Local

EFF-AD Adj.

P_o/P_o Inlet Adj. 1.348

WBLOW WTOTAL

WBLEED WTOTAL .00772

.9832

**************************************	MASA ENGL PAN TO 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2017-2 21-489 21-489 22-432 23-902 25-893 27-902	1000-30	@ 	VA-1 7SEC 536.8 529.9 510.1	VH=2 775EC F1 613.6 577.6	F		- B	8 2		NO.	75	SFEED C	V01	V01-2		70.00
76.0 613.6 536.8 613.6 546.4 -14.5 15.5 15.05 50.41 555.9 96.2 7.1149.4 -7711.8 670.8 77.5 15.05 613.8 536.8 613.6 546.4 -14.5 15.05 50.41 555.9 96.2 7.1149.4 -7711.8 670.8 7.7 15.0 15.05 52.4 50.4 96.4 7.7 15.0 17.1 1.	EAN TN - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -		000-70	@ F F N S F	500 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VM=2 013.6 577.6	F	1	~ •	7 = 2					_	Z = . O A		7
737.0 578.4 755.C 775.C	5 20,409 10,21,008 16, 21,589 30,23,314 60, 25,601				536.8 529.9 510.1 467.6	613.6 613.6 577.6	13EC FT		-		9	7			B 1 0 0 1 1 8 1	4 4 5 5 5 4	4	1
704.0 613.8 53.8 613.6 514.4 -11.5 19.21 -1.35 15.05 50.41 50.57 7 7.7 -11.4 19.4 7 -771.9 7 711.1 704.9 55.24 50.5 1 50.5 7 50.4 10.4 7 50.4 7 10.4 7 10.4 7 10.4 7 10.4 10.4 7 10.4 10.4 10.5 10.4 7 10.4 10.4 7 10.4 10.4 10.4 10.4 10.4 10.4 10.4 10.4	5 20,409 10 21,008 16 21,589 30 23,314 60,25,601		\perp \perp \perp		529 4 529 4 510 1 467 6	613.6 -577.6		125.00	GREE	בפאנגם	LGKEED	בפתנה	175EC T	ייי אנייי	173571	7050	1125	424
\$51,5 4 35,2 2 -28,6 44,02 -2,8 5 20,57 53,19 566,4 964,3 -196,9 -771,9 711;1 7 395,5 -35,7 43,6 4 -3,7 25,59 55,26 566,5 967,7 -244,3 -795,0 730,7 7 96,5 1	16: 21.589 16: 21.589 30: 23.314 50: 25.601	21,961 22,432 23,902 25,893 27,902	1 .		529.9 510.1 467.6	577,6	2.0.5		10.01	50.1	50.51	20.4	555	10201		0 1 1 / 1	0.0	
\$51,3 486,5 ~35,7 43,64 ~3,72 25,59 55,26 566,5 967,7 ~224,3 ~795,0 730,7 7 7 43,43 ~3.6,3 ~32,3	16: 21,589 30. 23,319 50: 25,601 70-27,818	22 432 25 893 27 902 29 382	.	1 1	510.1 467.6 438.4		512.2	-28.6	44:02	- 58 · Z ·	20.57	- 23 . 19 -	-266.4-	.64.3	-148.7	-771:9-	1111	74363
45.6 7 434.3 -36.3 42.88 -4.18 37.16 59.54 587.4 780.7 -354.6 -845.3 789.1 -845.5 395.5 -40.6 42.06 -5.14 47.04 63.7 643.5 1022.3 -471.0 -917.0 866.5 446.5 446.5 5 -40.6 42.06 -5.13 65.67 700.9 1081.1 -546.3 -471.0 -917.0 866.5 440.4 418.7 -32.4 45.01 -4.20 54.03 66.7 7 712.6 1117.4 -576.7 -1026.9 975.4 440.4 418.7 -32.4 45.01 -4.20 54.03 66.7 7 712.6 1117.4 -576.7 -1026.9 975.4 440.4 418.7 -32.4 45.01 -4.20 54.03 66.7 7 712.6 1117.4 -576.7 -1026.9 975.4 440.4 419.4 -32.4 45.01 -4.20 54.03 66.7 7 722.7 112.8 -610.6 -1056.9 1028.4 10.4 418.7 -4.45 56.39 66.20 733.1 1139.8 -610.6 -1058.3 1028.4 10.4 419.6 56.30 60.00 0 0.000	30 23 314 50 25 601 70 27 818	23.902 25.893 27.902 29.382	1.1		467.6	,	s	-35.7	43.64	-3,72	25,59	55,26	566.5	967.7	-244.3	-795.0	730.7	759.3
446.6 395.5 -40.6 42.06 -5.13 51.21 65.60 700.9 1081.1 = 546.3 -704.5 91.0 -917.0 846.5 8 446.5 3 -401.1 12.0 8 6.79 712.6 117.4 -576.7 1026.9 995.4 940.9 418.7 -32.4 45.01 -4.20 54.03 66.79 712.6 117.4 -576.7 1026.9 995.4 9414.9 417.8 -32.9 45.01 -4.20 54.03 66.79 712.6 117.9 -576.7 1026.9 995.4 9414.9 417.8 -32.9 45.01 -4.45 56.39 66.79 722.2 1129.8 -593.1 = 1042.7 1012.5 1423.3 417.8 -32.9 45.8 4 -4.45 56.39 66.79 722.2 1129.8 -593.1 = 1042.7 1012.5 1423.3 417.8 -32.9 45.8 4 -4.45 56.39 66.79 722.2 1129.8 -593.1 = 1042.7 1012.5 1012.9 1012.0 1012	50, 25, 601 70-27, 818		.	- 1	438.4	6.966	434.3	-16.1	42.88	. 44.18	37.16	- 59,54	587.4	780.7	5	-845.3	. 789.1.	-809.0-
##6.6 395.2 -10.1 #2.00 -5.13 51.21 65.60 700.9 1081.1 = 596.3 -001.5 995.4 #90.4 #18.7 -32.4 #5.01 -4.20 54.03 66.79 712.6 1117.4 = 576.7 -1026.9 995.4 #918.7 -32.4 #5.01 -4.20 54.03 66.79 712.6 1117.4 = 576.7 -1026.9 995.4 #918.7 -32.4 #5.81 -4.45 56.39 66.20 733.1 1139.8 = 610.6 -1056.3 1028.4 10.8 #917.8 = 32.9 #5.84 -4.45 56.39 66.20 733.1 1139.8 = 610.6 -1056.3 1028.4 10.8 #0.00 10	70 27,818	1 !	.	1	-	46.17	9 0	1	47 04	4	47	43 77	441.5	1022.1	0.174-	-917.0	866.5	876.4
#46.6 395.2 -10.1 #2.00 -5.13 51.41 65.60 /00.7 10.11 #46.4 #18.7 -12.4 #5.01 -4.20 54.03 66.77 712.6 1117.4 -576.7 -1026.9 975.4 #46.4 #18.7 -12.4 #5.01 -4.20 54.03 66.77 712.6 1117.4 -576.7 -1026.7 #23.3 #17.8 -12.9 #5.84 -4.45 56.39 68.20 733.1 1139.8 -610.6-1058.3 1028.4 #EGA-B D-FAC OHEGA-D LOSS-P LOSS-P PO2/ EFF-P EFF-AD EFF-P H-1 N-Z H'=1 P #EGA-B D-FAC OHEGA-D LOSS-P LOSS-P PO2/ EFF-P EFF-AD EFF-P H-1 N-Z H'=1 P #0012 3768 1106 0273 9708 0000 77417 6749 5337 4918 #0011 3991 1312 0335 0323 9655 0000 0000 7742 6188 4775 9488 #0017 4070 1159 0333 0228 9735 0000 0000 7742 6188 4775 9488 #0018 4241 0750 0217 0214 9907 0000 0000 88775 9314 5510 #0019 4424 0730 0217 0289 0000 0000 08173 5151 3714 5510 #0019 4424 0315 0220 9853 0000 0000 88775 5100 3714 5510 #0019 4424 0315 0220 9853 0000 0000 88775 5100 3714 5510 #0019 4457E S977 0287 9835 0000 0000 7781 5011 3768 6144 #0019 4877E LBH7SE S977 #0019 4878 8888 8888 8888 8888 #0019 6877 6877 6835 0000 0000 7781 5011 33612 6308 #0019 6877 6877 6835 0000 0000 7781 5011 33612 6308 #0019 6877 6877 6835 0000 0000 7781 5011 33612 6308 #0019 6877 6877 6835 0000 0000 7781 5011 33612 6308 #0019 6877 6877 6877 6877 6877 6877 6977	27.518		240.6	7.0														
440.4 418.7 -32.4 45.01 -4.20 54.03 66.79 712.6 1117.4 -576.7-1026.9 795.4 494.9 4118.7 -32.4 45.01 -4.23 55.21 67.36 72.2 1129.8 -593.1-1042.7 1012.5 1042.9 419.4 -3.2.9 419.4 -4.45 56.21 67.36 72.2 1129.8 -593.1-1042.7 1012.5 1042.9 419.4 -4.45 56.21 67.36 72.2 1129.8 -593.1-1042.7 1012.5 1042.9 419.4 -4.45 56.21 67.36 72.2 1129.8 -5010.6 -1026.3 1026.9 102.5 1026.9 410.6 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.2 102.3 417.8 -4.45 56.3 41		1			43.8	9.944	395.2	1.01-	42.00	E 2 1 3	51.21	09.59	100.4	1081.1	2.0.5	5.101	0.1.4	F . F .
#23.3 417.8 -32.9 45.84 -4.45 56.39 68.20 733.1 1139.8 -593.1-1042.7 1012.5 10 423.3 417.8 -32.9 45.84 -4.45 56.39 68.20 733.1 1139.8 -610.6-1058.3 1028.4 10 10 10 10 10 10 10 10 10 10 10 10 10	85 29 408	ļ		_	4,8.4	4.0.4	418.7	-32.4	45.01	-4.20	54,03	66.79	712.6	1117.4	-276.7-	1026.9	2 6 6	9.4.5
#EGA-B D-FAC OHECA-D LOSS-P LOSS-P PO2/ EFF-P EFF-AD EFF-P H-1 N-Z M'-1 PLOS 0.0012 376B 0.106 0.025-P LOSS-P PO2/ EFF-P EFF-AD EFF-P H-1 N-Z M'-1 PLOS 0.0012 376B 0.106 0.025-P LOSS-P PO2/ EFF-P EFF-AD EFF-P H-1 N-Z M'-1 PLOS 0.0012 376B 0.106 0.025 0.033 0.033 0.033 0.0000 0.0000 0.7427 0.048 0.025 0.033 0.028 0.032 0.0000 0.0000 0.7427 0.048 0.075 0.033 0.0298 0.023 0.020 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.00000 0.	an 27.914		588.0	I.	412.0	434.9	419.4	-32.1	.15.54	4.23	55.21	67,36	722.2	8	-593,1-	1042.7	1012.5	1010:6-
HEGA-B D-FAC OHEGA-B LOSS-P LOSS-P PO2/ EFF-P EFF-AD EFF-P H-1 H-2 H-1 H-2 H-1 H-1 H-1 H-1 H-2 H-1 H-2 H-1 H-2 H-1 H-2 H-1 H-2 H-2 H-1 H-2 H-2 H-2 H-2 H-2 H-2 H-2 H-2 H-2 H-2	95 30,382				405.7	423.3	417.8	•	45,84	\$ T.	56,39	68.20	733.1	1139.8	-610.6-	1058.3	1028.4	1025.4
HOCK 3766 .1106 .0276 .0273 .9708 .0000 .7407 .6749 .5337 .4918 .0011 .3991 .1312 .0335 .0332 .9708 .0000 .7407 .6749 .5337 .4918 .0011 .3991 .1312 .0335 .0332 .9755 .0000 .0000 .7154 .6468 .5025 .4998 .0017 .4070 .1159 .0333 .0278 .9735 .0000 .0000 .7721 .6188 .7795 .4988 .0017 .4070 .1159 .0331 .0278 .9735 .0000 .0000 .8775 .5587 .4314 .5610 .00159 .4872 .0560 .0171 .0144 .9907 .0000 .0000 .8773 .5151 .3914 .5610 .0159 .4848 .0730 .0241 .0188 .9880 .0000 .0000 .8773 .5151 .3914 .5610 .0331 .5206 .0704 .0315 .0200 .9853 .0000 .0000 .8169 .5130 .3382 .6080 .0331 .5206 .0794 .0377 .0287 .9853 .0000 .0000 .8169 .5111 .3768 .6144 .00251 .5505 .1049 .0377 .0287 .9835 .0000 .0000 .8169 .5011 .3768 .6144 .00251 .5505 .1049 .0377 .0287 .9835 .0000 .0000 .7961 .5011 .30612 .6308 .0000 .0000 .7961 .5011 .30612 .6308 .0000 .0000 .7961 .5011 .30612 .6308 .0000 .0000 .7961 .5011 .30612 .6308 .0000 .0000 .0000 .7961 .5011 .30612 .6308 .0000 .0000 .0000 .0000 .00011 .30612 .6308 .0000 .0000 .0000 .0000 .0000 .00011 .30612 .6308 .0000 .0000 .0000 .0000 .0000 .00011 .30612 .6308 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .0000 .0000 .0000 .00000 .0	INCS	INCH	DEV T	URN CA	HBER OF	EGA-B C	-FAC OH	EGA-B L	d-550	L055-p		EFF-P E	1	EFF.P		X-2		H - 2
.0012 .3768 .1106 .0276 .0273 .9708 .0000 .7407 .6749 .5337 .4918 .0011 .3991 .1312 .0335 .9708 .0000 .7154 .6468 .5025 .4998 .0017 .4070 .1159 .0332 .9755 .0000 .0000 .7721 .6188 .4795 .4988 .0017 .4070 .1159 .0333 .0298 .9735 .0000 .0000 .8773 .6188 .4795 .4988 .0008 .4741 .0759 .0213 .0200 .9907 .0000 .0000 .8773 .5151 .3914 .5510 .0008 .00159 .4848 .0730 .0241 .0188 .9880 .0000 .0000 .8773 .5151 .3914 .5510 .3018 .0000 .0000 .0000 .8773 .5151 .3914 .5510 .0000 .0000 .8773 .5151 .3914 .5510 .0000 .0000 .8773 .5151 .3914 .5510 .0000 .0000 .8773 .5151 .3914 .5510 .0000 .0000 .8773 .5151 .3914 .5510 .3018 .0000	PAN DEGREE D	EGREE DE	GREE" DE	GREE "DE	GREE SH	10CK	·	10	TAC P	ROFILET	T 104	OTAL T	OTAL S	TATIE	-			
2,70 5,64 12,50 46,07 53,84 ,0011 ,3991 ,1312 ,0335 ,0435 ,0000 ,0000 ,7154 ,6468 ,5025 ,4998 ,445	3,14	90.9	15.05	46.86	55.87	.0012	.3768		.0276	.0273	.9708	.0000	0000	.7407	.6749	,5337	9 1 6 5 9	.8372
3.24 6.18 11.33 47.35 52.56 .0017 .4070 .1159 .0303 .0298 .9735 .0000 .7421 .6188 .4795 .4988 .9735 7.44 11.04 47.06 50.67 .0046 .4241 .0759 .0213 .0200 .9855 .0000 .8275 .5587 .4314 .5151 .5151 .5346 10.90 47.20 49.60 .0068 .4872 .0550 .0171 .0144 .9907 .0000 .8773 .5151 .3914 .5151 .5151 .3914 .5151 .3915 .0000 .0000 .9194 .5151 .3915 .6200 .3914 .5915 .5916 .3918 .39	į	5.64	:	46.87	53.84	1100	ŧ		.0335	.0332	.9675	0000	.0000	.7154	6448	5025	4998	8378
4,45 7,44 11,04 47,06 50,67 ,0046 4241 ,0759 ,0213 ,0200 ,0000 ,0000 ,0275 ,5507 ,4314 ,5151 ,534		6.18		47,35	52,56	2100			.0303	.0298	. 9735	0000	0000	.7421	6819.	5444	4988	.8398
5.34 8.49 10.70 47.20 49.60 .0069 .4572 .0560 .0171 .0144 .9907 .0000 .8773 .5151 .3914 .5610 . 6.31 9.55 12.35 47.13 49.91 .0159 .4846 .0730 .0241 .0188 .9860 .0000 .8502 .5130 .3852 .6080 . 12.30 12.85 15.48 49.22 52.03 .0331 .5206 .0904 .0315 .0200 .9853 .0000 .8194 .5111 .3768 .6144 . 13.36 13.36 13.36 49.74 53.85 .0305 .5316 .0377 .0325 .0017 .9853 .0000 .8169 .5166 .3715 .6220 . 12.06 13.46 19.23 50.29 56.06 .0251 .5505 .1049 .0377 .0287 .9835 .0000 .0000 .7961 .5011 .3612 .6308 . 1NIET INLET INLET INLET INLET INLET LBM/SEC SQPT	4.45	7.44	i		50.67	- 0046	1	İ	.0213	0200	. 9855		0000	.8275	- 1855	+ 1 C h * -	-1516	1648
6.31 79.55 12.35 47,13 49,91 .0159 .4846 .0730 .0241 .0188 .9880 .0000 .8802 .5130 .3852 .6080 . 12.30 12.85 15.68 49.22 52.03 .0331 .5206 .0904 .0315 .0200 .9853 .0000 .8194 .5111 .3768 .6144 . 13.36 13.27 17.39 49.74 53.85 .0305 .0317 .0325 .0217 .9853 .0000 .0000 .8169 .516 .614 . 12.00 13.46 19.23 50.29 56.06 .0251 .5505 .1049 .0377 .0287 .9835 .0000 .7961 .5011 .3612 .6308 . 12.00 NCORR WCORR TO/TO PO/PO EFF-WCI/A! AREA INLET INL		8.49			09.64	• 00 B 9	4572		.0171	.0144	.9907	.0000	0000	.8773	1515	. 3914	.5610	. 8823
12.85 15.68		7.55	12.35	47.13		.0159	4848	1	-0241	.0188	- 9880	.0000	0000	.8502	-0613	23855	0809	1824
13.27 17.39 49.74 53.85 .0305 .5316 .0917 .0325 .0217 .9853 .0000 .0000 .8169 .5066 .3715 .6220 13.46 19.23 50.27 56.06 .0251 .5505 .1049 .0377 .0287 .9835 .0000 .0000 .7961 .5011 .3612 .6308 ORR WCORR TO/TO PO/PO EFF-P WCI/A1 AREA VIET INLET I	12,30	12.85		49.22	52.03	.0331	.5206	+040*	.0315	.0200	.9853	0000	.0000	.8194	1114.	.3768	**19.	. 6533
13.46 19.23 50.29 56.06 .0251 .5505 .1049 .0377 .0287 .9835 .0000 .0000 .7961 .5011 .3612 .6308 . CORR WCORR TO/TO PO/PO EFF-AD EFF-P WCI/Al AREA ULET INLET INLET INLET INLET INLET LBM/SEC 59FT PP LBM/SEC 8 SOFT	13,36	13.27	1	49.74 ··	53.85	.0305	.5316	4160	. 9326.	.0217	. 6883	.0000	0000	.8169	-9905	-3715-	- 6220-	-12965-
PO/PO EFF-AD EFF-P #C1/A1 INET INET INET IBM/SEC	95 12,06	13.46		50,29	56.06	.0251	5505	•1049	.0377	.0297	.9835	0000	0000	.7961	. 5011	.3612	6.630B	9696
TALET INLET INLET BHYSEC	Z	200	RP 10/	10 07	la Ere	-An EFF	/] = -	1	*									
FRON SECTION S	1 E	LET TAL	ET-THE	ET T'NE	ET-1N	ET TNE	ET TBK	Į,	L									
	æ	/H81 H4	SEC		PR ('		, t									

Rotor Pressure Ratio = 1,3905

9/ ₀	Local	.9793
EFF.AD	Adj.	77.65
P _o /P _o	Inlet Adj.	1.358
WBLOW	WTOTAL	.00816
WBLEED	W _{TOTAL}	ı

DIA-1 DIA-2 TY-5 CIAL DIA-2 TY-8 TY SEC FT/S	FT/SEC FT/SEC DEGREE DE	68 EE DEGREE FT/SEL 19.65	FT/SEC FT/SEC FT/SEC DEGREE DEGREE DEGREE FT/SEC FT	1063.7 1063.7 1063.7 1155.8 1155.8 1146.2 1467.3
974.0 807.977.7 794.0 807.7 794.0 807.7 794.0 807.7 794.0 807.7 794.0 807.7 794.0 807.7 794.0 797.8 721.9 740.5 719.	17/SEC DEGREE DE	8.05 SEE FT/SEC 8.09 SO.57 901.0 6.76 SO.57 901.0 6.76 SO.57 901.0 2.31 62.45 1180.7 2.31 62.45 1180.7 4.82 -64.34 1245.9 6.01 64.80 1245.9	507.66	1063.7 1063.7 1063.7 1157.8 1157.8 1151.5 1465.2
0375.6 1015.9 020.4 1012.9 697.6 037.3 994.0 807.0 990.4 651.6 0087.7 990.4 651.6 942.1 948.1 948.1 977.8 721.3 768.3 413.1 9831.3 777.8 721.3 768.3 413.1 9831.3 777.8 721.3 768.3 413.1 9831.3 777.8 721.3 768.3 413.1 9825.0 740.5 779.5 773.3 40.0 9825.0 740.5 779.5 94.7 771.9 41.0 94.1 0		4 .39 49 .22 886 4 6 .09 50 57 9010 1 6 .09 54 52 866 4 6 .09 54 52 1074 0 2 .31 62 45 1180 4 2 .31 62 45 1180 4 4 .82 67 45 1180 4 4 .82 67 43 1226 6 6 .92 67 43 1226 6 6 .92 67 43 1226 6 6 .92 67 43 1226 6 6 .92 67 43 1226 6 6 .92 67 43 1226 6 6 .92 67 43 1226 6 6 .93 1010 00000000000000000000000000000000	507.66	1063.7 1063.7 1157.8 11551.5 1151.5 1467.2
1037,3 994,0 807,0 990,4 651,6 1008,7 977,7 794,8 -972,9 621,1 948,3 922,0 775,8 915,0 545,4 902,1 871,7 761,6 865,1 403,3 81,3 777,8 721,3 768,3 413,1 81,4 777,7 764,4 771,9 41,0	-96.7 38.00 -5.66 2. -113.0 35.11 -7.04 3. -103.0 29.39 -8.99 5. -103.0 29.33 -7.99 5. -87.9 30.85 -6.94 5. -93.2 33.69 -8.20 5. -93.2 33.69 -8.20 5. -93.2 33.69 -8.20 5. -93.2 33.69 -8.20 5. -93.2 33.69 -8.20 5. -93.2 33.69 -8.20 5. -93.2 33.69 -8.20 5. -93.2 33.69 -8.20 5. -93.2 33.69 -8.20 5. -93.2 33.69 -8.20 5. -93.2 33.69 -8.20 5. -93.2 33.69 -8.20 5. -93.2 33.69 -8.20 5. -93.2 33.69 -8.20 5.	8.09 49.22 886.4 8.09 50.57 901.8 6.76 54.24 971.0 2.31 62.45 1074.0 2.31 62.45 107.0 4.62 64.34 1246.5 6.01 64.80 1245.9 6.01 64.80 1245.9 6.01 64.80 1245.9 6.01 64.80 1245.9 6.02 EFF-P EFF-AD	1516.4 -1566.0e1148.2 1017.1532.1 -424.7 -1183.3 1045.156.0 -58.9 -1270.7 1129.1661.4 -919.4 -173.0 1129.1661.4 -919.4 -173.0 1129.1661.4 -919.4 -173.0 1129.1661.4 -919.4 -105.0 -15.4 -1 1449.1660.3 -1050.1 -15.6 0.5 1471.	1063.7 1086.6 11254.6 11351.5 1446.2 1446.2
948.3 972.0 775.9948.3 922.0 775.831.3 777.8 721.831.3 777.8 721.831.3 777.8 721.831.3 777.9	= 113.0 35.11 = 7.04 3.11 = 7.05 4.21 = 7.	6.09 50.57 901.8 6.96 54.24 971.1 4.75 57.52 1074.1 4.82 64.34 1246.9 6.01 64.80 1245.9 6.02 67.43 1226.6 6.02 EFF-P EFF-AD	1552.1 -424.7-1183.3 1045. 1566.0 -583.9-1270.7 1129. 1661.4 -934.4-1473.0 1347. 1693.3-1022.5-1526.2 1347. 1690.3-1050.1-1560.5 1471. EFF-P H-1 M-2 H-2 H-2. 57671.0	1086.6 11257.8 11251.5 1445.2 1446.2
948.3 922.0 775.0 902.1 871.7 761.0 831.3 777.8 721.0 825.0 740.5 719.0 811.3 777.5	=113.0 35.11 =7.04 3.10 35.11 =7.04 3.10 35.11 =7.05 4.10 3.10 3.10 =7.05 4.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3	4.79 57.55 1074.0 2.31 62.45 1180.7 4.82 64.34 1246.5 6.01 64.80 1245.9 6.02 67.34 1226.6 0.7 TEFF P EFF-AD	1566.0 -583.9-1270.7 1129.1613.0 -756.8-1361.1 1240.1661.4 -943.3 1347.1679.5 1596.8-1361.1 1247.1693.9-1033.0-1534.1 1449.1690.3-1050.1-1560.5 1471.5 1471.6 1471.	1254.2 1254.2 1455.2 1446.2
902-1 871-7 761-6 831-3 777-8 721-8 825-0 740-5 719-8	= 106.9 32.39 = 7.05 4 = 121.5 29.79 = 8.99 5. = 103.0 29.33 = 7.99 5. = 87.9 30.85 = 6.99 5. = 93.2 33.69 = 8.20 5. PKGA=B LOSS=P LOSS=P POFILE PROFILE	4.79 57.55 1074.0 2.31 62.45 1180.7 4.82 -64.34-1248.5 6.01 64.80 1245.9 6.7 -67.43 1226.6 0.7 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7	1613.0 -756.8=1361.1 1240.1661.4 -934.4=1473.0 1347.1693.3=1020.5=1526.2 1424.1699.3=1030.1=1560.5 1471.5 FF-p H-1 StATIC	10054.2 10054.2 1005.2 1005.2 1005.2
831.3 777.8 721. 825.0 740.5 719.	=121.5 29.79 =8.99 5. =103.0 29.33 =7.99 5. =87.9 30.85 =6.94 5. =93.2 33.69 =8.20 5! HEGA-B LOSS-P LOSS-P P 10471 =0464 = 1559 6.0397 0.0390 6.	4.82 64.34 1248.5 6.01 64.80 1245.9 8.92 67.43 1226.6 027 EFF-P EFF-AD 027 TEFF-P TOTAL 037 TOTAL TOTAL 037 TOTAL TOTAL	1661.4 -934.4=1473.0 1347. 1693.3=1020.5=1526.2 1424. 1695.4=1033.0=1534.1 1449. 1690.3=1050.1=1560.5 1471. EFF-P H-1 H-2 H+1.	2 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -
825.0 -740.5 -719.3	-103.0 29.33 -7.99 -5. -87.9 30.85 -6.94 5. -93.2 33.69 -8.20 5. NEGA-B LOSS-P LOSS-P POFILE POFI	4.82 -64.34 1248.5 6.01 64.80 1245.9 8.92 -67.43 1226.6 02/ EFF-P EFF-AD 01 TOTAL TOTAL 01 TOTAL TOTAL 01 TOTAL TOTAL 01 TOTAL TOTAL	1693,311020,5=1526,2 124,1 1695,4=1033,0=1534,1 1449,1 1690,3=1050,1=1560,5 1471,1 142 1471,1 142 1431,1 142 1431,1 142 1431,1 142 1431,1 1431	1423.2 146.2 1467.3 H 0 = 2
777.7 696.	-93.2 33.69 -6.94 5. -93.2 33.69 -8.20 5. DMEGA-B LOSS-P LOSS-P P 101AL PROFILE P 11559 0397 0390 0	6.01 64.80 1245.9 8.92 67.43 1226.6 027 EFF-P EFF-AD 01 TOTAL TOTAL 01 TOTAL TOTAL 01 TOTAL TOTAL 01 TOTAL TOTAL	1695.4-1033.0-1534.1 1449.1690.3-1050.1-1560.5 1471.	1446.2 1467.3 M 0 E. Z
	MEGA-BLOSS-PLOSS-P 707AL PROFILE 1896 00471 00464	8.92 67.43 1226.6 027 EFF-P EFF-AD 01 TOTAL TOTAL 9169 00000 00000	1690,3=1050,1=1560,5 1471, EFF-P H-1 H-2 H-1 STATIC	1467.3-
655.3 633.	OMEGA-B LOSS-P LOSS-P P TOTAL PROFILE P 1896 0871 0864	02/ EFF-P EFF-AD 01 TOTAL TOTAL 9169 0000 0000	STATIC 9454 8855 7767	2 o M
		01 TOTAL TOTAL 9169 9169 9169 9169 9169 9169 9169 916	STATIC N=1 N=2 N=1 STATIC N=1 STA	¥ 1
	· •	01 TOTAL TOTAL 9169 0000	81A11C	:
DEGREE DEGREE	1896	0000	1917 - S 19 19 19 19 19 19 19 19 19 19 19 19 19	
	1559 ,0397 ,0390	000	C	.7878 7:3143
43,79 53,84	74		92/ 1/98	1.3227
52.41 .00302144	62c0 ccc0 6/21	0000		11,3359-
42,14 50,66	1130 .0315 .0308	0000	8255 ,8016 ,850	1,3615
39 44 49 59	10500319 0314-	1	00002792 - 78187549936;	1.1966-
38,78 49,88 ,000	1288 .0422 .0421		.1483 .7184 .6701 1.0271 1.4313	1.4313
37,32 32,13 0000	1641 0568 - 0568	0000	•	-44476-
37.79 53.74 .0000	0190, 0510, 0510	0000	•	1.4420
41,90 56.09	1827 . 0652 0652	0000	• ,•	-1:4244-
(4/15%-044443 CA1443 04/04 01/01 8865% 8865%				
INLET INLET I	1/5EC			
_	38.67			

Rotor Pressure Ratio = 1.7138

P _o /P _c	.9553
EFF.AD Adj.	77.50
P _o /P _o Inlet Adj.	1.631
W _{BLOW}	.00533
WBLEED WTOTAL	ı

V-2 -VM-1	7/SEC FT/SEC FT/SEC FT/SEC FT/SEC OLGREE DEG	7.500.3 625.8	678.2 695.2 670.5 470.0 =101.8 34.06 -8.64 51.61 65.24 1120.5 1601.5 -878.4=1454.3 1348.4 = 65.67 1120.5 1601.5 -878.4=1454.3 1348.4 = 65.67 1120.5 1601.5 -878.4=1454.3 1348.4 = 65.67 1120.5 1601.5 -878.4=1454.3 1348.4 = 65.67 1120.5 1601.5 -878.4=1454.3 1348.4 = 65.67 1120.5 1601.5 -872.7=150.0 1450.0 = 65.67 1120.0 1450.0 = 65.67 1120.0 1472.7 = 650.2 650.2 650.2 650.2 650.0 =61.6 38.43 =6.15 57.05 67.05 1159.1 1653.9 972.7=1530.0 1472.7	ONEGA-B D-FAC ONEGA-B LOSS-P LOSS-P PO2/ EFF-P EFF SHOCK TOTAL PROFILE PO1 TOTAL TO1 7	9,16 46,11 52,47 0004 03552 0779 0190 0131 9719 0000 0000 8772 8596 7043 7495 18 9,85 0000 0000 0000 8840 8005 6594 77895 18 0000 0000 0000 8840 8005 6594 77895 18 0000 0000 0000 8840 8005 6594 7788 18 0000 0000 0000 8840 8005 6594 7788 8005 8005 6594 7788 8005 8005 8005 8005 8005 8005 8005	0 - 0055 - 4564 3 - 0070 - 4729 6 - 0070 - 5359	NCON MICH INLET INLET INLET INLET INLET INLET INLET INLET INLET INLET INLET INLET INLET INLET INLET INLET INLET INLET INLET INCOMPANYSE IN
ATOR ANGLES ENGLISH IA-1 DIA-2	**************************************	22,432,991,9- 23,902,925,8	27,902 839,2 29,382—839,1 79,856 824,1 30,293—809,5	- 3	2.72 8.62 2.72 8.62 7.76 10.23	86 34 5.02 16.07 42.45 80 5.34 5.02 16.07 42.45 86 4.52 6.15 17.52 44.55	INFET INFET

Rotor Pressure Ratio = 1.7997

P _o /P _o Local	9776.
EFF-AD Adj.	81.28
P _o /P _o Inlet Adj.	1.753
W _{BLOW} W _{TOTAL}	.00532
WBLEED WTOTAL	ı

BLOW ONLY, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

STATOR ANGLES					AIRFOIL	- 1	AEROD YNAMIC	SUHHARY	Y PRINT	_ :		- 4	3:27:38	1 2 0	JULY 20	26,1971
5 - C	<u>.</u>			VH-2	1-0^	V0-2	1-0	8-2	8,-1	# KON	,	SPEED C		2012		70°65 3
1 20.409 2	21.489 1059	9 9 831	7 764.	0 828.2	77/SEC." F 733_8	7/SEC_0t _76.3	6866 DE	.GMEE .Dt	.GREE 01	53.43	1/SEC 905.3	1/5EC F 1390.2	1/56C F -254.1-	1756C.F.1 1116 ₆ 5	7 St C - F	1040.2
2 21 589 22	22 432 974	9. 770	3 720	3 763.8	657.0	5 66	42.76-	.6.39	23,69-	55,51	9 6	1397.3	-327.2-	1151.6	016.9	1063.1
5 25 601 25	902-918	3.9-738		5 731.3	5733	101.5	10.55	7,90	97,26	59,84	977.4	1455.6		1-1258.5	128.6	1157,0
72 919 22	7 902 653 4	13.4 67	2089 8	5 663 0	6.915	=107.9	37.11	92.6-	50.68	65.55	1079.9	1602.4	831.7	458 6-1	346.6	1350-7-
-	1958	79	0	3 613.2	24		40.29	6.24	08.48	67.0	1109.2	632.5	406.00	3-1513.0	448	4.5
"	5	-	1) ;	D-FAC 0	OKEGA"B DEFAC ONEGA"B LOSS"B		0.88-9	P02/ E	EFF B EF	Ţ			2-#		~
DEGREE DEGREE DEGREE	REE DEGRE	6-			20.4	146.			2		ĭ" c	TAT16	6 2	7035	7027	1,1759
1	43 - 9	64	16 53 8	000	-	1320	0335	0311	474	0000	0000	7453	8792	6730	7083	1813
2, 1	2.11.5	32-49	4550.6	0108	4082	- 1	0171	.0231	9792	0000	0000		7907	- 6224	.7590	1.2271
2.40		01 46.1	12 49.5	0201	4080	.0632	.0192	1610	9792	0000	0000	9159	.7762	6208	.8329	1,2851
25.0	6 62 12	29 46.	15 52 0	90136	40.4	0665	0346	2010	9775	0000	0000	7812	7157	5336	9397	. 3539
67.7	9.28 15	24 46 5		9	•••	1204	0425	0355	9661	0000	0000	7613	7016	\$905°	9297	3,00
NCOR	CORR	10/10	04/04	EFF-An EFF-B wellAl	1 m a											:
INC	TNLCT	TNET	TNLET	TNETTA	LET LBH	LBH/SEC										
100				ь												

Rotor Pressure Ratio = 1,8663

P_o/P_o Local

EFF-AD Adj.

P_o/P_o Inlet Adj.

WBLOW WTOTAL

W_{BLEED} W_{TOTAL} .9673

80.46

1.801

.00518

1

JULY 26,1971		7 1001 7	11.55.55	7 1420.4	9 1464.5	1 M'-2	57 1.1371	64 1,1554	26 1,1735	7340 1,2051		67 1, 3403	52 1,3247	59 1,3251	
•		1194,6 1043	1259 6 1127	1251 9 9451	1524.9 1468	H-2 H-1	6679 685	6374 69	69. 1519.	:	68 - 6155	5327 91	5075	4709 .905	
13;28;46	V0+1	8 377 3	8 520 9	8 868 3 6 879 -	2 -896.8		78 9161	54 8788	 	747 - 1792		7234	17 , 70 PB	*849 00	
0.000.7	36137 CE 5EC FT/5E 87 1 1351	02 3 1374	53 4 1436	90.4 1628	087.1 1630	-AD EFF-P	DIAL STATI	12. 0000	•	0000 .8591	•	9254	•	•	
1 N	5EGREE FT/	56.76 B 58.78 B	62.17 9	01 92 99 01 92 99	69.30 10	EFF-P EFF-AD	TOTAL TOT	• •	•	•0000	0000	0000	•	• 1	
HHARY PRIM	E DEGREE (65 23 35	56 37 62 78 43 63	75 52 78	01 55.59	P02/	1 PO 1	88 9349	69 ,9537	•	98.6	• •	62 ,9703	43 .9575	
AIRFOIL AERODYNAMIC SUHHARY PRINT	3-1 8-2 REE DEGRE	13,47 6	41 89 8 40 81 6	18 72 40 40 40 40 11 87 5 5	12.96 -6.	055-P L055-P	TAL PROFILE	0416 0388	•		200	0297 0212	•	•	
FOIL AEROD	VO-2 B	87.5	93.8	762	+ 09-	ONEGA-8 LOSS-P	107	699	1254	.0722	5000	0857	1037	.1526	101/A1 184/5EC S9FT
AIR	2 V0-1	999 8	3 606 2 588 2	8 553 4	9.175 0.	D-FAC	4.1.4	12 4473	95		0 2 7 3 0 0	46 5038	•	92 ,5820	ET INET LBH/SE
1	VH-1 VH- /SEC FT/SE 748 1 79.	136.2.752	681.2 705	6595 642	614.2 576	HEER ONEGATE	EGREE SHOCK	3.04		1	020				ET INCE
	SEC. FT	7	-	647.3	579.2	INCH DEV TURN CAHBER OF	DEGREE DEG	50.12	.03	50.45	ı		46,90	48.97	WCORR TO/TO PO/PO EFF TWLET TWLET TWLET TWL BH/SEC
S	2 V=1 FT/SEC	61 1014.4	93 900.0	500	93 839.3	M DEV	E DEGREE	12 8 2 8 21		99.9 54.	7. 8 82	713.17	77 16.54	61 17.66	WCORR TO
STATOR ANGLES	1 014-1 014-2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		314 23 902	9 408 29 382	30.382 30.293	INCS THE	REE DEGRE	21.5 91.2	2,97 5,9	•		7,67	6 06 6	2	NCORR INCET
STA	N SPAN TN	1 -	N 00		30		SPAN DEGREE	9		8:	8 1	ຂ່ໝ	8	8 8 -	

Rotor Pressure Ratio = 1.9079

Po/Po Local

EFF-AD Adj.

P_o/P_o Inlet Adj.

W_{BLOW} W_{TOTAL}

WBLEED WTOTAL .9663

81.14

1.838

12 12 12 12 12 12 12 12	
44445644664464444444444444444444444444	1.23.6 1.30.6 1.
70LT 20-197 70LT 20-197 70M1 70M1 70M1 70M1 70M1 70M1 70M1 70M	
14444444444444444444444444444444444444	
0.00 - 1.	2
10.22 10.22 10.22 10.22 10.23 10	H=1 H=2 H=2 H=1 H=2 6709 6518 6794 11108 6794 11108 1137 1137 1157 1158 1137 1158 1158 1158 1158 1158 1158 1158 115
13:116:32 CODE 10:POINT 8 V0'*2 F7/5c F7/5c F7/5c -3/45:6-107;6 -3/7:8-1139;8 -3/7:8-1139;8 -6/5:2-1139;8 -6/5:2-1139;8 -6/5:2-1139;8 -6/5:2-1139;8 -6/5:2-1439;4 -6/5:2-1435;4 -6/6:2-1435;4 -6/6:2-1435;4 -6/6:2-1435;4 -6/6:2-1435;4 -6/6:2-1435;4 -6/6:2-1435;4 -6/6:2-1435;4 -6/6:2-1435;4 -6/6:2-1435;4 -6/6:2-1435;5 -6/6:2-1435;4	
13716:32 1922:0 CODE U. POTENT VOTENT	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
# 32.5PEED CODE 10.POINT # 13.PAGE 36.02 V***I V***Z VUC**I VVO**Z VWIT VUC**Z V***I VV**Z FT/SEC FT/SEC FT/SEC FT/SEC 777.6 1322.6 = 245.6=1071.6 997.1 1057.3 798.2 1357.7 = 318.5=1139.8 1016.1 1062.2 797.2 1380.0 = 317.8=1184.4 1044.2 1084.9 841.6 1414.0 = 516.9=1240.7 1127.6 1156.0 930.8 1485.3 = 646.2=1313.4 11238.2 1152.3 1073.7 1605.8 = 868.5=1475.9 142.2 4 144.0 1073.7 1605.8 = 868.7=1480.6 1446.8 1444.0	1AL STATIC STATIC
7774 777 777 777 777 777 777 777	4
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	SHOCK SHOCK
E	m o
23.54 23.54 23.54 23.54 23.54 50.25 50.25 50.25	10000000000000000000000000000000000000
50HHAR 17.99 17.99 17.99 17.99 17.99 17.99 17.99 17.99 17.99 17.99 17.99 17.99	00 00 00 00 00 00 00 00 00 00 00 00 00
#16.550HM #16.550HM #16.650H #16.	PROFILE - 01449 - 0188 - 01
TIRFOIL AERODYNAMIC_SURHARY PRIN EC FTSEC DEGREE D	EGA-8-L05S-P-L05S-P 1745 01446 01419 1745 01446 01419 1760 0122 0154 1760 0122 0154 1760 0122 0128 1760 0122 1760 0128 1760
######################################	1745 1745 1763 1763 1763 1763 1763 1763 1763 1763
77 V O 1 T V S C C V V O 1 T V S C C V V O 1 T V S C C V V O V V O V V O V V O V V O V V O V V O V V O	187 - 1745 188 - 1745 188 - 1765 188 - 1765 189 - 1765 189 - 1862 189 - 1852 189 -
7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	44887 44887 4458 4458 4458 5882 5875 5875 5875 5875 5875
7755 7755 737-10 738-11 708-11 653-6 653-6 653-6	SHOCK SHOCK ONEGA BLOCK ONEGA BLOCK ON SHOW SHOW ON SHOCK ON SHOW ON SHOCK ON SHOCK ON SHOCK ON SHOCK ON SHOCK ON SHOCK ON SHOCK ON SHOCK ON SHOCK ON SHOCK ON SHOCK ON SHOCK ON SHOCK ON SHOCK
	PACKONNE MAI
	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
7 V=2 7 T/SEC FT/ 7 T/SEC FT/ 7 15-0 683.6 683.6 683.7 683.7 683.7 683.7	URN CA 440-647 440-647 440-64
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 DECREE DEGREE DEGREE SE SE SE SE SE SE SE SE SE SE SE SE S
SPEC PEC	CH CORRECTED
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	GREE DEGREE DEGREE DEGREE 2.70
STATOR_ANGLES NASA ENGLISH DIAL! DIA-2 BU N 1 DIA-2 S 20-409 21-96 10 21-008 21-96 10 21-589 22-43 10 23-314 23-90 10 23-816 27-90 10 27-816 27-90 10 27-816 27-90 10 27-816 27-90 10 27-816 27-90 10 27-816 27-80 10 27-816 27-80	10055
STATOR N 1 A 1 C C C C C C C C C C C C C C C C C	AN DE GREE 2 2 3 4 4 5 1 2 4 4 6 1 1 4 6 1 1 1 1 1 1 1 1 1 1 1 1 1
: 8	1NCS 1NCH DEV TURN CAMBER MEPAN DEGREE DEGRE
	 1

Rotor Pressure Ratio = 1.9269

P_o/P_o Local

	STATOR ANGLES	ANGLES					A IRF	AIRFOIL AERODYNAMIC SUMHARY PRINT	DYNAMI	C SUMHA	RY PRIN	-		ci,	1:00:52	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	Jeust 3	C1:03:52 AUGUST 31+1971
Z	WASA ENGLISH (SPECTAL)	SI	PECIAL)									# NOR		SPEED CO) DE 100	0In1 #	15 + PAGE	36.02
	DIA-1 DIA-2	DI A-2	٧-1	V-2	VH-1	VM-2	V 0-1	V 0-2	e- 1	8-S	81	82	_	21	VG*-1 \	20/	U-1	N-2
A SPAN I N	HUNI		FT/SEC FT/SEC FT/SEC	TASEC F	T/SEC F	T/SEC F	I /SEC FT	/SEC DE	GREE DE	GREE DE	GRFE DI	EGREE. F		IVSEC F	I/SEC FI	/SEC FT	/SEC F1	/SEC
-	20.409	20.409 21.489 1039.7	1039.7	746.4	722.8	745.3	747.3	0.04-	45.95	-3.07	18,39	55.39		1312.1	-24 3 3-1	1073.8	94789	1039.8
5	10 -21:008 21.961 T007.5	71.961	1007.67	713.9	723.3	711.2	2 704.5 -61.0 44.36 -4.92 23.42 57.66 78	-61.0	44.36	-4.92	23.42	57.66	•••	1330.0	-312•Č-1	123.7 1	016.6 1	1062.7
1	21.589	11.589 22.432	967.1	684.9	4°C69	580.0	677.1	-81.8	64,45	-6.87	28.05	59.77	. ,	351.1	-367.5-1	167.2 1	044.7	1085.5
8	23,314	23.902	869.6	627.8	603.4	622.4	626.1	-82.1	90.94	-7.51	39.75	63.32	-	1386.3	-505-0-1	1239 • 7 1	1128.1	1156.6
3	25.601	25.893	870.6	651.1	621.1	647.3	610.1	-40.9	64.44	-6.25	45.35	63.94	٠.	. 9.8741	-628-8-1	323.9 1	238.8 1	1252.9
2	27.818	27.902	852.9	635.5	628.5	631.0	576.6	-75.5	42.54	-6.82	50.73	66.12	-	1.6551	-769.5-1	1425.6 1	1346-1	1350.2
8	. 29.408 29.382	29+382	877.9	642.6	638.1	639.6	602.9	-61.3	43,37	-5.47	52.11	19.99	•	1615.1	-820-1-1	483-1 1	423.0 1	1421.8.
8	29.914 29.85	29.856	874.2	630.0	619.0	628.7	617.2	-36.8	44.92	-3,33	53,30	67.00	-	1.609	-830.3-1	1481.5 1	1447.5	1444.7
98 !	30-382 30-293	30.293	0.498	598.3	593 6	597.4	623.0	-33.6	46.15	-3.23	54.75	68.28	•	1614.2	-847-1-1	439.4 1	470.2 1	1465.9
					:		:		:	:								
	INCS INCH	INCH	730	TURN CAMBER		MEGA-B	B D-FAC CHEGA-B LOSS-P LOSS-P	ECA-B L	1 4-SSO.	-0550-	P02/	EFF-P EFF-AD E	FF-AD	EFF-P #		M-2	H -1	H2
* SPAN	* SPAN DEGREE DEGREE DEGREE DEGREE DEGREE	DEGREE"D	EGREE D	EGRES 0		HOCK		Ξ.	JTAL P	ROFILE	P01	OTAL T	OTAL S	TATIC				
9	3.58	6.50	13.33	49.03	_	.0145	.4665	•1974	.0491	.0455	.918	0000	•0000	. 6844	.9019	.6243	.6621 1	1.0974
2	3.02	55.95	10.52	1,9.28	53.84	.0136	. 4821	.2053	• 0523	•0488	.919	.0000	•0000	.6740	-87 42	. 59 70	• 6809	1.1121
	3.91	6.85	8. 03	51.33	52.40	.0174	2464.	.1804	• 0469	.0424	.933	0000	•0000	.7109	•8378	.5718	.6768	1.1280
8	7.54	10.53	7.72	53.57	50.67	.0374	9,05	•0803	,0224	.0120	•9755	0000	0000	.8658	-7427	.5216	.5676	1.1517
.	7.82	10.95	9.77	50.74	49.55	9640*	906 + •	.0797	.0243	16 00 •	.975	0000	.0000	• 8525	.7368	.5385.	.7463	1.2186
2	6.88	10-12	10.68	49.36	26°64	.0439	.5080	4460	.0311	.0166	.972	00000	00000	.8247	.7181	+5233	.8361 1	1.2839
	10.92	11,26	14. 42	48.85	52.01	•0483	• 5326	1001	.0502	•0332	.926	0000	.0000	. 74 09	.7 329	. 5237	- 8676	1.3164.
8	12076	12:72	18.29	48.25	53,85	9450	.5455	.1574	.0558	.0364	.953	0000	00000	.7247	•7259	•5106	. 8600 1	1.3044
8	12,33	13.78	20.45	49.38	56.06	.0557	. 5820	.1911	• 0688	.0488	116.	.0000	0000	.6880	.7142	. 48 24	.8578	1,3013

NCORR WCORR TO/TO PO/PO EFF-AD EFF-P WC1/AI INLET INLET INLET INLET INLET INLET LBH/SEC RPM LBM/SEC * * SOFT IID90- 174-54 I-2473 I-890D 80-57 82-22 32-85

Rotor Pressure Ratio = 1.9982

P _o /P _o Local	.9575
EFF-AD Adj.	80.17
P _o /P _o Inlet Adj.	1.879
WBLOW WTOTAL	.00546
WBLEED WTOTAL	ı

BLOW ONLY, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

AIRFOIL AERODYNAHIC SUHHARY PRINT RUN # 3 VH=2 VD-1 VD-2 B-1 B-2 B-1 B-2 FT/SEC FT/SEC DEGREE DEGREE DEGREE FT/SEC 64,9 719,1 -72,5 45,91 -6,07 -23,11 56,43 735, 64,9 719,1 -72,5 45,91 -6,07 -23,11 56,48 755, 64,9 719,1 -72,5 45,91 -6,07 -23,11 56,48 755, 65,3 61,8 -44,5 -93,5 47,45 -6,07 -23,11 56,48 755, 613,8 644,5 -93,5 46,16 -8,42 7,52 50,16 66,46 752, 624,3 644,5 -93,5 46,19 -7,52 50,16 66,46 752, 624,3 644,5 -83,5 46,19 -7,52 50,16 66,46 752, 615,0 65,7 -62,5 46,19 -7,52 50,16 66,46 752, 616,0 65,7 -62,5 46,18 -7,57 51,80 67,46 91,1 616,0 65,7 -62,5 46,18 -7,52 50,16 66,46 77,7 981, 616,0 65,7 -62,5 46,18 -7,57 51,80 67,47 91,1 616,0 65,7 -62,5 46,18 -5,07 64,6 91,12 60,00 600 618,5105 -21,67 60,52 60,54 91,11 70,11 60,11
7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7

P_o/P_o Local

EFF.AD Adj.

P_o/P_o Inlet Adj.

WBLOW WTOTAL

WBLEED WTOTAL

Rotor Pressure Ratio = 2.0123

.9464

77.96

1.898

LES	AHIC SUMMAR	PRINT		-	Ö :		שר אחר	-
ENGLISH (SPECIAL) A.S. V1 V2 VM-1 VM-2 VG-1 VG-2	8-2	RUN 81 . 82	32	+ SPEED CO	CODE 10,PO	* 01N1 *	16,PAGE U-1	36.02
1NFT/SEC FT/SEC"FT/SEC"FT/SEC"FT/SEC"FT/SEC"FT/SEC"FT/SEC"FT/SEC"FT/SEC	E DEGREE DEG	DEGREE DEGREE	FT/5EC-F	۴ _	1/SEC F1	1/5£C" [1]	7/5EC-F	1/5tc
21.008 Z1.961 1000.7 679 9 699 69 69 69 69 69 69 69 69 69 69 69	69 5 32	ŗ	197	313.5	• •	-	5 9 101	200
21,589 22,432 961,4 654,2 670,3	81 -7.31	5	4 759 8	1336.7	355,4-1	1168.4	9.440	P. 5801
30 23,314 23,902 870,9 609,0 586,4 603,3 643,8	58 - 7 -	9 15.	9.092 - 50	1374.7	484.2-	1239 . 7	. Q . g Z I I	
25,893 872,8 626,6 601,1 621,0 632,8	59.	۰ د	7 853 4	1473.5	605	1336.2	1238 ,	1252,8
27,818 27,702 865,3 627,3 607,5 621,3		7		1564.0	7.27		345	1350.0
85 29 408 29 382 888 6 634 1 609 8 630,2 646,3 w	۶.	1.86	1 987		٠.	1492,3	1422.9	1421.6
914 24 856 B66 2 628 2 540 0 625 6 661 0	25 -5.11	53,1267	37 463 1	629.	802	5,0081.		7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
TOPER 20,00 7000 00,00 00000 0000 0000 7000 7	'		- !	-!		0 0 0 0		
INCS INCH DEV TURN LANKER ONEGA-B D-FAC ONEGA-B	P 1055-P	PO2/ EFF-9	EFF-AD	EFF.p	-	7-X		H 2
XEE SHOCK	PROFILE	-	TOTAL	TATIC				
7.89 12.57 51.18 55.87 .0192 .5037 .2117	7	42	0000	•	.8938	0045*	.6377	1.0791
9 33 7 7 26 10.12 51.01 51.84 7.0179 51.59	0548 0503	79167	0000	6796	-867 F	2895	1959	-6260-1
5.19 8.13 7.58 53.11 52,38 ,0228 ,5267 ,1882		9318 0000	•	7181	8321	5437	6552	1109
9 08 12 07 7 37 55 52 53 67 0495 5330 1850	600	9741	:	6700	7429	5038	- 9449 -	1407
12,92 8,37 54,13 49,55 ,0679 ,5324 ,1021		• •	• •	, 8330	7360	5153	7162	2117
9 73 -12 96 - 9 61 53 29 49 93 - 0710 5437 - 1120 -	į.	' '	•	9210	7241	5127	-1929-	2789-
13,95 14,49 13,49 53,06 52,02 ,0812 ,5686 ,1622	•	0000 6056	•	7340	7362	,5 i 26	919	3004
15.98 15.94 16.53 53.16 53.87 87 87 6097 5790 1684	96 0279	0000 7486	0000	7238	7310	1503	1118:	2700:
15,86 17,21 18,52 54,79 56.07 ,0934 ,6061 ,	,	9451 ,0000	•	6958	7193	9181	.8070	,3084
		i						
INCETT								
LBM/SEC S SQ								
11089, 170,71 1,2587 1,9243 79,36 81,19 31,57								
Rotor Pressure Ratio = 2.0146								
	3	;		;				
	WBLEED	WBLOW	MO	٩° ٩°		EFF-AD		0/0
	WTOTAL	w _T o	WTOTAL	Inlet Adj.		Adj.	-	Local
	ı	.00558	89	1.913		78.95	o.	9532

BLOW AT 48 PERCENT CHORD ONLY, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

7 / V V V V V V V V V V	7 SEC F7	#775EC F75EC F75EC DEGREE DEGREE F06REE F75EC F7	E O C C C C C C C C C C C C C C C C C C	E DEGREE FT/SEC FT/SEC FT/SEC BT/SEC FT/SEC	755C F75C F75C F75E F75E F75E F75E F75E F75E F75E F75E	7 VO 1 1 VO 1 1 VO 1 1 VO 1 1 VO 1 1 VO 1	755C FT/5EC FT/5
5 20.407 21.487 1075.4 1020.4 81 10 21.006 21.961 1037.0 999.2 80 30 23.314 23.902 949.2 927.0 77 80 25.601 25.893 901.9 874.7 76 70 27.616 27.902 931.9 784.0 77 80 29.914 29.856 811.2 732.1 69 80 29.914 29.856 811.2 732.1 69 80 29.914 29.856 811.2 732.1 69 80 29.914 29.856 811.2 732.1 69 80 29.914 29.856 811.2 732.1 69 80 20.962 80.25.0 70RN CAHB	4.2 977.4 621.9 4.2 977.4 621.9 5.4 919.0 545.7 1.0 769.7 1483.6 1.0 769.7 1483.	121.9 35.14 17.12 19.03	25 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	38 5 6 1 6 6 1 6 6 1 6 6 1 6 6 1 6 6 1 6 6 1 6 6 1 6 6 1 6 6 6 1 6 6 6 1 6 6 6 1 6 6 6 1 6 6 6 6 1 6	551.7 = 252 551.7 = 252 551.0 4 = 423 551.0 4 = 423 551.0 8 = 562 551.0 8 =	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	708.0 1016.7 101
16 21.589 22.432 1008.5 983.0 775.2 30 23.314 23.902 940.8 927.0 77 76 30 25.601 25.893 901.9 874.7 776 30 25.601 25.893 901.9 874.7 776 30 25.914 29.856 831.1 780.0 72 80 29.914 29.856 811.2 73.2 69 80 23 30.293 760.8 811.2 73.2 69 80 23 87 87 87 87 87 87 87 87 87 87 87 87 87		104,4 38,03 = 6,114,9 38,12 = 7,114,9 38,12 = 7,114,9 38,12 = 7,114,9 38,12 = 7,114,9 38,12 = 8,114,9 38,12 =	2	443 1073 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	00000000000000000000000000000000000000	12.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
30 23.314 23.902 946.2 927.0 777 50 27.818 27.902 831.1 780.0 72 86 29.908 29.318 2 824.9 744.9 77 6 80 29.914 29.856 811.2 732.1 69 80 29.914 29.856 811.2 732.1 69 80 29.914 29.856 811.2 732.1 69 80 20.293 760.8 658		121.8 35.14 =7.126.2 29.82 =7.26.5 29.35 =7.76 = 29.35 = 2.76 = 2	25	09 1247 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	666574 66650	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	# 4422 # 4422
80 25,601 25,893 901,9 874,7 76 70 27,818 27,902 831,1 780,0 72 86 29,918 29,918 29,744,9 744,9 71 86 29,914 29,856 811,2 732,1 69 86 30,382 30,293 760,8 658,8 63 SEAN DEGREE D		114.9 32.42 -7. 126.2 29.82 -9. 197.6 -9.35 -7. 197.7 - 33.72 -8. 197.1 - 33.72 -8. 166.8 LOSS - PROFI	55 44.77 57 53 54 55 56 56 56 56 56 56 56 56 56 56 56 56	.63 1073.0.1 .07 1179.6.1 .08 1244.7 .38 1225.4 1	6420.01 645.01 645.04 6	7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 4 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
86 29 918 29 382 824 9 744 9 7 9 9 9 9 9 9 9 9 9 9 9 9 9 9		297.66 29.35 27.66 29.35	55 55 90 64 90 65 90 65 90 65 90 65 90 65 90 65 90 65 90 65 90 65 90 65 90 90 90 90 90 90 90 90 90 90 90 90 90	124749 18 122549 18 122549 19 12710	2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	# 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
90 29.914 29.856 811.2 732.1 69.85 30.392 30.293 7.60.8 658.8 63.8 63.8 63.8 63.8 63.8 63.8 63.8 6		#97.1 - 33.72 8. FGA*8 LOSS*P LOSS	51 58.90 64 51 58.90 67 F PO1 TOTA	.61 1244.7 1 38 1225.4 1 EFF-AD E	695.6-1031 694.2-1098 FFFP HT	8=1531.8 9=1563.5	399 I 400 K
88 30,392 30,273 '60,8 658,8 03. 1NCS 1NCH DEV TURN CAMB SEAN DEGREE DEGREE DEGREE DEGREE 6 2 05 05 05 05 05 05 05 05 05 05 05 05 05		EGA-8 LOSS-P LOSS TOTAL PROFI	51 58.70 6/ -P PO2/ EFF -E PO1 TOTA	-38 1225.4 1 -p EFF-AD E L TOTAL ST	674.2=1048 FF-P H-1	.v.1563.5	9951 I ** E
SPANDEGREE DEGRE		EGA"B'LOSS"P LOSS	-P - PO2/ - EFF	TP EFF-AD E	FF"P H"	H-2	- H I - E.
REAN DEGREE		TOTAL PROFI	555	L TOTAL ST	ATIC		
SC 06, th 52, 51 /0, CU, 54 8			757.0		***		
70 TH FF B7 TH CGV 10 78 GL	0027 .2200	. 1575 . 140 . 1571 . 1575 . 1401 . 1594				87 8722	7780 1.3284
16 2,39 55 8,82 44,14 52	1 1003 1	1287	9488	0000 0000	.0000 9626 88	8618 8578	,-
-3.3434 7.67 42.69	.0026 .2185	1144 ,0319	9586	9450-1-0000- 0000	-	8254 .8065	8500 1.37
	.57	Ī	. 4627	0000	: -		.7353
-5.92 -2.68 8.13 39.13	· 1000 · 8	* 0 4 2 4	. 9594	0000	.0348	•	1.0259 1.43
-2,65 12,44 36,88	0000	- 6850 ·	9156	1	2291	106 6372	10763 1.44
-, 79 -1.26 14,71 37,67 53	0000	-	. 0.55.0	0000 0000	•	6754 ,6230	.0683 1.44
15,16 42,23 56	.090	.1916 ,0684 ,0683	4528	. 0000 0000	.3313	. 55555* 55	1:0424 .1 . 42
	EFF-AD EFF-P COTAL	¥ 1					
-		SEC					
100-1 101-02 1.945 1.657	77.66 79.18 38.65						

Rotor Pressure Ratio = 1.7138

Po/Po Local	.9553
EFF-AD Adj.	77.48
P _o /P _o Inlet Adj.	1.633
W _{BLOW}	.00261
W _{BLEED} W _{TOTAL}	1

BLOW AT 48 PERCENT CHORD ONLY, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

	<	AIRFUIL AE	-	AERODYNAMIC SUMMARY	RY PRINT	- 1		į	٠.		Ì	7
(SPECIAL)	VM=2 v0=	_		2-5		* CZ * G	?	, SPE tO C	CUDE 10.	10.POINT #	11-1 11-2	7 7 1
C.FT/SEC FT/SEC FT/	EC F7/5	1.8	EGREE D	H 8	DEGREE D	~ ~	TYSEC F	1/5EC F	FT/SEC F	FT/54C F	TZSEC F	17 SE
21,008 21,761 1030,0 855,4 776,0	152.5 677	3-10.5	L.	4.7.4	73.64	-53,05	F-2+8-	1418.6	-239-7-	1133.	1017.01	106901
1 21,589 22,432 991,6 828,3 755,3		-	40,37	-5.8 l	28.04	54,83	856,8	1431.0	۲.	-1169.6	1045.1	1085.9
23,314 23,902 925,3 777,9 726,5	į	1.06-1	38 27	. 6.67	37,40	58,23	9.5	7		•	1126.6	115/1
25,601.25,893 908,7 760,7 731,1	756,4 539	, e00.4	36,43	,0°0.	43,73	60,43	1012,2	•	۲.	-1333.8	1239,3	1253,5
27,818 27,902 838,1 679,5 693,5	ĺ	-	34,14	-8 54	51.61	91.59	1117.8	1599.7	•	9.1511	1346.7	1350.7
29,408 29,382 837,7 650,9 682,8		. 1 - 1.	35,41	-6.28	53,96	95.99	1160.5	1627.8	ູ•	3-1473.7	1423.6	1422,
29 856 822 6 631 2 855 6 30 293 802 9 572 5 627 6	569 9 500	6 .54.3	37 - 5	5 50	55,43	69.46	1155.6	1626.2	970.2-1	1521,2	1448	2 9 9 4 1
					;				· .	: : •		· ·
INCH DEV TURN CAMBER O	GA-B D-FA	MEGA"B D"FAC OMEGA"B LOSS"P LOSS"P	L055-P	L0557p			٠	EFF - P	ī	7_U	X	7 . H
DEGREE DEGREE DEGREE DEGREE SH		!	TOTAL	PROFILE	Pol T	TOTAL T	TOTALS	STATIC				. '
.05 2.97 12°58 46°22 55°87	•	•	•0295	.0279	.9485	.0000	.0000	.7211	• 9366	1884.	1351	1.2049
-,20 2,73 10,70 45,85 53,84	•		•0256	1 6 20 .	6856	0000.	00000	17009	8937	.7297		1.2101
2,91 9,17 46,19 52,47	•	3535 .0746		.0177	.9712	0000	• 0000	.6210	. 8592	.7059	.7478	1,2195
20 2.81 8.54 44.94 50.66 .	•	i	1	.0101	.9850	0000	0000	. 8777	8001	1199	.7970	1.247
. 29 2,85 9,96 42,50 49,58	•	3710 .0599	•	.0152	.9801	0000	0000.	0059	.7787	.6436	.8756	1.2776
-1.61 1.63 8.90 42.69 49.87	1	•	.0165	.0150	4884	0000	00000	. 6929	7162	.5730	.9636.	1,3490
1 3,56 13,69 41,69 52,11 .	•	•	.0305	.0285	.9748	0000	.0000	.7899	.7095	.5426	.9853	1.3569
5,49 5,16 16,55 42,08 53,71	•	ľ	.0278	.0253	. 9783	0000	0000	8176	6431		9758	1816.1
4,67 6,31 18,18 44,08 56,06	.0073 .53	5367 ,1389	6640	.0472	.9634	0000	0000	1214	6737	9174.	.9723	1,338
Ŀ	0 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	14/17										
I INCET INCET INCET IN	INCET	LBH/SEC										
11095 180.46 1.2151 1.7605 81.	1.48 82.88	36.81										
•		-										
Rotor Pressure Ratio = 1.7997												
				WBLEED	•	WBLOW	~	P./P.	•	EFF-AD	0	P. 0/0
				WTOTAL		WTOTAL	Ą	Inlet Adj.		Adj.		Local
				ı		.00260		1.756		81.28		9776

BLOW AT 48 PERCENT CHORD ONLY, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

2		STATOR	STATOR ANGLES					ABRF	JIL AER	DOYNAMI	C SUMMA	AIRFOIL AERODYNAMIC SUMMARY PRINT	-	,		19:55:54	•	JULY 2	20,197
FINSEC FT/SEC FT	Z	SA ENG	1SH DIA-2		_	1 E X	VM.2	1 - 0 A	V0-2	i	8-2	91	RUN 1		V-2	==		K 1 - 1	U-2
101	SPAN	Z	Z.	FTISEC	FTZEC	FT/SECT	FYZEC F	T/SEC.F	77 SEC-01	EGREE"D	EGREE-D	EGREE-D	EGREE-F	1/SEC-4	FT/SEC-1	7.1/SEC-F	7/SEC-F	-1/5EC-F	17566
Z2 432 96.5 715.2 715.	ø 9	20 40	21.48		5.8//	737.7	1.1.1	741.4	1.00		7.00	0000	7		1940				
1 23.902 902.4 685.5 664.1 688.9 610.9 -66.9 42.617.25 37.85 61.25 841.1 1417.1 -516.1.1242.2-1127.0-115 1 25.893 895.3 700.2 670.5 670.5 670.5 670.5 593.0 40.85 61.25 841.1 727.8 140.5 -51317.0 1227.4 6 125 2 5.893 895.3 700.2 670.5 670.5 670.5 670.5 170.5 170.5 174.8 6 174.8 6 175.8 140.5 174.8 6 175.8 170.5 174.8 6 175.8 170.5	5	21.00			2.84	7,10,7	1.1	0.999	97.5	43.56	7.79	28.25	58.91	7967	1380.2	376.9	1181.9	9.6 101	1084
25.893 895.3 700.2 670.5 697.2 593.4 -65.3 91.51 -5.35 91.85 62.11 929.6 1990.2 -644.2-1317.0 1237.6 125.97 125.893 895.3 700.2 62.8 64.8 64.8 10.8 64.8 10.8 64.8 10.8 64.8 10.8 64.8 10.8 6.8 10.8 10.8 10.8 10.8 10.8 10.8 10.8 10	8	23.2	21.90	2 902	- 687	444	6.189	-610	-0.96	-42.61	7 . 25	37.85	-61.23-	- 8 41 . 1 -	-1417.1		-1242.2-	1127.0-	1155.
27,902 869,5 661,2 664,9 656,0 544,7 -82,8 -39,32 7,19 50,24 65,37 1040,5 1574,8 -800,1-1131,6 1344,7 134 29,502 863,4 645,7 653,8 644,2 53,9 553,9 554,10 78 51,60 664,6 1078,5 1610,5 -857,7 1470,4 1421,6 142 129,502 863,4 645,7 653,8 644,2 253,9 553,9 554,10 60,01 1074,7 1619,6 -864,6 1147,7 1470,4 1421,6 142 230,293 844,6 501,9 610,1 579,8 584,1 -47,6 43,75 -44,74 55,40 69,01 1074,7 1619,6 -864,6 1512,0 1468,7 146 EGREE DEGREE DEGREE SHOCK ESA 13,74 47,74 55,87 0114 660,4 1440 0375 0338 9468 0000 0000 0000 0000 0000 0000 0000 0	8	25.60	25.89	3 895.3	700.2	670.5	697.2	593.4	-65,3	11.51	5.35	43,85	62.11	9.824	1490.2	-644.2-	1317.0	1237.6	1251.7
29,382 863,4 645,7 653,8 643,2 563,956,1 40,784,98 52,68 66,46 10,76,5 1610,5657,7 1476,4 1421,6 1422,7 29,856 855,47 652,7 6010 622,7 578,456,1 40,784,74 55,40 657 1003,4667,71975,51446,1 147,2 12,5	2	27.81	27.90	5 658 - 2		6 499	_D.959	-S44 7-	82.8 ···	39.32	- 19 -	50.24	. 65,37	1040.5	-1574.8	-800.1-	. 9 . 16 . 1 .	1344.7	1348 B
130,293 844,6 501,7 630,0 622,7 578,4 134,2 43,7 55,40 69,01 1074,7 1619,6 1684,6 1512,0 1468,7 146 1468,7 146 1468,7 146 1468,7 146 1468,7 1468	2	29.40	29.38	2 863,4	645.7	653,8	643.2	563.9	-56.1	40,78	4.98	52,68	94.99	1078.5	1610,5	-857.7-	4476.4	1421.6	1420.3
INCH DEV TURN CAMBER OHEGA-B LOSS-P LOSS-P PO2, EFF-AD EFF-P H-1 N-2 N+-1 N+ DEGREE DEGREE EFFE FOR SHOCK A 43,75 .44,74 55,40 69,01 1074,7 1619,6 .884,6-1512,0 1468,7 146 DEGREE DEGREE FOR SHOCK A 43,7 1807 .0450 .0420 .9248 .0000 .0000 .6930 .9765 .6559 .6978 1.11 DEGREE DEGREE FOR SHOCK A 43,7 1807 .0450 .0420 .9248 .0000 .0000 .0974 .9761 .9762 .6988 1.11 S 29 9,49 49 61 53,84 .0116 .9453 .0918 .9760 .0000 .0000 .7741 .9755 .6724 .111 S 29 9,49 49 61 53,84 .0116 .9422 .0430 .9787 .0000 .0000 .9845 .7741 .9755 .7214 .111 S 29 9,49 49 61 53,84 .0116 .9422 .0688 .0210 .0113 .9780 .0000 .0000 .9853 .7285 .7214 .111 T 7 17 7 97 49 66 50.67 .0239 .9453 .0031 .0249 .9791 .0000 .0000 .9853 .7285 .7214 .111 T 7 18 10.67 46.86 45.69 53.82 .0345 .5255 .1180 .0419 .0254 .0000 .0000 .0000 .9853 .7285 .9893 .9821 .111 CORR WCORR TO/TO PO/PO EFF-P WC/Al NLET INLET INLET INLET INLET INLET INLET EM/SEC RPM LBM/SEC	8	29.91	29.85	\$ 558-1	6237	630.0	-622-7-	-578	-34-2	-95:21	-3-13-	-54:02	-67-15-	•	-1603.4-		-477.5-	14444	P * * * * * *
INCH DEV TURN CAMDER OHEGA-B	8	30,38	30.29		5.81.9	610.1	579,8	584.1	9.47.	43,75	4.74	55,40		1074,7	1619.6	-884.6-	1512,0	1468.7	1464.
DEGREE DEGREE DEGREE SHOCK S. 64 13.74 47.74 55.87 .0122 .4377 .1807 .0150 .0120 .0120 .0200 .0120 .0211 .0539 .0438 1.11 S. 64 13.74 47.74 55.87 .0112 .0122 .0137 .1807 .01450 .0220 .0000 .0000 .0000 .0430 .0436 .		INCS.		0Ev	TURN	-AMRER O	HEGA-B	D-FAC OF	1EGA-8 L	1 4-SSO.	4-880.		Eff-p E	FF-AD	EFF-P	1-k	H-2	1 - · H	H - 2
5.29 9.49 49.61 53.04 .0122 .4377 .1807 .0450 .0420 .9248 .0000 .6914 .9101 .6539 .6786 1.11	M	EGREE	2	DEGRE	DEGREE	SEGREE S	HOCK		1	TAL P	ROFILE.	:	DIAL T	OTAL "S	TATIC"				!
5.29 9.49 49 61 53,84 0116 4553 1807 0459 0430 9768 0000 0000 6536 6558 6858 1618 1618 6608 7,10 51,35 52,37 0141 46.0375 0338 99468 0000 0000 0000 8454 7741 5575 7741 5741 5	-	7.2	9	4 13.74	47.74	55.87	.0122	.4377	.1807	.0450	.0420	.7248	.0000	• 0000	•	1016	.6539	9849	
6.08 7.10 51,35 52.37 .0141 .4604 .1446 .0375 .0338 .9468 .0000 .7451 .8367 .6035 . 7.17 7.97 .49.06 -50.67 .0209 .4533 .0810 .0226 .0168 .9735 .0000 .0000 .8454 .7741 .5755 . 7.18 7.19 10.67 46.86 49.554 .0316 .4422 .0688 .0210 .0113 .9780 .0000 .8653 .7265 .5833 .8780 .0000 .0000 .8535 .7265 .5489 .0000 .0000 .8526 .0273 .5023 .0278 .0279 .0000 .0000 .8683 .7285 .5489 .0000 .0000 .8658 .0278 .0278 .0278 .0278 .0279 .0000 .0000 .8026 .7247 .5302 .0000 .0000 .0000 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .0000 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .0000 .0000 .0000 .7271 .7018 .4720 .00000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .00000 .0000 .00	5	2.36	l	•	19.64	53,04	-0110	4553	1807	0486	0430	9267	0000.	0000	.0630	8765	- 6 2 5 8 -	- 6724-	1.1.10
7 17 7 97 49 06 50.67 0209 4533 0810 0226 0168 9735 0000 8454 7741 5755 79 79 10 00 0 0000 8454 7741 5755 79 10 00 00 00 00 00 00 00 00 00 00 00 00	2	7	•	7	51,35	52.37	.0141	4094	91410	.0375	.0338	9446	0000	0000	1542	.8367	.6035	.6888	1.1580
7.98 10.67 46.86 49.54 .0316 .4422 .0688 .0210 .0113 .9780 .0000 .8535 .7623 .5833 .0690 10.27 46.82 49.54 .0316 .4724 .0701 .0231 .0152 .9791 .0000 .0000 .8583 .7285 .5489 .0000 .0000 .0000 .8583 .7285 .5489 .0000 .0000 .0000 .8026 .7247 .5302 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .7271 .0000 .0000 .7271 .7271 .7201 .0000 .0000 .7271 .7271 .7201 .0000 .0000 .7271 .7271 .7201 .1200 .0000 .0000 .7271 .7271 .7201 .0000 .0000 .7271 .7271 .7201 .0000 .0000 .7271 .7271 .7201 .0000 .0000 .7271 .7271 .7201 .0000 .0000 .7271 .7271 .7201 .0000 .0000 .7271 .7271 .7201 .0000 .0000 .7271 .7271 .7201 .0000 .0000 .7271 .7271 .7201 .0000 .0000 .7271 .7271 .7201 .0000 .0000 .7271 .7271 .7201 .0000 .0000 .7271 .7271 .7201 .0000 .0000 .0000 .7271 .7271 .7201 .0000 .0000 .0000 .7271 .7271 .7201 .7201 .0000 .0000 .0000 .7271 .7271 .7201 .7201 .0000 .0000 .0000 .7271 .7271 .7201 .0000 .0000 .0000 .7271 .7271 .7201 .0000 .0000 .0000 .7271 .7271 .7201 .0000 .0000 .0000 .7271 .7271 .7201 .0000 .0000 .7271 .7271 .7271 .7201 .0000 .0000 .7271 .	8	-		7 -	49 06	- 50.67	. 020	4533	0160	.0220	. 8910.	9735 -		.0000	. +S+8 ·	1622	5275	7214-	1.1864
6,90 10,29 46,52 49,90 0240 4724 0701 0231 0152 9791 0000 0000 8583 7285 -5489 -8 8,74 14,92 45,76 52,02 0273 5033 1008 0351 0249 9702 0000 0000 0000 8026 7247 5302 0044 18,92 45,76 52,02 0273 5033 1008 00351 0249 9702 0000 0000 0000 0000 0000 0000 000	2	8	4.9	9 10.67	46.06	49.54	0316	4422	8890	0210	.0113	.9780	.0000	0000	96535	.7623	.5833	. 7916	1.2413
8 74 14.92 45.76 52.02 .0293 .5033 .1008 .0351 .0249 .9702 .0000 .0000 .8026 .7247 .5302 .0044 18.94 46.92 .0000 .0000 .0000 .7247 .5302 .0044 18.94 48.69 56.07 .0347 .5813 .1672 .0601 .0476 .9531 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .0000 .0000 .0000 .7271 .7018 .4720 .0000 .0000 .0000 .0000 .0000 .0000 .7271 .7018 .4720 .0000 .	2	3.6)	6	1-10.29	46.57	- 49 9 A	-024U	47.74	. 0701		0152	- 626		0000 -	- 68583	7285	- \$845 -	48827	1,3074
0.444 0.46 45.67 53.82 0.345 5.556 1180 0.0417 0.296 9660 0.0000 7.807 7.306 5.008 1.40 18.94 48.49 56.07 0.347 5.813 1.672 0.0476 0.953 0.0000 0.7271 0.7018 0.4720	2	0	8,7	14.92	45.76	52.02	.0293	5033	1008	0351	.0249	9702	0000	0000	9000	7247	.5302	9088	1.3225
1,40 18,94 48,49 56.07 .0347 .5813 .1672 .0601 .0476 .9531 .0000 .0000 .7271 .7018 .4720 . IR WCORR TO/TO PO/PO EFF-AD EFF-P WC1/Al IT INLET INLET INLET INLET INLET SETT	8	25.01	b 0	10.46	.69 Sh	53.82	-2945-	5256	1180	-61.50	-0296-	0996	-0000	-0000	1004-	-7136-	- 5009	-8449	1:3082
IR #CORR TO/TO PO/PO EFF-AD EFF-P IT INLET INLET INLET INLET INLET INLET INLET INLET INLET S	8	6	F	18,94	48,49	26.07	.0347	5813	1672	1090	0476	9531	0000	0000	,7271	1019	.4720	86.48	1.3137
T INLET INLET INLET INLET INLET INLET S S S		2	CORR	T TEORE	0/T0 P	1/P0 EF	6 - AD	1-P WC1/	14.				Í	1					
I LBH/SEC 8 8 5		1	NLET		N_ET_T	VIET TIN	127	LET LBM	SEC										
		ļ	_	3H/SEC			*	50.	-										

Rotor Pressure Ratio = 1.9269

BLOW AT 48 PERCENT CHORD ONLY, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

8	A I A	AIRFUIL AERODINAMIC SUMMARY)n	- !	- 1			A LUC A LUCA			JULY 41,1771
SA ENGLISH (SPECIAL) DIA-1 DIA-2 V-1 V-2 V	1 VM-2 VO-1			H	B - 2	7.	1 4-2	5	•	?	27
FT/SEC FT/SEC FT/	FT/SEC_FT/SEC	FT/SEC DE	REE DE	EGREE	DEGREE FT	SECT	FT/SEC FT/SEC	T/SEC_FT/SEC_FT/SEC_	1	/SEC FT	T/54C
benez hannol tobel z tobecz s	7 / 11 / 102	0.0	- 1		22.4	- C	7 7 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8	2.53	1		
21.589 22.432 970.8 688.7	680.9 683.8 692.0	8	45.47 .6.83	27.4		767.9	353.2	353.0-1		-	1005.7
884.6 633.8	.3 628.3	-83.2	:	38,6	63.13	781.3	1390.2	-487.8-1		-	150.9
25,601 25,893 880,5 657,3	.3 653,3	-72.4	45,30 -6,3	44.7	63.77	71.6	1477.9	613,2	~		1253,3
27.818 27.902 872.3 643.9	.6 639.4	-76.5		149.6	98+59	78.1	1563.8	745.9	0	•	350.5-
29,408 29,382 897,5 650,4	.2 647,8 630.	-58.0	Ş	2 51.1	66,36	18.9	~	-143.4-1	_	_	422,1
30,293 884,0 607,3	6 606.0 651	39.6			•	1014.0	1615.1	1002.9.1484 6 _819.1_1505		1470.51	1466.2
	<u>'</u>			•		•					
INCS INCH DEV TURN CAMBER	BER ONEGA-B D-FAC OMEGA-B LOSS-P	OMEGA-B LO	SS-P_L055-P	P02/	EFF-P E	EFF.AD	EFF-P		H-2		H 2
DEGREE DEGREE DEGREE DEGREE DE		101	AL PROFI	5	TOTAL	OTAL S	7 1 1 7				•
4 44 7 35 12.92 50.29	2010	2028	0505	19100	0000	0000	0 4	2002	070	0150	101
30.17 50.27 50.38		0.02.				0000	000		0, 6	0.00	766.
00,24 10.0 24.7	50.67 .0413 .45113	1032	9120 1810	16 .9625	0000	0000	1664	1552	. 9525	6.00	1528
8 64 11.77 9.70 51 61	9750 #5	741				0000	7859	7440	5424	7355	2195
7.86 11.10 10.67 50.34	1	576	•		•	0000	7108	7327	. 2 8 3 ···	1 6217	2630
12.17 12.48 14.77 49.70	. 6190. 00	.2106	•	٠.	•	0000	# L79°	1441	5278	_	,3111
31 13.98 18.07 49.72	5. 1890. 5	. 2276	0007 080	0565 9306	•	0000	. 6089	2014	-66155	19393	3028
13,65 15,10 20.00 51,15	. 0705	.2590	₹,	,0679 ,9230	0000	0000		,7283	4673	8357	3020
NCORR WCORR TO/TO PO/PO	EFF"AD EFF"INLET	#C1/A1									
LBM/SEC 174,58 1,255	77.92.79	SQFT 32.51									
		,									
Rotor Pressure Ratio = 1,9981			WBL	WBLEED	WBLOW	>	9/°		EFF.AD	Δ.	P. /P
			WTOTAL	TAL	WTOTAL	,	Inlet Adj.		Adj.		Local
			1		.00257		1.884		80.07	o.	9588

BLOW AT 48 PERCENT CHORD ONLY, STATOR BLADE ELEMENT PERFOR-MANCE AND DESIGN DATA

	AIRFOIL AERODYNAMIC SUMMARY PRINT		12;00;49 94;00;10;00;49	3	JULY 21,1971
A ENGLISH (SPECIAL) OIA-1 DIA-2 V-1 V-2 VH-1 VH-2 VO-1 VO-2 OIA-1 DIA-2 V-1 V-2 VH-1 VH-2 VO-1 VO-2		8 - 8 - 8 - 8 - 8 - 8 - 8 - 8 - 8 - 8 -	V*=2 VO*=1 1/50'F1/VE	101 2 001 101 2 001 1755 81755	0-7
18 18 18 18 18 18 18 18 18 18 18 18 18 1	-4.02 18.0	56.85	736-6 1302-0 -228-1-1090-1 987-8 1040-	10901 987	10+01
10 -21.008 21.961 1000.9 685.4 699.4 699.4 716.0 -63.9	5.37	7 59.80 761.8	1317, 9-300, 6-1126, 8	,	8 10.62 T
22,432 761,6 659,0 670,8 653,6 687,0 -83,8					
611.8 587.1 605.8 643.3 ±85.0	46 44 17 43 45 25	9 4 9 4	9,909 6,4741	-405.U-1241.U 1129. -606.6-1335.U 1239.	
2 10 1 1 2 10 10 10 10 10 10 10 10 10 10 10 10 10	7 4 7	15 94	_	1346	1350
27,702 661,6 626,7 607,6 629,8 645,7 471,3	9	67.13	777	.3 1423	-
29 9 4 7 29 856 885 5 628 4 589 6 626 0 660 6 54 0	-4.92	67,33		7.10	5641
30.382 30.293 875.2 606.5 566.6 604.3	24:42		1634.0 -803.6-1510.	.0,41 1.0151-	2.001 5
CH DEV TURN TAMBER OMEGA"B"D"FAC OMEGA"B		EFF"P EFF"AD	H d		H 2
E DEGRÉE DEGREE DEGREE SHOCK		TOTAL TOTAL			-
" 4,95 "7,87 12,38 51,35 55,87 ",019 [50022130 "	30 0482	0000 0000		0.45	95-00-1 F
4.31 7.24 10.07 51.04 53.84 .0179 .5107 .2151	.0502	0000	0/90 00/00	•	
5,18 8,12 7,56 53,11 52,37 ,0227 ,5220 ,1872		0000			
9.05 12.09 7.24 55.60 50.67 .0471 .5303 .0708		0000 0000		2025	
0.87 5.90 40.90 10.00 10.00 00			7899 .7238	5139	. –
. 9895 6080 60°65 01°65 65°61 88 5186°11	0331		1	5123	П
577 53,95 16,71 53,17 53,87 ,0896 ,577	.0326	0000	•	. 5053	_
15,88 17,23 18,76 54,57	,0723 ,0387 ,941	0000° 0000° 5	.6730 .7187	. 4853 8072	2.1.3074
1 00/00 01/01 0800m					
INLET INLET INLET INLET					
PH LBH/SEC 8 8 920 170.80 1.9205 79.15 80.97					
Rotor Pressure Ratio = 2.0146					
	;				
	WBLEED	WBLOW	0/6 0/0	EFF-AD	9/°
	WTOTAL	W _{TOTAL}	Inlet Adj.	Adj.	Local
	i	.00278	1.915	78.90	.9513

BLOW AT 18 PERCENT CHORD ONLY, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

-6-000-6-	2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
JULY 20, 1971 J. P. P. C. S. C. C. C. C. C. C. C. C. C. C. C. C. C.	2
4 82 4 8 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	20 0022000
44225 44225 44225 44225 44225	# 00 00 00 00 00 00 00 00 00 00 00 00 00
N 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 42 40 40 40 40 40 40 40 40 40 40 40 40 40
100 100 100 100 100 100 100 100 100 100	
20 100 4 4 4 6 6 4 4 4 6 6 6 6 6 6 6 6 6 6 6	
19:51:56 VO = 1 V V = 2 F 7/5E F / V = 2 F 7/5E F / V = 2 F 7/5E F / V = 2 F 7/5E F / V = 2 F 7/5E F V =	
0 0 0 0 H P P P P P P P P P P P P P P P	7 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
A + 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	# F F F F F F F F F F F F F F F F F F F
	4 4 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
7 7 5 5 6 1 3 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
N N N N N N N N N N N N N N N N N N N	00000000
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1000000000
R I N I N I N I N I N I N I N I N I N I	20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	44 46 40 40 40 40 40 40 40 40 40 40 40 40 40
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7	E DEGREE DEGREE GEREE GEREE B 13.05 SO 77 SS 89 20 T 10.30 SO 77 SS 89 20 T 10.30 SO 77 SS 89 20 T 10.30 SO 77 SS 89 20 T 10.30 SS 89 20 T 10.30 SS 89 20 T 10.30 SS 89 20 T 10.30 T 10.20 T 1
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P_o/P_o Local

EFF-AD Adj.

P_o/P_o Intet Adj.

W_{BLOW}

WBLEED WTOTAL

Rotor Pressure Ratio = 2.0146

.9513

79.09

1.917

.00307

ı

	STATOR ANGLES	ANGLES					AIRF	OIL AER	ODYNAMI	AIRFOIL AERODYNAMIC SUMMARY PRINT	RY PRIN	_		_	08:55:80	-	4UGUST 24,197	16616
	MASA ENGLISH	I SH	ISH (SPECIAL)									* NOR	38,	_	CODE 10.	_	1 1, P.A.	1,PAGE 36.02
	01A-1	Z-Y 0	1.	٧-2	V M = 1	VH-2	1-01	V0-2	1.8	8-2	1 - 18	8.2	VF-I	v v - 2	1-101	. Z=40Å		2=0
KSPAN	2	2	FT/SEC	1/SEC	FT/SEC	FT/SEC P	FT/SEC F	T/SEC D	EGREE D	EGREE D	EGREE D	EGREE F	T/SEC F	1/SEC	FIVSEC DEGREE DEGREE DEGREE FIVSEC FIVSEC FIVSEC FIVSEC	T/SEC !	T/SEC	FT/SEC
6	104.02	686.12	1.8501 V	831.5	1.9//	1.0EB	720.0	-38 · 4	58.25	₽8.5-	44.81	25.37	820.9	1380.8	-767 D.	0-101-0	1.484	6.4601
2	21,008 2	21.961	2	800 B	750.4	796.2	681.0	.83.7	42,22	-6.02	24.07	55.19	822,2	1395.5	-335.0-1145	.1145.8	1016.0	1062,1
£	21.589 2	22,432	2 972.9	177.2	721.5	4.697	9.259	-106.7	42.13	-7. A.	28,46	57,13	821.6	1418,8	391.5	9.1411.	1.4401	1084.9
8	23,314	23,902	•	•	7.007	736.6	593.5	9.46-	40.26	-7.32	37,31	59.50	881.0	1451.4	-534,1-	-1250.6	1127,5	1156.0
8	109.52	25.89	3 404 8	739.7	7.807	736.2	570.7	-7 L.6	38.86	-5.56	13,30	26.09	473.3	4.4151	-667.5	8.6261-5	1238.2	1252.3
8	27,818	~	845.0	6.499	677.0	9.659	505.7	.83.5	36,75	-7.22	51.09	65.28	1078.9	1577.6	-839.7	-1432,9	1345.4	1348.4
8	805.42	24.382	L	6	4.999	637.0	513	8.15.	75°45	4.64	53.75	10.00	1:22:1	Lande	1-0-404	9.2411	1.22	D. 12 . 1
8	59,914	~		628	9.849	627.5	527.4	.35.8	39,12	-3.26	54,80	67,02	1125,1	1607,3	-919.3-	3-1479.8	1446.7	1443.9
2	30,382	30,382 30,293		1.509	632.8	603.2	535,1	44.4	40,22	4.54	\$5.89	68,26	68.26 1128,5 1628,	1628.7	-934.3.	3-1512.8	1469 .	1465,1
		!			i								+	1	-	6 -		6.7
		¥ Z	۰ ۲			OMEGATB	OMEGATE DEFAC OMEGATE LUSSTP LUSSTP	Mr. GA B	1.055°P	1.055°p		۵.	_		! E	y L	E	
& SPAN	MSPAN DEGREE	DEGREE	DEGRÉE	DEGREE		SHOCK		-	TOTAL P	PROFILE	100	TOTAL T	TOTAL S	STATIC				
9	.52	F.			55,87	0,00	3870	1563	0384	.0372	4335	0000	0000	6937	\$234	1,01	B/1/*	1.1532
2	96.	3.90	9.42	48,24	53.84	9,000	.3993	1269	.0323	.0303	5446	0000	.0000	4542	8794	•	.7152	1,1818
2	1.72	49.4	50.7	50.02	52,42	\$ 00°	4026	0879	.0228	.0202	4673	0000.	0000	bb 8 •	8420	. 6575	1817.	1,2001
Ř	1.83	4,83	3 7.90		50.66	.0127	3997	.0530	9,10.	.0112	.9820	.0000	.0000	8744	. 7910	,6268	,7623	1,2250
3	2.17	5,30	10.47	44.42	49.56	.0191	4021	.0632	.0193	PE 10.	1616	0000	0000	8533	•	.6210	4357	1,2719
8	1.05	4.29	10,24	43.48	49,89	.0117	4439	.0582	1610	.0153	.9830	.0000	0000	.8780	.7191	2955.	,9226	1.3197
8	5.32	9.5	15.29	42,25	52.06	\$210	15/4	6980.	.050	.0260	15/4	0000	0000	9608	1108	56250	6256	1,3293
8	7.14	7.01	1 18,32	42,38	53,81	9410.	.4879	9980.	.0307	.0256	.9756	.0000	.0000	6618.	7030		.9464	1,3246
26	46.9	7.87	19,13	91.44	26.06	hh10.	,5238	. 1064	.0340	.0338	10/6	0000	0000	1008	2469.	596h.	0956	1,3359
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	=	****	180.83 1.4231 1.6111	1 1677	-	84010	1	?										

Rotor Pressure Ratio = 1,8594

P _o /P _o Local	.9745
EFF.AD Adj.	79.57
P _o /P _o Inlet Adj.	1.8111
W _{BLOW} W _{TOTAL}	ı
W _{BLEED} W _{TOTAL}	.01165

STAI	STATOR ANGLES	S				- V	AIRFOIL AERODYNAMIC SUMMARY PRIN	RODYNAMI	CSUMMA	RY PRI	<u>_</u>	. ,		16:95:0	₹	August 2	24,1971
NASA ENGI	ENGL I SH	(SeEct)	1, 1								RUN	381	SPEED C	CODE 10.	INIO	2 . P. A.	PAGE 36.02
1-V10	- V 1 Q	2	, .	VM-1		V0-1	2 0 Å	- 8 -	B-2	1.8	8 - 2	- · · · · · · · · · · · · · · · · · · ·	, V = 2	¥0,*	2-10/	- 1	.y-2
S SPAN IN	2		4,	4	1 3 E C	5,75	7,35,7	DERKELD	DEGREE	10 Kg	PEGMI E	1,55c F	1875	3,300,	25.0		֓֞֝֝֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֟֝֓֓֓֟֝֓֓֓֓֓֟֝֓֓֓֟֝֓
5 20.	2 1 . 1	_	6322		T	/2/	.39.5	43,05	-2.64	16.43	52.20	0.12.	1302,	-25, 5-	0, 01	1.	1037,3
10 21,	1,008 21,7	761 1022	.3 802,8	8 757	œ	686	2 .83.9	42.16	-6.02	23,53	55,13	827.0	1346 9	-327 Y	0 9	1016.0	1062.1
18 21.	589 22.4	32 979	3 776	726	692 6	959 +	2 -106.5	42.07	7,88	28.07	57,14	824 7	418.4	2387 9	11,11	1044.1	1084.9
30 23	314 23 9	02 012	4 732	1 69	3 726	595	5 . 93 3	40.74	7,32	17.58	59 83	8723	1 445	532 1	249 3	1127 5	1156
52 . 09 _	. 0	93 . 904	5 733	1 700	8 729	571	70.8	39.22	5,55	43,54	61,12	967.0	1,11,1	-666 2-	1323.1	1238.2	1252.3
70 27	27.9			2 675	8 66n 9	511	8 83.6	37,13	.7 22	50.93	65.23	1073 4	1578 2	833.5	433.0	1345 4	1349 4
88 29	408 29 3	82 846	3 640.	9	3 638	1 521.	8.15.	38.06	59. t-	53,50	15.99	1120.3	2 5091	-,000,-	8 2 2 4 1	1422,3	1421 0
90 29	914 29 85	56 841	6 630	49 9	2 629	536	4 .35.7	39,62	-3.24	54.54	66,95	1117.4	1609.0	-91071-	479.6	1446.7	1443.9
- 98 30.	362 30.2	293 831	1 600	4 628	1 598	544	3 -47,3	40.92		55,83		1118.2	1626.6	-925	1512,4	1469.4	1465.1
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- 		0 ^c v		Ù	3149140 8	N DIFAC	OME GALB	L055-P	L 055*P	, p 0 d	۵.	CFF = AD	4.1.2	!	, I	I	, ,
SPAN DEGREE	7	DEGRE	a	DEGREE	E SHOCK		TOTAL	TOTAL	PROFILE	104	TOTAL	TOTAL S	STATIC				
9	2	63 13,7	1.56 5/	70 55	8700, 78	391	1629	90,0	.0386	9301	.0000	.0000	6836	9301	.7072	.7180	1.1543
2	3	82 9	87	53	84 ,0082	403	1418	0360	0340	9428	0000	0000	7213	8879	6796	7,98	1,1824
15	1.67	19.	6 64 6	6 52.	44 .0102	407	1024	•	.0239	5196	0000	0000	7886	8479	,6567	7157	1 661 1
30	2,30 5,	30 7,9	0.84 0	, 5 ₀	şę	407	5 0548	.0153	*110°	9817	.0000	0000	8739	7853	.6172	7535	1.2179
50	2.53 5.	0.	. ++ 8	49	9	•		•	0117	800¢.	0000	0000	8644	77.25	6119	8295	1,2675
2	2 2 2 7	68 10.2	25 44.3	35 49 8	89 .0133	•			0148	9829	0000	0000	8772	7210	5567	9171	1,3,88
8	9 8/ 9	15.	42,	2.	90	3 ,4802	ľ	.0328	.0279	97.28	0000	0000	7970	551/°	.5297	0946	1,3277
8	7,66 7	52 18,3	34 42.	6 53	91 017	264	6 0 0 39	,0333	.0273	9733	0000	0000	, 8 ₀ 74	7068	5189	9387	1,3230
88	. B . PO.	6 6	13 45.4	95 9	9,10. 90	9465, 5	. 1214	•0436	.0373	5996	0000	0000	9186.	0469.	h! 64.	4357	1,3312
	NCORR	WCORR	T0/T0	00/00		EFF P W	WC1/A										
	INCT	INIET	INLET	INLET	INET	ь	AH/SEC										
	E:	LBM/SEG		a .		10	SOFI										
•	_	100.27		1,62/1 1,0134	91.0	03.0	0000										

Rotor Pressure Ratio = 1,8646

P _o /P _o Local	.9730
EFF-AD Adj.	79.58
P _o /P _o Inlet Adj.	1.8134
W _{BLOW} W _{TOTAL}	1
W _{BLEED} WTOTAL	.02169

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2	700
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7	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
0.00 V 2 V 2 V 3 V 3 V 3 V 3 V 4 V 4 V 4 V 4 V 4 V 4	,0380 ,0380
DE B 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.028 .038 .038
VH-Z VO-1 VO-2 B-1 B-2 P43 SEC FT/SEC FT/SEC DEGREE	0445
E	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
A 100 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	9 80
7 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1238 1238 141 17
A 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	112 07 135 07 156 12 126 12 126 12 126 12 135 57
A 170.00 000 000 1 0000 000 000 000 000 000	535 535 535 535 535 535 535 535 535 535
NU-0-NF-FB	0148 4812 1 0177 44935 6 6 6 0181
0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0148 0177 0181 0181 FF AD EF NLET IN 8
7/7	552.0 553.8 56.0 56.0 75
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	
7477 88.55 89.24 70.24 60.34 60.	42.9 45.59 45.55 70 772
7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	10/10 10/10 10/10 10/27
SPEC 1 1 1 1 1 1 1 1 1	15.30 19.13 4R T(17 1N
25	6,22 15,30 42 7,64 18,33 42 8,68 19,13 45 R WCORR TO/TO LBH/SEC 180,59 1,2272
NG C C C C C C C C C	
STATOR ANGLES SIANICISH 20,409 21,40 21,509 22,406 21,509 22,406 22,500 22,406 23,314 23,90 23,414 23,90 23,414 23,90 23,414 23,90 23,414 23,90 23,414 23,80 23,414 23,80 23,414 23,80 23,414 23,80 23,414 29,80 24,40 20,20 24,40 20,20 25,40 20,20 26,40 20,20 27,40 20,20 2	13 8 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
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STATOR ANGLES NASA ENGLISH SEAM IN 10 21 20 21 20 21 20 21 20 21 20 21 20 21 20 21 20 21 20 21 20 21 20 21 20 21 20 21 20 21 20 21 20 21 20 22 22 23 24 25 26 26 26 26 26 26 26 26 26	
	% & &
	. •

Rotor Pressure Ratio = 1.8691

Po/Po Local

EFF-AD

Adj.

P_o/P_o Inlet Adj.

WBLOW WTOTAL

WBLEED WTOTAL .9729

80.09

1.8175

.01938

(SPECIAL)	IC. SUHHARY PRINI	RUN B	12:56:36 45.SPEED CODE 70,POINT	OCTOBE	1,1771
A+2 V+1 V-2 VH+1 VH+2 V0-1 V0-2 B-1 PT/SEC FT/SEC FT/SEC FT/SEC DEGREE	Brel. E DEGREE	64EE FT/SEC	#1/5EC FI/5EC FI/5EC FI/5E		U=2 C FT/SEC
21,008 21,961 795.2 884,4 649,1 868.0 459,3 -169.2	35.27 -11.03 21.17	1 5.969 24.94	-251.3]	742.8
16 21.589 427.1 = 183.3 3 4.17 3 30 428.8 839.0 427.1 = 183.3 34.17 30 23.314 23.902 695.2 793.0 602.4 769.7 347.0 = 190.8 29.93	-12.36 25.71	52.39 747.2	262.0 -303.1	-948.1 730.2	756.8
25.601, 25.893 644.2 732.0 561.3 709.2 277.5 -181.2	1	827.4.1	273.1 -588.5-1057.0	965	875.8
70 27,818 27,802 606,0 676,1 561,5 641,6 227,6 -213,1 22,06 85 29,408 27,408 27,408 59,408 29,408 29,408 59	-18,38 51,77 -18,71 54,63	60,98 908,0 1	323.0 -713.3-1156.9 339.8 -781.6-1197.4	197.4 994.7	943.8
5 5 78 4 6 2 6 1 5 3 6 7 5 9 3 0 2 1 5 6 - 2 0 0 . 9 3 5 5 8 9 5 5 9 9	-18.72		348.2 -796.3-1210.8 389.5 -809.8-1279.6	1011.8	1004.9
9 9 9			- I		
DEGREE DEGREE DEGREE DEGREE SHOCK	PROFILE POI TO	TOTAL TOTAL STA	STATIC		•
55,87 132 1962	0.158	1279-1-0000-0000-1876		.6268	-1981-
0, 10, 10, 10, 10, 10, 10, 10, 10, 10, 1	14/4 /200	.0000, 0000. 644,1 0000, 0000.	1546 6760	1750, 2000,	7071
30 -8.66 -5.66 5.66	•	1 0000 0000	•	.6692	1373
-11.298.15 49.59000008190463	1	.0000	i	!	1454
02.55 - 1.5 10.50 - 49.86 .0000 .1252 .0717 .0225	•	0000	1,2197 ,5382	#6070 .8136 I	1877
80 -9,91 -10,21 - 53,71 ,0000 1734 ,0958 .	. 0326	0000 0000	5477 .5115	5586 .8530	8707
-10a7a -9.13 - 56.05 .0000 .2344	ì	1 0000		Ī	-2353-
NCORR MCORR TO/IQ POZPO EFFEAD EFFE HC1/A1					
INLET INLET INLET INLET INLET INLET LBH/SEC					
135,65 1.0017 1,2495 80,46 81.06					
	WBLEED	WBLOW	6 0/6	EFF-AD	P./P.
	WTOTAL	WTOTAL	Inlet Adj.	Adj.	Local
Rotor Pressure Ratio = 1,2495	.03123	1	1.2495	78.38	.9856

SUCTION ONLY, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

STATOR ANGLES	A 1 R 5 0 1 E	AIREGIC AERODYNARIC SURHARY DRINI		12:57:54	2:57:59 OCTOBER 14.	1471
NASA ENGLISH (SPECIAL)			RUN E	45, SPEED CODE 70, POINT	DINT # 2. PAGE	36.02
SSPAN DIA-1 DIA-2 V-1	VN-1 VH-2 VO-1	Bell Bell Bell Bell Ben Ben Ben Ben Ben Ben Ben Ben Ben Ben	V ! - 1.	7	1.0	7.5
786.9	**	JOEC DEGREE DEGREE DEGREE . 17 31	7356	1/35C 71/35C 71	7 /3c(7 /3c(7 /	29.0
748.0	500.1 740.8 472.2	7 39.14 -11.28 22.52	1 4.828.4	-240.4	.892.7 712.7	
21.589 22.432 716.8	561.1	7	52.28 630.7.1	5 - 286 -	924.9 732.4 7	10.10
.314. 23.902 661.1		1.9 34.95 -14.86 37.24	56,22 681.0 1	185.9 -412.1 -	-985,7 790,9 8	1 Ú . B
١	6_520.7_608.9_320.4_167	7.6 31.60 15.40 44.44	59,78 .756,1-1	210.5 -5 48.0-1	i	78.4
70 27.818 27		1.5 29.07 -21.10 52.47	64,57 833,9 1	283,3 -661,5-1	0 943.7	4 è . 5
29.408 29.382 572.8	-	3-2 29.28 -21.48 -55.15	64.55 A74.3	142,1114,54016	20109 89204	22922
29.914 29,856 565.7			67,09 872,3 1	319.0 -724.6-i	214.9 1014.8 10	015.0
30.382_30.293_558.Z_535.1	1-473.2 497.9 296.2 -196	1.0 -32.02-21.49-57.18	-61486-874.0-1	321+1734.5-1	223,7-1030,7-10	1027.6
INCS ENCH DEV TURN CAMBER	ANARES ONECATE DIFFER	ONECARR DIFFE ONECARR 1055-8 1055-8			H-2 H-1	x 2
MSPAN DEGREE DEGREE DEGREE	DEGREE SHOCK	TOTAL PROFILE POI	TOTAL TOTAL ST			
	55.87 .0000 2125	12 0312 964	4	1832 6983	6936 5627 1	7570
10 -2,13 ,80	53.85 .0000 1995	.0893 .0224 .0224 .9771	1116.6 0000. 0000.	•	.6711 .5567 1	0306
	300001972	.060401549854	1 0000 0000	.9015 .6321	6512 . 5599 1	0379
-3.59	*2020 . 2024	.0120 .0120	0000	4686 S817	1 5509. 2409.	0150
-5,15	90000 2111	.0100 .0100	0000	3/21 . 5381	1 2587 , 6709 1.	0,07
-6.67	9992 0000 9	.0128 .0129 .	• 0000•	.9283 .5109	.5212 ,7392 1.	1751
-2,73	, .0000 .3179	0836 .0272 .0272 .9067	.0000 .0000	5552 5525	4921 .7632 1s	1205
-1.01 -1.18	53.77 .0000 .0558	.0732 .0242 .0242 .9867	· 0000 · 0000 ·	2735 ,4951	.1 ++97. 1644 1.	949
. = 1.86 = . 10	56.04	+0246 +0318 +0318 +7852	\$0.00 0.000 0.000 ·	-040¢4883-	1,1672 - 27642 1.	153%
#CORR TO/TO	PO/PO EFF-AD EFF-P MC1/Al	,				
INLET INLET INLET		١				
7775 128 44 1 0044 1 305e	1 305c 83 72 84 32 32 6.	1				
		WBLEED	WBLOW	P ₀ /P ₀	EFF-AD	P ₀ /P ₀
		WTOTAL	WTOTAL	Inlet Adj.	Adj.	Local
Rotor Pressure Ratio = 1.3201		.03456	ı	1.3055	80.43	.9894

2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	P _o /P _o Local	0686.
# PAGE 14, PAGE 14, PAGE 14, PAGE 17	EFF-AD Adj.	80.93
15.5FLEG COUE /J, POINT 1	P _o /P _o Inlet Adj.	1.3373
EGREE FT/SEC FT/SEC F 15.5/FLU C 15.5/31 594.9 1145.5 16.5/31 594.9 1145.5 16.5/31 594.9 1145.5 16.5/31 594.9 1149.5 16.5/43 70.2 1140.5 16.5/43 70.2 1140.5 16.5/43 70.2 1140.5 16.5/43 70.2 1140.5 16.5/43 70.2 1140.5 17.6/6 813.4 1248.3 17.6/6 813.4 1248.3 17.6/6 813.4 1248.3 17.6/6 813.4 1248.5 17.6/6 813.4	W _{BLOW} W _{TOTAL}	1
C	W _{BLEED} W _{TOTAL}	.03695
FT/StC FT/SEC FT/SEC DEGREE DE		
1-2 VD-1 VC-2 5EC FT/SE		
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		
EC FT/SEC	= 1.3528	
10 10 10 10 10 10 10 10 10 10 10 10 10 1	Rotor Pressure Ratio	
AASA Erich 15:1 SEPAN D1A-1 U1 10 21-508 2	Roto	

SUCTION ONLY, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

STATOR ANGLES ALBORNAL (SPECIAL)	_AIRFOIL AERODYNAMIC. SUHHARY, PHINT	HIN B 45° CPEED	13:00:31	oct.	JUER. 14.1971
A+2 V+1 V-2 VH=1 VH=2 V0=1 V0=2 FT/SEC FT/SEC FT/SEC	E DEGREE DEGREE	FT/5EC F	V0*-1	<u></u>	U.2 FT/SEC
21.961 717.7 648.4 519.6 629.6 495.1 -155.2		55.06 564.0	-218.4		
4 23,902 631,0 580,9	J.55 - 18.87 - 38.29	61.18 602.2	140.8 -373.2	-716.6 191.8 -499.5 791.8	9 1 1 8
25,601, 25,873, 580,9, 533,9, 447,5, 502,1, 370,4, 181,5	-19.87	670.4.	-1	649	879.4
29.192 568.8 500.9 428.4 420.9 373.0 e170.5	30.36 08.71 87.08		259.8 -625.0x1168.9 259.8 -625.0x1168.9	ŀ	997.9
29.856 \$61.3 490.1 416.3 460.8 376.4 =166.8 30.293 555.4 477.7 407.3 427.7 37.7 6 =211.0		763.2	1267.6 -634.5-1180.8	.5-1160.8 1016.0	1014.0
BECARE DEGREE DEGREE DEGREE DEGREE GROOK ANDER DEFAC ONEGA-6055-P-655-P-7027-EFF-P-EFF-AD EFF-P-514-P-	55-p-1055-p-p027-	TOTAL TOTAL STA		N=4	H - 2
8 4 80 1302 1302 1305	33 0332 764	00000	4229 6637	5888 4995	2673
10 2,38 5,31 5,31 53,85 ,0005 ,3254 ,1115	.0276	0000 0000	•	•	9627
3,13 6,07 52,54 ,0011 ,3216 ,0802	• 0203 0201 9825.	0000 0000	0209 8275	1564	9637
1,00° 9745, 9100° 7,000 000 000 000 000 000 000 000 000 0	• 0158	. 0000	6527 ,5516		1946
2 2 2 4 2 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2	• U 34 • U 24 • 7.7 Z 3.	•—	0,020	779C - Dear .	1.0644
8,51 8,95	0263	0000 0000		4318 6581	9 5 P D 4 L
53.77 .0082 .4709 .0924	. 0281	0000 0000	6313 .4849	.4215 .6603	1.0702
8492 10449 5404 40069 5224 41085	Ĭ	1	6116 47.63	-101010001-	1+1261-
-MCORR - #CORR - 10/10 - PO/PO - EFF-40-EFF-P - #C1/A1-					
T INLET INLET INLET					
7784, 116,64 1,1108 1,3558 82,05 82,80 29,86					
	i	3	9	((((•
	WBLEED	WBLOW	م'ہ م	EFF-AU	9,0
Rotor Pressure Ratio = 1,3745	TOTAL	"TOTAL	Adj.	ż	
	03930	i	1,3558	78.95	.9868

NASA ENGLISH (SPECIAL) ***SPAN_DIA-1_DIA-2_V-1 IN			:		1114		YUMO 1	ALKS OLD APRODUMABLE COMMAND FROM				25:10:61	3	. CCTUBER 14,1771	7,11
0 - 0	. ,		,						NOX:	5	451SPEED C	CODE 70, POINT	Polar	6 . P A G	6, PAGE 36.04
1N 1N 1N 20 21 489 21 008 21 961		V V N ** 1 V	¥.		V0-2	1.8	. 6-2		B'=2		V - Z	VO1. VO2		7.0	7=0
21.008 21.961		<u>.</u>	SEC	FT/SEC F	FT/SEC DEGREE	EGREE DE	DEGREE DE	DEGKEE DE	DEGREE F	FI/SEC F	TISEC F	FT/SEC FI/SEC FT/SEC		FI/SEC FI/SEC	. / SE C
21.008 21.961	438.7	500.0	615.9	534.2	162.0-	46.41-15.35	-15.35-	17.20	55.58	-533.4	1082.5	4.58.4	- 888-	683.0	727.6
CERC OF SIC	9		594.7	505.0	-163.1	45.62	-15.34	22.46	56.80	536.6		-208.3	8.804-	713.3	7.5.7
4.1.50 7. 66.136.	- 1	476.7	-	483.4	n162.7		1015.82	27.61	50.13	538.9	1086.6	-249.6	6. 424.4	733.0	751.7
23,902		452,6	517.3		-190.7	43,86	-20.24	36.19	65.69	576.7	. 3	-356.6-1002.2	1002.2	791.6	811.6
25,601.25,873	ļ	417.0	469.5	197.5	- 183.0		-21.30	48.51	66.15	629.9	1161.4	-471.9-1062	1.062.2	869.3	879.2
	485.1	410.4	451.9	. 7	-176.4		-21.32	53,28	40.84	686.6	1211.2	-550.4-1123.8	1123.8	9.44.6	4.7.4
29,408 29,382 565	472.2	181	419.9	1	171.B		21,13	56.65	69.19	497.0	1249.4	-582.Zel	1169.4	978.5	997.6
90 29.914 29.856 562.8 85 30.382 30.293 556.8	2.002	378.3	4.04 2.04 0.04	Φ,	-169.7	47.77	17 -21.34	57.72	69.64	708.4	1260.7	2.598.9-1183.5	9-1183.5	1015.7	7.610
	-							!			ì				
DEV	TURN	TURN CAMBER ONES	1EGA-B-C	*EAC DI	IEGA=B.L	ATB DEFAC ONEGATE LOSSTP-LOSSTP	- 1	P02/	EFF=P.EFF=AD EFF=P	FF-AD	EFF.P.	1-1	H . 2	1-14	H!-2
DEGREE DEGREE DEGREE	DEGREF D	DEGREE SI	SHOCK		, -	TOTAL P			TOTAL TOTAL	OTALS	STATIC				
		55.88	91004	1691	1381	7	0328	9658	agnge	ä	5 297	6494	15571	47.02	9256
10 4,35 7,28		53,85	.0020	,3662	1186	.0292	.0287	.9128	0000	0000	6916.	1619.	.5379	91240	6443
4,97	j	\$2,56	*0035	3670	. 0994	.0250	.0242	9787	0000	0000	26190	5947	5025	4737	9466
5.44		50.68	•000•	.4003	.0924	.0244	,0226	9888	0000	0000	2149.	5483	.4793	\$505.	50 p.6.
4.93 10.05		49.61	-01.47	4332	.0732	.0209	-0167	9.664	0000	0000	.0517	- 5016	4363	4844.	5500*1
8.19 11.43		49.87	.0258	4797	1901.	.0328	.0248	.9037	0000	0000	2549.	. 4933	.4177	5955	16.000
14465 15426	,	52.03	£ 40°	5289	1125	0412	4570	9801	-0000	0000	5769	18.71	4037	2009	1990
15,80 5,58		53.77	• 0505	21452	.1423	1 / 40 *	.0305	. 9789	0000	00000	5787	4836	.3982	96090	1.0762
96 _14 0 JS 15 0 B Z	1	56.04	• 0437	-5827	-2781-	0.470	-0110-	8787_	0000	-0000	-\$575¢	-47.79	-1913	-6102	-101,133
DIVOT SECON SECON		Po/PO FFF	-	1 6 5 5 - D W C 1 . A 1	141										
INLET		INLET INLET	, 	INLET LBH/SEC	/SEC										
DPM I BUILT				1											
110,23		,3675 7	19.00 79.91	9.1 27.9	96										
							×	WBLEED		WBLOW		9,0		EFF.AD	₽,
							Š	WTOTAL		WTOTAL	. 4	Inlet Adi		Adj.	Local
Rotor Pressure Ratio = 1.3933	33											•			

SUCTION ONLY, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

	AIRFOIL AERODYNAHIC SUHHARY PRINT	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	10:54:42	OCTOBER 26,19	1971
0 A=2 V=1 V=2 V	218	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \			4.),
20.409 21.489 1088 1 1109.2 025.4 1	2010	1 1 _ 6	-262,5-1159	- -	ه حل
1052.5 1074.5 811.7	52 -7.26 23.30	4/ 78 884 8 1022	5021-a 0cc- 2	•	
21,507 22,432 101/, 0 10/5,3 /76	50 6.53 27.49 69 35 38 47	47.57 697.0 1640.	415,1-1247	1 1048,8 1089	ه ّر د
501 25.893 873.2 930.1 738.4 918.2 4	26 - 9 9 9 46 45	56.86 1072.7 1679.	777 6-1406	4 1245,7 1259	! **
818 27,902 802,8 833,5 698	45 -11.01 53.82	61.62 1185.0 1721.	956 6-1514	6 1351 4 1355	տ
29,408 29,382 799,3 798,5 704,9 786,7 3		63,30 1266,3 1750.	-1051-4-1501-	7 1428 6. 1427	•
65 10 182 10 29 714 27 856 785.2 788.3 694.3 779.4 395.0 = 117.7 27.27.	77	63.57.1268.7.1751.	2=1068.2=1568. 7=1086.4=1593	1 1453.2 1450	- j -
			•	•	
INCH DEV TURN CAHBER ONEGA"B D"FAC ONEGA"B	p02/	<u>a</u>	H-1 H-2	N1 N2	~
DEGREE DEGREE DEGREE SHOCK	PROFILE POL	d	95.9	71.97	þ
0202° 4501° 0400° 40°45 10°04 44°01 02°1	7050 7750	44,4 0000, 0000,	996 576	· ·	
1,92 1,02 6,39 47,03 52,40 ,001 1,451	Ĭ.	1	89.18	7863	0655
-3.5556 4.87 45.24 50.67 .0016 .1455 .1299	0354	1.0000	6063	2 8460.1.	2.5
1101 8651 1100 09 65 57 17 78 9 10 11	.0303	.0000	7582	2 ,9319 1.	03
" " " 3 95 1.0 08 17 98 52 58 0000 2305 1964	010 1010 010	1	27, 7, 7, 7, 7, 7, 7, 7, 7, 7, 7, 7, 7, 7	2 1 0243	
0.001, 0.021, 0.000, 0.002, 0.000, 0.0	0.00	0000 0000	6760	1.5	
-3,05 -1,59 14,38 40,07 56,06 ,0000 ,2545 ,1927	•	.0000-5	•	5 1.0874 1.5055	
NCORR HCORR TO'TO PO'PO EFFTAD EFFTE WC1/A					
IN ET IN ET IN ET IN ET IN ET					
11134, 182,65 1,1894 1,6013 75,94 77,50 39,46					
	WBLEED	W _B OW	d/ d	EFF.AD	é
	WTOTAL	WTOTAL	Inlet		0,,0
Rotor Pressure Ratio = 1,6847		!	Adj.	•	
	.02472	ï	1.6013	73.95	.9517

	AIRFOIL AERODYNAMIC SUNMARY PRINT	Y PRINT			10,55,58		OCTOBER 26,1971	1471
ISA ENGLISH (SPECIAL)		- 1	RUN.	45 SPEED CODE	-	O . POINT -	ZIPAGE 36.02	36.02
	1-1 B-7	.6 1 .6	7	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	. 1	70,01		U=4
1040.6 844.8 752.4 839.1 719.0	3.70 -6.68	9-0-3-19	69 80	-	2 -272 4	1142.0	6 1 6 9	143.8
10 21,008 21,961 994,2 813,1	13.05 -8.61	25,21 55	5,92, 8 ₀ 3	3.4 1434	8 -341,8	8-1188.3	1020.	1.990
952,1 788,8 695,1 7	13,10 -9,89	29,77 57	108 19.	0541 8.1	.8 -396.1	.1225.0	1048.6 1	94.40
30 23 314 23 902 893 2 249 4 668 0 7	11.60 9.98	38.7260	2,24 85	8.6 1487	.0 .539.5	-1290.8	1132.4.1	161.0
25,601 25,893 885,1 746,7 678,0 7	10.00 -7.86	44,84	45 956	6.5 1548	5 449- 0	1359.7	1243.5 1	157,7
70 27 818 27 902 821 9 674 3 645 7 658 9 508 4 41	8.21 - 12.21	52.51 66	25 106	2.0.1636	6 842 8	1497 9	1351.2	55.3
29,382 818,5 645,0	19,32 -8,41	55,16 67	.25 110	6 4 16 49	8 604 A	-1521.6	1 428.4 1	127.2
80 29 914 29 856 812 0 633,7 612 0 630,4 533,6	11.09 -5.71	56,3667	. 39110	4.6.1639	4 -919 5	-1513.4	1 453.0' 1	150.2
382 30.273 802.5 612.3 572,8	17.38 -4.76	57,62 68	1.16 110	1.0491 0.7	6.469- 1.	-1522,3	1 475,8	
A THE CONTRACTOR OF THE PROPERTY OF THE PROPER	1 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0	202/ 668		A. 666-2		4-2	1 8 7	M. 1.2
FIRST STARTED		•	TOTAL	٠		י ב		
5 4.28 9.72 50.38 55.87 00.79 3801 1641	9	9121	١	6	17 9055	7169	6976	2026
1351 7486 8800 88.85 89.15 68.8 07.4 77.1 III		7.087	0000	000	94 8611	5689	6970	2167
3 5.06 52.99 52.44 .0.15 .3850				76	76 . 9221	6680	6935	2286
3.15 6.15 5.24 51.57 50.66 0158 3864 0567		9817		0000	22 ,7669	6328	7398	2555
3,32 6,46 8,17 47.86 49,57 ,0222 ,3877 ,0651		9795		9818 0000	•	.6273	. 9119	3004
2.53 5.77 5.23 50.44 49.88 ,0155 ,4419 ,0630		9825	Ì	0000	1	5640	1,104,	3690
7.34 11,53 47,73 52,07 ,0175 ,4739 ,1053	.0364 .0304.		0000	•			. 9333 1	3657
9,12 8,95 15,68 46,60 53,81 0217 ,4809 ,1056		i	i	197 0000	0009 61	Ī	9252	3496
8,54 10,02 18,91 47,14 56,06 ,0224 ,5034 ,1227	1960. 1440.	1896	0000	7*7. 0000.	٠.		,9238 1	3439
IN ET IN ET IN ET IN ET IN ET IN ET DAVEL								
LBM/SEC 8 8								
11132, 180.92 1,2266 1,8169 82,00 83,44 35,68								
	WBLEED	EED	W	W	P_0/P	ū	EFF-AD	9
	WTOTAL	TAL	WTOTAL	<u>}</u>	talet Adi	_	Adj.	o.,o.
					į			
Rotor Pressure Ratio = 1.8673	.02766	99	ı		1.8164	7	79.45	.9732

SUCTION ONLY, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

	ATRFOIL AERODYNAHIC SUMHARY PRIN		65.01	0C10	26,19
NSA ENGLISH (SPECIAL) N DIA-1 DIA-2 V-1 V-2 (N N N FIVE FIVE FIVE FI	-1 8-2 8-1 REE DECKE DECKE	1 8 2 V = 1 E DECREE FINSE	SPEED_COOL U	10.P01NT # 3.F	1.0 AGE 30: U. 2.
489 1034 5 831 8 961 988 4 800.3	4 01 6 06 20 3 49 8 25 25	14 53 84 792 6	1402.0 -272.9	1132 0 991	1 1044.2
912 947 3 776 8	3.54 -9 97 29	6 57 99 793 7 60 37 859		-1224 4 1049	1 1090.0
99 888 4 746 3 679 0 741 3	8 26 44 6	5 61.13 954.	9 1535,5 671,2 7 1622 1 843 3	-1344°6 1244	7 1355.8
362 610,9 635,4 626,7	39 - 8 52	67.57 1106	4 4 5 9 4 9 t		1. 1427 7
90 29 914 29 856 802 8 621 9 605,2 618,3 527,4 - 64,6 4	2.32 -4.99 -5.8	11 68 69 1110.0	1636.7 -926.	5-1515-3-1453	3-1472.0
AHRER OHEGA"B O"FAC ONEGA"B	4 d. SOT d.	FFF EFF AD	EFFER HE	H-2 H1	H - 2
4.5° 10.34 50.77 55.81 0.004 3864 11506 55.81 0.004	98 0377 9	156	7060 8551	7048 690 6775 688	03 1.1879 83 1.2044
3,13 6,07 4,97 53,51 52,42 ,0126 ,3948 ,0927	.0207	0000	7800 81		-
3,15 6,15 5,02 51,78 50,66 ,0161 ,3930 ,0600	i	į	8384	1	-;
3,4/ 6,60 4,37 46,81 47,57 ,0232 ,3863 ,0641	. 0124	0000 0000 72	6488 6948	6265	162 1.2870
6.95 7:39 11.43 47.90 52.07 .0171 .4789 .0937	0324 .0265 974	0000	1199 6811	١.	-
9 97 15 63 47 02 53 80 0208 4877 0948	0335 0262 9752	52 0000 00000	7656 6615	5650 927	6 1.3476
NCORR WCORR TO/TO PO/PO EFF-AD EFF WET IN FT IN ET IN ET		-	•	•	•
LBM/SEC 180.85 1,2267 1,8223 82,44 83,84					
	i	:	!		:
Rotor Pressure Ratio = 1,8718	WBLEED WTOTAL	WBLOW WTOTAL	Po/Po Inlet Adj.	EFF.AD Adj.	Po/Po Local
	.02762	ı	1.8223	80.38	9739

10 21 008 21 961 1029 6 752 1 10 21 008 21 961 1029 6 753 1 10 21 008 21 961 990 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	VH-1 FT/SEC FT/ 720,0 7			- E	RUN		-	5 =		9,PAGE 36.02	. ~
21,008 21,961 990,8 21,589-22,432-949,4- 23,514 23,902 83,5 27,818 27,902 83,6- 27,818 27,82-836,83,6- 27,818 27,82-836,83,6- 27,818 27,82-836,83,6- 27,818 27,82-836,83,6- 27,818 27,82-836,83,6- 20,382-30,293-622,6-		F1/SEC F1/SEC	DEGREE DEG	GREE DEGREE	DEGREEF	7/5EC F	FT/SEC FT	FT/SEC FT/SEC	F1/SEC F1/SEC 8=1127.0 992	71/5EC	1
25.601.25.893	673,3	6693	44.61	-0.57 24.63 -10.42 - 29.49 -9.65 39.30	57.7	777.6	~ 0	-326,3-1180 -361,1+1223 -518,2-1279			1
	4 1 1	546,7 = 130,7 546,7 = 130,7 559,0 = 101;6 575,4 = 68,8	42.79	11.36 51.83 -9.07 54.36 -6.22 55.58	66.34	1025.9 1025.6 1066.0	0.9491 6.24.7 6.24.7 6.49.0	-806.7-1488 -806.7-1488 -871.7-1531 -880.0-1521	1352,7 1249 1488,2 1353 1531,0 1430 1521,3 1455 1530,5 1478	1 157 5 1 157 5 1 152 5 1 1452 5	1
### 1968 1968	0 E G R E E SH	66A-B D-FAC ONEGA-B LOSS-P-LOSS-P 0127	8 LOSS ** P LOSS ** P C C S S ** P C C C C C C C C C C C C C C C C C	PROFILE POL 10442 9228 10442 9228 10137 9585 10137 9787 10146 9787 10146 9787 10285 96787 10285 96787 10285 96787	1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 00000000	21 A T 1 C C C C C C C C C C C C C C C C C C	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	6575 6532 6532 6632 6632 6631	2 1 1 1 2 1 4 2 1 1 1 1 1 1 1 1 1 1 1 1	
Rotor Pressure Ratio = 1.9343				W _{BLEED} W _{TOTAL}		WBLOW WTOTAL		P _o /P _o Inlet Adj.	EFF-AD Adj.	L -	o /P
				.02843		I		1.8699	79.14		.9671

SUCTION ONLY, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

STATOR ANGLES	531			•	IRFOIL	AIRFOIL AERODYNAHIC SUMMARY PRINT	IC SUMMA	RY PRIN				0:7	S a	OCTOBER 26,197	971
ESPAN DIA-1 DIA-2 V-1	A-2 V-1		2	V0 Y	-1 VO-2	1 2 2 2 2	8.2 Dr.GR.r. D	0 - 1 168 - 1	B - 2	1-17	* * * * * * * * * * * * * * * * * * *	CUOE 14 PU VO*-1 VO F*/Sr(F*/	V0 -2 U	U-1 U-2	7
5 20,409 21.	489 1030-1	0 0	723.3 788	3 73		12.2		9 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	99.45	765.9	363.7	251,6-11	12.8	95.0 103	0
21.589	1	7.2	4	١	9	3 5 7 8	4.6	50.14	10.65	775.7	410.0	377 4-12	01 + 0	42.0 108	
50 23 314 23	87.4	7,4	9 68	9	1 - 0	5 44 29	16.6	39 39	61.76	1010	445	514 3-12	73.1.11	125.2 1153	0.0
27,818		. 9	9		8 -12	40,4	-10.56	51,96	66.12		605.0	799 8-14	67.6 13	42.6.1346	
29,408	837.	0	8		۰.	41.52	64.6	54,05		1067,8	642.8	864 4-15	13.61	141 6 9 141	
95 30,382 30.	30.293 824.0	1	585,7 617	6 579	5 -47	2 44 70	4.36	55.20	67,75	1062.9 1	630.8	986 8-1509	-	466,4 1462	-:-
KSPAN INCS IN	05.0	TURN CAM	CAMBER ONEGA		C ONEGA.	0"FAC ONEGA"B LOSS"P LOSS"P	L055-p	P02/ E	EFF-P EFF-AD	,	EFF		H-2	H'-1 H'-2	.2
3.83	6	0.0	5.87	20	229 .191	5.0	5550	. 9223	188	188	6386	8941	64.70	6767	487
0		54,39	2,40	•		i	Ī	8646	0000	0000	7 7 6	H 6 1 8	6619	-	864
59.65	. 84	54.21 5	0.6702	•	į	i	!	6146	0000	0000	9300	7479	5817	7	\$012.
3 1	9.24 9.03	49.75	19.54 .03	•	4250 .0693	•	٠	9789	0000	0000	9306	. 1967.	5875	7707 1,2	2543
41.4	7	1	֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	0313 50	1	1	Γ	9634	0000	0000	7255	707	1	┤╌	35.18
11016	1.07 15.51	49 40 5	53.85	֓֟֝ 	5080 1338		-	9631	0000	0000	7257		5125	8864 1,339	161
10.89	<u>-</u>	_	•	0394 ,5230	130 1454		•	.9609	0000	0000	.7156	. 6842.	5045	8828 1,32	3282
NCORR.	WCORR	TO, TO PO, PO	O EFF-AD	EFF P	WC1/A1										
K & C	LBH/SEC	1	3	, ,	₹										
11082	1,0,0,1	4450 1 A262	919	į	- 44-44										
							3	WBLEED	_	WBLOW		P /P	Ü	EFF-AD	P ₀ /P ₀
Rotor Pres	Rotor Pressure Ratio = 1	= 1.9210					\$	^W TOTAL	-	WTOTAL		Inlet Adj.		Adj.	Local
							o.	02860		ı		1.8555	32	79,25	.9663

	ANGLES				AIRFOIL		AERODYNAH1C	SUHHAR	SUHHARY PRINT	: -	S		10:57;20		OBEK A	OCTOBER 26,1971
ESPAN DIA-1 DIA-2	. •	1/=2 1/cf. FT	VH-1	VH-2	V0-1	V0-2	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0-2 ECREE DE	8 - 1 8 E E	8 - 2 = 2 = 5 = 5 = 5 = 5 = 5 = 5 = 5 = 5 =	V 1 = 1		VO *-1 . V T/SE/ FT	/0 = 2 / SEC F		U=2 1/5E
l = 10	9 8 101 68		691.0	735.2	7.68	75.1	ا ا⇔نھا	5.83	90.00	56.70	732 8	1339.0	243 3-	100	9,166	104401
18 21 589 22 43	2 443.2		650.0		683.5	120.5	. T	10.09	29.35	60.76	7.46.7	387.2	365,5-1	210.4	9.0	-6601
30 23,314 23.9	12 865.9		581	636.1	641.3	-101.5	47.78	40	40.19	63.26	761.7	1414.0	1-4-1-4-1	262.8	1132.7	1.161.3
50 25 601 25 873	96		57 C B	652.8	626.5	88	99 9	7.0	46.25	64.13	200	. 94	7617,3-1	4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	243.8	1258.0
29 408	965.1	651.1	6043	643.6	619	7.87	45.70	6 7.9	53.26		1010.3	656 4	60,7	526.3	428.8	1427.5
90 29 914	861.2	ļ	_	640.7	635.5	-76.0	47.57	6.75	54.61	67.23	!	5 5591	.817.9.1	5.925	1453.4	1350.6
8 30,382 30,293		630.1	558 8	627.8	643,3	-53.6	49,02	4.87	56,14	67.63	_	9.6491	-832°9-1	-1525.4	1.9261	1471.8
ASPAN INCS INCH	E DECREE DEC	N A	CANBER ONEGA	۵	D-FAC OMEGA"B		1055-P	L055-p	p02/	EFF-P E	EFF-AD.	EFF	- X	N-2	H:-1	H1-2
8 4.90 7.	10.57		55.87	9210	7174.	\$2099	2	7750	8916		0000	6159	8905	6173	1469.	1.1185
4 65 7	7.06	54.43	53.85	0179	4830	2022	0511	9910	9240	0000	0000	6594	8510	5951	6849	1.1914
5.86	4 7 9	\$6.54	52,39	,0241	4908	1709	0440	.0378	1046	0000	0000	7065	9136	\$738	8159	1,1570
9.25	616	56,85	50.67	9650	4949	1025	.0284	-01.46	9690	0000	0000	8152	7371	5345	46454	1,1732
80 10.00 13.13	13 8,31	<u>~</u>	25.0	5890.	4882	10%	,0333	•0125	9494	0000	0000	7830	,7257	5435	7182	1.2344
	 	١.	7	0.57	21.2	75.7	07.72	0220	770	non	0000	050		272		1.
90 15.29 15.2	7 - 1	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	53.87	2000	54.5	7 4	000	, 50°	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0000	0000	5199	7 1 6	5218	8292	1.3387
15.26	00,01 1	j	56.06	.0837	.5560	1,008	9890.	.0385	1946.	0000	0000	0,440	7007	1,05.	. 6246	1,3276
N CORR	WCORR TO'	TO/TO PO/PO		FF-AD EFF	EFF-P WC1/A	NC1/A1										
	LBH/5EC 173.65 1.2	2545 1.9	87 - SE09 1	9.22 81	8 SQFT	36										
	•							WRIFFD	c	W	M	9/ d	٠,	EFF-AD	9	ą,
								WTOTAL	. -	Wrota		inet o	. د	Adi	!	0 -
Rotor Pressure Ratio	atio = 1,9950	0						5	ī	2	<u>,</u>	Adj.				Š
								.02996	9	Í	ı	2.5	1.9035	76.99	66	.9544

COMBINED BLOW AND SUCTION, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

14,1971 10,10	1.152 1.1545 1.1546 1.1526 1.1526 1.1526 1.1546 1.1742	P _o /P _o Local	.9819
13:62;37 OCTODEM 14,1971 17:5PEED CODE 70:POINT # 21:PAGE 16:0 75EC FTSEC FTSEC FTSEC FTSEC FTSEC 702.2 1276:1 189.2 -901.2 691.1 726.2 698.3 1275:1 -250.2 -956.5 70.4 746.5 748.8 1258.9 -441.1 -995.0 788.4 808.2 928.7 1311.2 -713.0 1192.2 993.4 940.5 1311.4 -781.3 -1182.2 999.3 940.6 1310.4 -781.3 -1182.2 999.3 940.6 1310.4 -781.3 -1182.2 999.3 940.6 1310.4 -781.3 -1182.2 999.3 940.6 1310.4 -781.3 -1182.2 999.3 940.6 1310.4 -781.3 -1182.2 999.3	7522 8344 6291 152 7009 6031 6236 159 6777 6779 6263 1190 6109 7779 153 6709 1215 5114 6099 6145 1216 5414 6099 6145 1216 5518 5511 6156 5156 5614 8550 1199 6156 5614 8550 1199	Q	44
LJ: LZ: 17 COUE 70, POINT NO**1 VU**2 FI/SEC FI/SEC = 18 Y P POINT = 25 U 2 P9 S PS = 441:1 P9 S PS * 73 D = 118 Z PS = 78 S PS PS PS PS PS PS PS PS PS PS PS PS P	22 8344 99 8031 99 77 7769 17 99 7750 17 99 1750 17 99	EFF-AD Adj.	77.44
13:62:137 SPEED CODE 70; V:-2 NO'-1; V:-2 NO'-1; V:-2 NO'-1; V:-2 NO'-1; V:-2 NO'-1; V:-2 NO'-1; V:-2 NO'-1; V:-2 NO'-1; V:-2 NO'-1; V:-2 NO'-2; V:-2		P _o /P _o Inlet Adj.	1.244
47.5PEED 7.5EC FT.SEC 7.02.2 1270.1 6.00.8 1270.2 7.48.8 1228.9 7.48.9 1271.2 9.00.8 1258.9 9.00.8 1291.9 9.00.8 1310.8 9.00.8 1310.8 9.00.8 1310.8 9.00.8 1310.8	FF.A0EFF.P 	~o = 4	
22 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	### FFE PEFE A D	W _{BLOW} W _{TOTAL}	.00620
2 VG_1 VG_2 B_1 B_2 b_1 l_1 l_1 l_1 l_2 l_2 l_3 l_3 l_3 l_3 l_3 l_3 l_3 l_3 l_3 l_3	902/66 901 101 9763 9763 9894 9855 9789 9789 9789		
ETILABLE SUSTILER BELL BELL GGREE DEGREE DE 15.50 -10.01 19.50 -10.02 29.86 -13.62 25.42 -16.66 21.95 -17.13 21.75 -17.19		W _{BLEED} W _{TOTAL}	.03110
8 8 1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	100 100 100 100 100 100 100 100 100 100		
FT/SEC FT/SEC DE 500000000000000000000000000000000000	2 1108 3 0824 1 0527 7 0960 7 0960 0 0796 0 0809 0 0809 0 0809 0 0809 0 0809 0 0809 0 0809 0 0809 0 0809 0 0809		
7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	SHOCK SHOPEAC ONEGA SHOCK SHOC		
	& m & & N & o w & O P & O		
V-2 VH-1. 920.2 67.5EC 920.2 65.6 959.5 631.2 959.5 631.2 731.3 604.7 731.3 583.2 639.2 558.9 639.2 558.9	E OEGREE DEGREE 918 818 818 818 818 818 818 818 818 818		
SPECIAL) Y = 1 FT/SEC FT/SEC 9 840.9 920.2 7 7 7 93.2 6 9 7 4 7 93.2 6 9 6 9 6 9 6 9 9 9 9 9 9 9 9 9 9 9 9	0 ' ' 0 2 •	= 1.2685	
A 10 L C S P E D I A Z F I V S P E S	#SPANDEGREE DEGREE 0	re Ratio	
STATON ARGLES NASA ENGLISH DIA-L DIA-Z BESPAN IN IN IN 10 21-008 21-489 10 21-008 21-489 10 21-008 21-489 10 21-018 21-489 10 21-0	DEGREE DEGRE OF GREEN	Rotor Pressure Ratio	
A N SEPOND 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	MARY 0 5 5 8 8 8 8	Ro	

## 47.5PEED CODE /U.POINT # 22,PAGE 36.UZ V***********************************	22.53 51.10 628.5 1165.7 -241.0 -907.1 713.2 745.6 27.02 -52.75 632.0 1160.9 -287.2 -928.7 733.0 761.6 37.25 56.00 682.2 1170.5 -413.0 -970.4 771.5 811.5 46.45 60.78 7527.6 1221.4 -549.2 11068.0 844.5 877.1 52.40 64.00 835.5 1255.4 -662.1 1128.3 944.5 947.3 55.40 64.00 835.5 1285.6 -717.6 11128.3 948.5 947.3 56.03 66.23 874.2 1295.6 -724.9 -1185.7 1015.6 1013.6 57.02 66.76 876.6 1303.7 -723.9 -1185.7 1015.6 1029.6	FAREEF-AD EFFER H-1 H-2 H7-1 H7-2
AMGLES (SPECIAL) (SP	10 21,000 21,701 748.9 747.6 581.2 731.9 472.3 -101.5 39.09 -12.40 22.53 51.10 16 21,500 22,432 717.5 725.8 562.1 700.3 445.8 -107.1 38.40 -13.11 27.02 52.75 40 23.432 717.5 725.8 562.1 700.3 445.8 -107.1 38.40 -13.66 37.25 50.70 50 23.314 23.90 24.89 -13.66 37.25 50.00 60 23.314 23.90 24.89 -13.66 37.25 50.00 60 28.89 27.816 27.80 2 562.4 57.8 2 56.40 64.00 60 60 60 60 60 60 60 60 60 60 60 60 6	

Rotor Pressure Ratio = 1.3200

9875

Po/Po Local

47.5PEED CODE 70.POINT # 24.PAGE 36.02 1 V1-2 VD-1 VD1-2 U-1 U-2 C FT/SEC FT/SEC FT/SEC FT/SEC 9 1190.5 191.1 -093.6 694.9 7 71.1 6 1126.9 -274.6 -918.6 734.5 74.2 9 1165.2 -393.7 +1002.6 793.2 813.2 9 1185.2 -393.7 +1002.6 793.2 813.2 9 1185.2 -393.7 +1002.6 793.2 9 1185.2 -393.7 +1002.6 793.3 1313.9 -672.9 +125.2 1000.5 999.6 5 1314.9 -672.9 +125.2 7 1000.5 999.6 7 1338.7 -626.9 +125.3 8 1033.7 1015.8	6780 6416 5272 1,0045 6412 6108 5272 1,0045 6132 6902 5246 9916 5619 502 5246 9916 5512 473 5645 1,0236 5503 4788 65207 1,036 6903 1,0831 4907 4581 7101 1,1539 4907 4581 7101 1,1539
# 47.5PEED # 47.5PEED # 527.9 1140.5 # 597.9 1120.9 # 597.9 1120.9 # 597.9 1120.9 # 18.5 1131.9 # 18.5 1131.9 # 18.5 1131.9 # 18.5 1131.9 # 18.5 1131.9 # 18.5 1131.9	EFF.P.EFF.AD EFF.P. TOTAL TOTAL STATIC TOTAL TOTAL STATIC TOTAL TOTAL STATIC TOTO
FUNDAL AERODYNAHIC SUHHARY FRINT RUN RUN VO-1 VO-2 B-1 B-2 B-2 B-1 B-2 B-2 B-1 B-2 B-2 B-1 B-2 B-2 B-2 B-2 B-2 B-2 B-2 B-2 B-2 B-2	A*B LOSS*P-LOSS*P- TOTAL PROFILE 000 00243 00243 95 0127 0177 95 0115 0115 95 0193 0193 95 0193 0193 95 0193 0193 95 0193 0103 95 0091
VH=1 VH=2 /5EC FT/5EC F5-5-5-5-5-5-5-5-5-5-5-5-5-5-5-5-5-5-5-	DEV TURN CAMBER OMEGA-B D-FAC-OMEGA-B B D-FAC-B
STATOR ANGLES NASA ENGLISH (SPECIAL) DIA-1 DIA-2 SEPANIN 1	INCS INCH DEV TURN CAHDER SSPAN DEGREE DE

Rotor Pressure Ratio = 1,3528

.9874

80.59

1,332

.00681

.03681

Po/Po Local

EFF.AD

Adj.

P_o/P_o Inlet Adj.

WBLOW WTOTAL

W_{BLEED} W_{TOTAL}

PATER ACTION AND TO SELECT	200		36.0.70.4.1		5
15H (SPECIAL)	Turus Turus Turus Ta	RUN # 47.SPEED	CUDE 73.	DINT # 25.PAGE	T + 1 . 1
A-2 V-1 V-2 VM-1 VM-2 VD-1 VD-2 8-1	8-2 8-1	8 -2 V -1 V			7-0
N FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC DEGREE	DEGKEE	FT/SEC FT	F1,5EC	<u>.</u>	T,SEC
21.489 753.0 676.6 539.6 657.5 525.2 -159.6 44.23	17.21	564.9	- 167al - Padi		724.0
21.961 718,3 645,2 519,6 627,0 496,0 -152,1 43,67	22.65	563.3	15 -216.7	-	745.0
22,432 686,8 623,2 497,4 604,2 473,5 -152,6 43,58	27.47	561.5	258 9	-913.6 732.4	760.4
30 23,314 23,902 631,3 575,2 472,1 544,0 419,1 -186,9 41,59	_		-371.8		810.8
+601.25.893.581.1.527.9.447.4.496.1.370.8.4.190.4.39.65		69.89 669.3 1169	7	-6-1058.Z 868.Y	878.4
70 27,818 27,902 571,3 510,2 446,7 479,4 356,3 -174,6 38,58	52,73	7.38.0	3 -587	943	5.946
471.3 374.0 -171.7 41.02	55.42	757.5	٠		996.7
80 29.914 29.856 562.4 496.3 417.1 466.3 377.3 -169.8 42.14	00.45	48 761.9	.3 -637	1 9.	1012.0
30.382 30.223 556.6 486.2 408.4 433.5 378.1 .217.8 42.80	-57.96-	749.8	. 1 . 652	7	1027.6
SOUTH THE STATE OF			1 X X Y X Y X Y X Y X Y X Y X Y X Y X Y	N=2 == 1 x++2	7
EGREE AEGREE DEGREE DEGREE SI		TOTAL TOTAL STATIC			!
2	9714	U	5148 6639	5933 4994	7 6 9 2
to 2,46 5,39 53,85 ,0005 ,3297 ,1062 ,	•	0000	•	9564. 9495.	6848
3,18 6,12 ,0012 ,3289 ,0812	.0203 .9822			9466 0545	0849
30 3,14 6,14 50.67 50.67 ,0020 ,3571 ,0641 ,	•	9° 0000° 0000°	•	•	91 66
2,76 6.09	i	• 0000	\rfloor	-	1.0177
70 2.92 6.16 49.89 .0027 .9148 .0597 .	•	0000	•	•	925001
8,45 8,92 . 52,04 ,0075 ,4546 ,0621	5046 6610	0000 0000	441 4937	4324 6566	10801
. 5740. PEAR. E800. 08.82.	67.66	• 0000•	. 4862	•	1.0739
g S	01549820	Z*0000 *0000	7847 4805	**177	1.1331.
NCORR MCORR TO/TO PO/DO EFF AD EFF D MC1/A1					
INLET INLET INLET INL					
3 6 6					
00-10 15-70 4/61-1 40-11-1					
	,	×	<u>d</u>	EFF.AD	Q
Rotor Pressure Ratio = 1.3745	BLEED	BLOW	0		0,,0
	WTOTAL	WTOTAL	inlet Adi	Adj.	Local
			·íp		
	03833	01200		6	0
	70000	01/00	1.349	/8.29	.9840

STATOR ANGLES NASA ENGLISH (SPECTAL) DIA-1 DIA-2 V-1 V-2 ESPONIN IN FT/SEC FT/SEC FT	VM-1	AIRFOIL AERODYNAHIC SUHHARY FAINT HON W 47.5PEED CODE 70, POINT W 26, PAGE 36.04 NOW W 47.5PEED CODE 70, POINT W 26, PAGE 36.04 FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC	VO=1	VO=2	B-I.	AIRFOIL AEROGYNAHIC SUHHARY -1 - VO-7 B-1 - 6-7 EC FT/SEC DEGREE DEGREE DEGREE	BY FAINT BO = 1	HUN E	47; V*=1 T/SEC F	SPEED C V - Z T/SEC F	3197193 006 7071 VOT#1 V	00. 01NT # 70*=2	47.5PEED COUE 70,POINT # 26,PAGE 36,42 1	1971 36.02 75EC
10 21.008 21.961 706.3 6	9.6 493.0	593.6	505.9	177.6	45.73	-16.65	22.79	55.11	532.1	2./601	207.5	7.22.4	712.8	745.2
30 23,314 23,902 627,2 55	8.5 475.6	57.1.8	483.9	176.8	45.49	-17.19	38.21	58.63.	537.5	1098.6.	355.8-	-937.9	732.6	761.2
60 25,601 25,893 575,5 50	2,3 416.0	461.6	197.6	198.0	43.70	23.22	48.52	66.79	628.6	1171.5	471.1e.	076.6	868.7	878.6
70 27.818 27.902 569.0 48	3,6 408,9 5,9 382,5	444.4	395.7 - 417.2 -	190.8	44.07	23.24	53,27	66.66	683°9 695 _° 4	1221.3	5.80.7-1	1137.6	943.9	946.B 997.0
90 29 914 29 856 563,0 46	9.6 377.8	431.4	417.5 -	5°581	47.86	123.57	57.69	70.20	707.0	1273.9	597,6-1	9.861	1 0.510	017.1
	- 1	117.2	4 12 0	1.00		-53.62.	-1 z • 35	4.0 • 0.7		7.6771	, -r - , , , o -	700.07	1-x*0r0	02/-2
**SPANDEGREE DEGREE DEGREE DEGREE	1	QMEGARB_DRFAC_OMEGA-B_LOSS+P_LOSS+PPOZZEFF+P_EFF+ADEFF=P Smock	-FAC-0H	EGA-8-1	055+p.	LOSS - P	P02/	EFF:P.E	FF-AD	FFEER	1-1	H-2	N=1	H 1-2
6 4.12 7.04	~	4	1598	, 111	0266	0.26.3	9724	900	0000	5.78.4	6487	5629	4626	9673
19 4 48 7 44 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	53,85	0021	3675 1148 0281	1 1 4 8	0281	9142 0000 0000 0000 4142 6750 1850 1850	9737	0000	0000	9809	6178 5739	5216	4729 9575	9573
30 5,52 8,51	50.68		9404	9960.	.0251	.0234	.9021	0000	0000		.5481	1474.	.5040	9702
70 8,38 11,61	88 67	.0275	4436	1040	.0217	.0233	9879	-• 0000°-	0000	-\$017.	5013	4349	.5948.	0516
. 85 14 67 15 33	52.06	40556	5111	1001	0351	6110	- 1	0000	anna	6618	4874	4069	15931	1080
20° 11° 02° 21° 21° 02° 21° 21° 21° 21° 21° 21° 21° 21° 21° 2	50.05	0440	5468	1417	0740	.0222	9795	0000	0000 0000 6432	6432	4764 3689	4004	1 1,19	0,00
NCORR MCORR TO/TO PO/PO	u	FETAD EEFTP MC1/AL	-P-4C1/	VI-										

Rotor Pressure Ratio = 1,3933

P _o /P _o Local	.9982
EFF.AD Adj.	74.85
Po/Po Inlet Adj.	1.360
WBLOW WTOTAL	.00751
W _{BLEED} W _{TOTAL}	.04217

	1			1		×	O TE VEN		MINT TREEDOM TIMES TO THE TOTAL TO THE TENTE	7	_!	1		61.0		٠ د	. 1 1 7 7
NASA ENGLISH		(SPECIAL)									X 0 X	÷	SPELD	47.SPEED CUDE 10, PUINT	U, PCINT	*	21, PAGE JOOUL
DIA-I DIA-Z		>	7-5	- 117	VH=2	1-07	V 0 - Z		9 = 9		2-,8	-	V = 2		×0.4	-	0-7
S SPANIN		FT/SEC FT/SEC FT/SEC	I/SEC F	T/SEC F	TISEC F	T/SEC F	T/SEC C	EGREE D	T/SEC FT/SEC FT/SEC DEGREE DEGREE DEGREE DEGREE F1/SEC	EGREE	DEGMEE		FTISEC	FT/SEC F1/SEC F1/SEC	F1/56C	FI/SEC	11/56
5 20.409	21.489	1089.8	1109.4	827.8	1105.2	708.8	-96.0	40.57	70.4-	18.64	45.89	874.9		1587.9 -262.6-1140.1	6-1140.	991.6	1104
10 21.008	21.961	21.008 21.961 1054.3 1096.2	096.2	5 - 5 - 5	1088.6	669	-128.6	39.42	-6.74	23.32	47.68	1		u -351.	-351.2-1195.6		7 1007
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23.31	43,404		9 4 4 6 5	761.7	978.2	529.1	-179.4	34,78	-10.39	36.38	53.88		1657		-403.6-1340.	7 1132.	9 - 9
25,601	25,893	975.9	935.8	741.6	920.9	466.1	-166.3	32,14	-10.24	46,34	57,11	1075	1696.	3 -777.	8-1424.	4 1243.	9 1256
27.818	27.902	0.908	840.8	702.6	823.2	394.8	-171.2	29.32	-11.76	53.68	61.67	1187.3	1734.	-8.956.8	8-1526.	9 1351.	6 1355
86 29 408	29.382	802.7	805.7	708.9	793.2	376.6	-141.0	27.98	-10.07	56.03	63.18	1268.8	1 1757.	7-1052.	2-1568.	6 1428.	1427
80 29.914	29,656	7.887	791.3	688.3	783.2	384.9	-112.4	29.22	91.8-	57.21	63.38	1271.1	1746.	2-1068.5-	5-1563.	0 1453.	1450
86 30,382 30,293	30.293	765.5	756.3	6.88.9	746.5	L.	-121-2	30.60	-9.24	58.77	9	_	1759	5-1086.7-1593	7-1593.	1 1476.	2 1471
		1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	: :											•	-		
INCS	NCH	INCS INCH DEV TURN CANBER ONEGA-B D-FAC ONEGA-B LOSS-P LOSS-P POST EFF-P EFF-AD	TURN	AMBER	HEGA-B	D-FAC C	MEGA-B	1.055-P	LOSS-P	P02/	EFF	EFF-AD	EFF-P	- -	H-2	1	I
MSPANDEGREE DEGREE DEGREE DEGREE	DEGREE	DEGREE DE	GREE D	EGREE S	SHOCK		_	TOTAL PROFILE	ROFILE	-01	TOTAL TOTAL STATIC	TOTAL	STATIC				
6 1981	11.1	11:43	45,54	55,87	*DD39	1625	12401	. 0596	•0586	+6928		• DOD1	*5c8 * 2 0000 . 0000 *	4 , 9588	8 .9197	17 .7700	10 1.4022
16.1- 01			46.10	53,84	0,00.	.1508	.1943		.0483	h / 16 °		0000	.0000 2.812		4 .9687		4 1 . 4 4
16 -2,01	. 0	6161	49.64	52,40	0,000	41407	1486	0385	.0375	99.69	0000	1000	876-1 0000	0.68.	0556. 0	7886	V
•	67		45.17	50.67	.0016	1410	.1207	.0333	.0329	.9578	0000	.0000	0 1.6240	9808. 0	45/8. 9	48485	37.1
į	2 4 4 5		42.39	49.60	.0010	.1522.	0440	0283	0280	9700		Ī			8 . 8 9 8	. 9343	3 1.40
M .6.38			41.08	49.88	0000	1894	.1289	81.50	0418	.9641		1	.0000 2.1405	:	8 .7323	11.0317	1.51
. 1	80: h=	9.87	38,05	52,08	0000	.2217	1732	9650	0596	.9522	0000		000048.160	1 .6942	2 :698	10 1.0967	7 1.52
	16.2-	13.42	37,38	53,80	00000	.2208	61910	0.500	.0570	9569	0000	•	000035.376	ľ	2 .682	3 1.0955	10507
96 - 3.23	-3a23 -1a76	14.43	19.84	56.06	. 0000	2529	.1906	.0679	*0679	49521	0000	į	.0000-5.692	0959	849	1.1.090	1.507
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P_o/P_o Local

EFF-AD Adj.

P_o/P_o Inlet Adj.

WBLOW WTOTAL

WBLEED WTOTAL

COMBINED BLOW AND SUCTION, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

- 6	,			•	,			.	•		
-	٠ <u>٠</u> .	1060	1356	1472. H 2		1,2158	1,291	- t	1,352		Po/Po Local
OCTOBER	7.5EC FT	1021-72 1049.5 1133.3	352.3 429.6	H 1	6973	. 7396	9036	9339	• 4252		
	VO:-2 FT/SEC F	0-1+77-3- 4-1212-5 8-1286-3	536.2	535,1 H-2	7131	6604 6238	6202 5578	5353	. 5004		EFF-AD Adj.
	10, polny -1 vo ^e -2 Ec ft/sec 3,6-1136,	**	7 7	7				١,	*		_
	U	1	9 9	.2 -936 P H-1	' '			- -	•		Po/Po Inlet Adj.
1	* SPEED V=2 V=2 1910.	1478.6		1651	6534 6534 6659	936					~ o
į	V . 1	801.7 801.7 858.8 956.9	062.6 1108.9	1108.7 FF-AD	0000	0000	.0000	0000.	0000.		ب `
:	8 -2 6 REE F	57.06	2 2 4	68,39 1108, EFF-P EFF-AD	9346 .0000 .0000 .65 9460 .0000 .0000 .65	0000	0000	0000	0000		WBLOW WTOTAL
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HARY	906	00 29	1 1	en le			• •				ED FAL
NS 311	. B.	000		-5.86 LOSS-P	PROF1LE 0373	ļ	1	- 1	.0286		W _{BLEED} W _{TOTAL}
AIRFOIL ALRODYNAMIC SUNHARY PRINI	8-1 DEGREE	43.04	39,35	540.662.5 42,325,86 D-FAC OMEGA-8 LOSS-P LOSS-P	1014L FROFILE 3 ,0392 ,0373	0248	0203	.0278	.03		
IL AER	V0-2 /SEC D	122.0	107.9	-62.5 EGA-8	1583	0959	0668	0805	.1017 .4.1 .7.5.0 .7.0		
AIRFO	Ε_			540.6	3819	3949	3931	1	289 S 94		
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		1 1	1 1	608.1 OHEGA-8	5H0CK • 0079	4110°	- 1	- 1	.02 		
	VH-1 1/56C 751.7	780.6 694.3 739.6 667.1	633.3	593.7 AMBER	12 49'99 55,87	52,44	49.57	52.05			
	V-2 1/5EC-F 840.7	1 !	4.6.6	611.3 URN C	8 6 0 0 9 0	52.11	50:72	6 6 6			
	(SPECIAL) V=1 -F1/SEC-F1 9 1039,8	1 !		803.0 C	GREE DE (5,95	- 1	~ .	10/10 10/10 10/10	= 1.8672	
دم	(SPEC) 2 V=1		1 1	73 803 0EV	0E GR	-	1	- 1	WCORR INCET		
44611	15H 01A-2 1N 21,48	22,432	29,382	30.293	0.GRCE	5.64	-	` '	C 13 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	ure Rat	
STATOR ANGLES	-NASA ENGLISH (SPECIAL DIA-1 DIA-2 V-1 PAN-IN	16 21,589 22,432 30 23,314 -23,902-	70 — 27; 818 — 27; 902 85 29; 408 29; 382 90 — 29; 914 — 29; 856	30,382 INCS	EGREE C	3.17	2.56	8.0		Rotor Pressure Ratio	
55	-NASA ENGLISH (SPECIAL)	 	5 8 8 1	8	*SPANDEGREE DEGREE DEGREE 1937 4,29 10,1	: # R	 3. R	8 8 	78	Roto	

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NACA FIGHT IN CEPTALL	AIRFOTE" AERODYNAHIC"SURHARY"PRINT	1		12	21:01:10	00.10	OCTORFR 22.1971	1971
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989.4 799.7 716.5 791.6		25.16 56.07	0.7 792.0 1418.7		-436.3-1477,1 1018.5	177.1 10		1064.7
22.432 948-1 774.5 686.1 763.7	43.64 -9.59	29.73 57.81	191.0	791.0 1476.5 -392.3-1216.4	392.3-1	216.4 10	1046.7 1	1087.5
23.902 897.6 736.1 670.2 7	41,70 -9.35	38.50 60.40		470.3 -	-533.2-1278.4	778.4 11		1158.8
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821.2 659.9 643.5 646.2 510.1 -	3A.40 -11.67	57.47 66.4R	_		-838.6-1485.9		~	1352.7
- 88 79:408 29:382 811.5 639.7 625.7 633.6 516.7 - 87.3	39.55 -7.84	55.46 67.	67.28 11R3.6 1639.2	i	-909.0-1511.8		_	1424.5
90 29.914 29.856 803.4 625.1 604.4 622.5 529.2 -55.7	141.21 -5.10	56.73 67.	67.54 1101.8 1626.9		-921.1-1503.2		14 50 .3 1	1447.5
- 08. 30.382 30.293 793.5 598.4 565.6 596.4 535.2 -48.7	42.42 -4.67	54.01 68.	68.54: 1105.7 1630.4		-937.7-1517.3	517.3 14		1468.6
THE THE THE TOTAL CAMBER OFFEE OFFEE OFFEE OFFEE	d-5501 d-5501	PO2/ FFF-	FEF-P FFF-An	d-333	- - -	M-2	N - 1	C - N
*SPANDEGREE DEGREE DEGREE DEGREE SHOCK	TOTAL PROFILE	_	TOTALS					,
1.78 4.69 10.22 50.29 55.87	.0359 .0338	9405	.0000	.6882	6999	1064	6 86 7 1, 1886	1886
5.29 7.34 51.69 53.84 .0100	.0305 .0279		0000 00				68 89 1	1.2008
19 3.23 6.17 5.36 53.22 52.44 .0129 .3966 .0837	.0216 .0183	0000 - 2016	00000	1	!	ì		1.2141
50.56 .0165 .4024		•						1.2391
3.59 6.73 9.61	.0241 .01 FR	0000 6416.	0000. 00	. 1975	. 7571	6158	.8126 1	1.2774
2.73 5.97 5.80 50.07 49.89 ,0163		.9811 .0000	noon. no	PO+8.	6969	.5517	1 8868.	1,3535
7.00 7.47 12.09 47.39	.0236 .0174	.9817 .0000	000.	. 8416	6833	5297	9295 1	1.3573
9.19 9.02 16.49 46.30	.0250 .0173	51885 • OUDD	_				•	1.3400
. 86 8 56 10 05 19 47 09 56 07 0718 5117 0917	.0350 .0271	.9752 .06	•0000 •0000	. 8066	•6621	4064	9231 1	1.3383
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rotor ressure Katio = 1.8719	אַ מּרְינֵינ		P.C.W	ם סיק	_	Ť		0
	"TOTAL		TOTAL	Adj		¥aj.		Local
	.02764	Ų,	.00480	1.814		80.19		9724

COMBINED BLOW AND SUCTION, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

STATOR ANGLES WIRE FULL TERESTALLING	AIRFOIL AERODYNAHIC SUHHARY FRINT	- T	13:50:24	20.	UBER 25,1971 29.046F 34.02
54 15FC1AL1 01A-2 V-1 V-2 VH-1 VH-2 VO-1 VO-2	8-2 8*-1	• _	V*-2 V0*-1	V0*=Z· U-1	, .
N FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC FT/SEC DE	DEGREE DEGREE	ŗ.		:1/5Ec FT/5E	C_FT/SEC
21,489 1027.8 ,793.2 725.0 789.9 728.6	4 -5.18 19.95	71.10 7.15	1367.2 -263.2-1115.	1115. 7 791.7	7 1044.2
22,432 946,2 734,8 678 0 722.9	3 -10-11 29-83	59,39 782,6		• •	٠
23.319 23.902 873.1 689.2 627.7 677.7 506.8	7	18 22	1454,2 526,1-1	286.7	_
25,601 25,893 869,2 703,7 641,3 697,3 585,8	6 -7,77 45,70	62,74 9,8,3	1522.4 -657.2-1	353,4 1	_
27.818 27.902 828,0 658,6 628,0 645,6	7 -11:37 -52:25	66,50 1026,8	218-61	1561.9.5841-0	.7 1355 B
29.408 29,382 838.2 650.0 630.5 641.3 552.3	2 -9.38 54.28	67.31 1079.9		-1533,7 1429	.0 1427.7
	4 -4.29 56.71	67.83 1077.4	619.8 -900.6	9241 5 8151-9	3 1472.0
	-	EFF-P EFF-AD	- I	H-2 KI-	
TELEGREE DEGREE DEGREE DEGREE SHOCK	FROF 11 E	747		!	!
2 50,32 55,87 ,0110 ,4182 ,1810	•	0000 0000	_		71517 +0
1+41° ZST+° 2110° +8°CS Z2°ZS C6°9 19°S -89°Z	. 2170.	0000 0000	1.		F
3,76 6,70 4,57 54,57 52,40 ,0149 ,4398 ,1358	.0312	•	•		-
5.58 8.58 4.75 54.50 50.67 0253 4442 0735	.0133	•	•		-
8,93 8,25 50,23 49,54 ,0348 ,4297 ,0627	.0085	•	•	•	-
5.03 8.26 6,12 52,05 49,91 ,0286 ,4723 ,0607	.0124	•	•		-
8,72 4.09 10,51 50,60 52,01 ,0294 ,4991 ,1038	.0257		•	•	-
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LBH/SEC s s					
16017					
	WBLEED	WBLOW	9/°d	EFF-AD	و ف
Kotor Pressure Ratio = 1.9210	WTOTAL	WTOTAL	Inlet Adj.	Adj.	Local
	.02856	.00469	1.853	79.60	.9671

COMBINED BLOW AND SUCTION, STATOR BLADE ELEMENT PERFORMANCE AND DESIGN DATA

1~1 1 1 1 1 1 1 1 1		~
44.000 10.0000 10.000 10.000 10.000 10.000 10.000 10.000 10.000 10.00	Po/Po Local	7196.
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10. FOLLOW 1 = 10. FOLLOW 10. FOL	EFF-AD Adj.	79.17
22 CODE 10.PD1NT FEE CODE 10.PD1NT SEC FT/SEC F1/SEC 10.4 - 224, 5-1198, 652 10.4 - 224, 5-1198, 652 10.4 - 224, 5-1198, 652 10.4 - 224, 5-1198, 652 10.4 - 224, 5-1198, 652 10.4 - 224, 5-1198, 652 10.4 - 224, 5-1198, 652 10.4 - 224, 5-1198, 652 10.4 - 224, 5-1198, 652 10.4 - 224, 5-1198, 652 10.4 - 224, 5-1298, 652 10.4 - 224, 5-1	a°	998'1
	P _o /P _o Inlet Adj.	1.8
\$3,55 \$1,55 \$1,55 \$1,55 \$1,57 \$1,50 \$1	W.	×
2	W _{BLOW} W _{TOTAL}	.00486
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2000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	W _{BLEED} W _{TOTAL}	.02845
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AIRFOIL AERODYNAH VMR2 VMR2 VM2 TSEC FT/SEC FT/SEC DEGRIE 736.6 66.5 = 128.1 44.67 736.6 66.5 = 128.1 44.67 736.6 66.5 = 137.0 44.33 674.9 617.0 = 137.0 44.33 652.4 547.8 = 100.4 40.85 652.4 547.8 = 100.4 40.85 652.4 547.8 = 100.4 40.85 652.4 547.8 = 100.4 40.85 652.4 547.8 = 100.4 40.85 652.4 547.8 = 100.4 40.85 605.8 564.8 = 17.2 45.15 601.2 49.9 8 18.2 6 01.58 601.2 44.8 6 01.58 601.2 44.8 6 01.58 601.3 44.8 6 01.58 601.3 44.8 6 01.58 601.3 44.8 6 01.58 601.3 6 46.7 6 06.3 1 60.20 601.3 6 46.7 6 06.3 1 60.20 601.3 6 46.7 6 06.3 1 60.20 601.3 6 46.7 6 06.3 1 60.20 601.3 6 46.7 6 06.3 1 60.20 601.3 6 46.7 6 06.3 1 60.20 601.3 6 85.7 8 110.8 60.3 1 FFAU EFF WELTAR NLET INLET LBM SEC 82.08 83.5 8 34.32		
7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
FT/SEC FT 736.6 736.6 736.6 674.9 674.9 651.9 635.8 626.4 626.4 626.5 606.5 601.35 601		
ECIAL) /SEC F1/SEC F	= 1.9343	
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E E E E E E E E E E E E E E E E E E E	ressur	
NASA ENGLISH	Rotor Pressure Ratio	
NASA NASA NASA 10 10 20 20 20 20 20 20 20 20 20 20 20 20 20	es.	

	AIRFOIL AFRODYNAMIC SCHMARY PRINT	RY PRINT		21:02:15		OCTORER 22.19.71
ISH (SPECTAL)		RUN	# 53+SI	53.SPFFD CORE 10.POINT	B THION-D	26 . PAGF 36.02
- 1	-7 B-1 R-2	B 1 A 2	۷۰-1	10A 2/	VG • -2	U-1 U-2
ISEC FIVSEC FIVSEC FIVSEC FI	C DEGREF DEGREF D	FGREF OFGREF	FIVSFC FT.	ISEC FIVER	FTVSFC FI	1757 C F175FC
0 748.9	-60.0 47.42 -4.69 19.38 56.48 729.5 1323.6 -24.2.1-1103.4 991.0 1043.	19.38 55.48	729.5 1323.6	323.6 -242.	1-1103.4	991.0 1043.4
981.6 704.8 679.4 698.1 708.5	5.7 46.70 -7.83	24,64 59,00	747.9 1	1355.8 -311.0	-311.6-1162,1	1020,1 1066,3
16 21.589 22. 432 941.4 680.6 646.9 670.8 683.9 -11	5.4 46.60 -9.77	29.19 60.89	743.4		-364.3-1204.6 1048.3	1048, 3 1089, 2
1 23-902 863-8 632-8	3.2 47.99 -9.11	40.79 63.64	758 . U 1		-490.3-1260.8	1132.0 1160.6
25.893 859.0 650.9	3.4 46.88 -8.25	46.37 64.50	851.1	496.4 -616.	1-1350.6	1243.1 1257.2
842.4 636.8	1.9 45.35 -10.39	51.74 66.91			-751.4-1469.7 1	1350.7 1354.8
863.2	2.7 . 45.92 -9.19	53.18 F7.4F	1006.61	655.8 -807.	m	1427.9 1426.7
859-1 637-9	3.9 47.80 -6.37	54.74 67.38	999.7 11	1647.3 -816.	-816.2-1520.5 1	1452 .5 1449.7
- 86 30.382 30.293 849.9 624.2 554.8 622.2 643.8 -49.	9.1 49.25 -4.56	56.29 67.75	i	999.4 1643.0 -831.4-1520.6	4-1520.6	1475,2 1470,9
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7.97 11.71 52.12 55.87 .0181 .4727	6050	.9190 .0016.	6433. 0000. nonn.	.6647 .A7AR	4 .6123	.6312 1,1050
7.74 7.61 54.03 53,85 ,0184 ,4879	.2004 .0507 .0461	.9249 • 00000			9 .5AB3	
8.97 5.12 56.37 52.40 .0247 .4964	• 04 35	9411 .0000	0000	.7159 .A117		.6388 1,1493
9.46 12.45 6.11 57.10 50.67 .0513 .5065	8620.	TOOD. 5178.	• 0000	0 81 70 . 7 35 0	•	7
49.55 .0703 .4980	.0378	.96 A1 .0000	0000		.5386	.7146 1.2336
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172.82 1.25445 1.8652 30.32 81.10						
13676 07676	i					

Po/Po Local

EFF.AD Adj.

Po/Po Inlet Adj.

WBLOW WTOTAL

WBLEED WTOTAL

Rotor Pressure Ratio = 1.9951

.9546

77.00

1.896

.00493

.03011

APPENDIX D

SYMBOLS

A	_	area, ft ²
A _{an}	_	annulus area, ft ²
$A_{\mathbf{f}}$	_	frontal area, ft ²
C_p	_	pressure coefficient
c	_	chord length, in.
D	_	Diffusion factor
g_{C}	_	conversion factor, 32.17 lb _m ft/lb sec ²
Н		interference shape parameter
ⁱ m	_	incidence angle, angle between inlet air direction and line tangent to blade mean camber line at leading edge, degrees
i _S	-	incidence angle, angle between inlet air direction and line tangent to blade suction surface at leading edge, degrees
M		Mach number
MR		mass average in radial directions
N	_	rotor speed, rpm
n	_	interger whose reciprocal defines the exponent for the power law representation of the boundary layer velocity distribution
P	_	total pressure, psfa
p	-	static pressure, psfa
q	-	dynamic pressure, psfa
r	_	radius, ft
R	_	gas constant for air, ft-lb/lb _m °R

S	_	blade spacing, in.
T	_	total temperature, °R
t	_	static temperature, °R
t/c	_	thickness-to-chord ratio
U	-	rotor speed, ft/sec
V	_	air velocity, ft/sec
Vm	_	meridional velocity $(Vr^2 + Vz^2)^{1/2}$, ft/sec
W	_	weight flow, lb/sec
β	_	absolute air angle, $\cot^{-1} (Vm/V\theta)$, degree
β΄	_	relative air angle, $\cot^{-1} (Vm/V\theta')$, degree
Γ_3	_	Gerster shape parameter
γ	_	ratio of specific heats for air, 1.4
Δβ	_	air turning angle, degree
Δeta^*	_	camber angle, degree
δ	-	ratio of inlet total pressure to standard pressure of 2116.22 lb/ft ² *
δ	_	Boundary Layer Thickness *
δ°	_	deviation angle, angle between exit air direction and tangent to blade mean camber line at trailing edge, degrees
δ*		boundary layer displacement thickness
ϵ		angle between tangent to streamline projected on meridional plane and axial direction, degree
η	_	efficiency, %
θ_3		interference momentum loss area

^{*}Symbols δ and θ have dual meaning in this report. Both are such common uses that a change might result in confusion. However the use in context should be clear.

θ ratio of inlet total temperature to standard temperature of 518.6°R* θ boundary layer momentum thickness* viscosity, ft²/sec mass density, $lb-sec^2/ft^4$ ρ solidity, ratio of chord to spacing σ total pressure loss coefficient ω angular velocity of rotor, radians/sec ω Superscripts relative to moving blades designates blade metal angle axial direction a adiabatic ad fs free stream polytropic or profile p radial direction r meridional direction (in z-r plane)

shock

suction surface

axial direction Z

m

sh

SS

free stream direction Х

^{*}Symbols δ and θ have dual meaning in this report. Both are such common uses that a change might result in confusion. However the use in context should be clear.

$\boldsymbol{ heta}$	_	tangential direction
0	_	plenum chamber
7		instrument plane upstream of rotor
8	_	station at rotor leading edge
9	_	station at rotor trailing edge
10	-	station at stator leading edge
11	_	station at stator trailing edge
12	_	instrument plane downstream of stator

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